



# STUDIO ITA

INGEGNERIA CIVILE E TECNOLOGIE ANTINCENDIO

## Consorzio di Bonifica **PIANURA di FERRARA**



44121 Ferrara - Via Borgo dei Leoni, 28  
Codice Fiscale 93076450381  
Tel.: 0532.218211 - Fax: 0532.211402  
E-mail: info@bonifica Ferrara.it



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**MINISTERO  
DELL'INTERNO**

**RIPRISTINO DELLA FUNZIONALITÀ IDRAULICA DELLA CONDOTTA  
FINSIDER AMMALORATA COLLOCATA LUNGO IL CANALE NAVIGLIO IN  
LOCALITÀ BAURA (FE)**

## PROGETTO ESECUTIVO

IL RESPONSABILE DEL PROCEDIMENTO:  
ING. MARCO VOLPIN

IL PROGETTISTA:



ING. ELISA MANIEZZO

## RELAZIONE DI CALCOLO

DATA EMISS.  
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09/03/2023

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02

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0722-CONBFE-PE **02** 01

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ALLEGATI:

ALLEGATO A: Output di calcolo ProSap



## **2. PRINCIPALI FONTI BIBLIOGRAFICHE**

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- [14] Gruppo di lavoro CPTI (2004). Catalogo Parametrico dei Terremoti Italiani, versione 2004 (CPTI04), INGV, Bologna
- [15] Gutenberg B., Richter C.F. (1944). Frequency of earthquakes in California. Bulletin of the Seismological Society of America, 34(4), 1985-1988.
- [16] Associazione Geotecnica Italiana AGI (2005). Linee Guida “Aspetti geotecnici della progettazione in zona sismica”, Patron, Bologna



### **3. NORMATIVA DI RIFERIMENTO**

Le Normative di riferimento adottate sono le seguenti:

D.M. 20 febbraio 2018 "Norme Tecniche per le Costruzioni"

Circ.C.S.LL.PP. n.617 del 2 febbraio 2009, "Istruzioni per l'applicazione delle "Norme Tecniche per le Costruzioni" di cui al DM del 14 gennaio 2008".

Eurocodice EC7, parti 1,2,3.

Eurocodice EC8, parte 5.



#### 4. PREMESSA

L'opera oggetto di intervento fa parte di un progetto di tombamento del canale Naviglio in località Baura e Pontegradella, proposto intorno agli anni '60 dal Comune di Ferrara per motivi di tipo igienico sanitario. La problematica rilevata all'epoca, era legata agli scarichi acque nere nel suddetto canale, con conseguenti emanazioni di cattivi odori.

A seguito di tale richiesta è stata emessa la Concessione n. 2718 a favore del Comune di Ferrara, per la realizzazione di un tombamento in c.a. a sezione quadrata, lungo circa 60m. Tale tombamento è stato poi allungato di altri 80 m ed è stato realizzato con una tubazione tipo finsider oggetto del presente progetto.

In definitiva, il tombamento ha sviluppo lineare totale (parte in c.a.+ finsider) pari a 139m.

Per quanto concerne la sezione trasversale del tubo finsider, compatibilmente con le attuali condizioni dell'opera (ved. capitolo **Errore. L'origine riferimento non è stata trovata.**), sono state eseguite misure in sito che definiscono una luce netta del tubo pari a 4m e una altezza di 3m.

La restante geometria dell'opera è stata ricostruita a partire da informazioni bibliografiche inerenti opere similari.

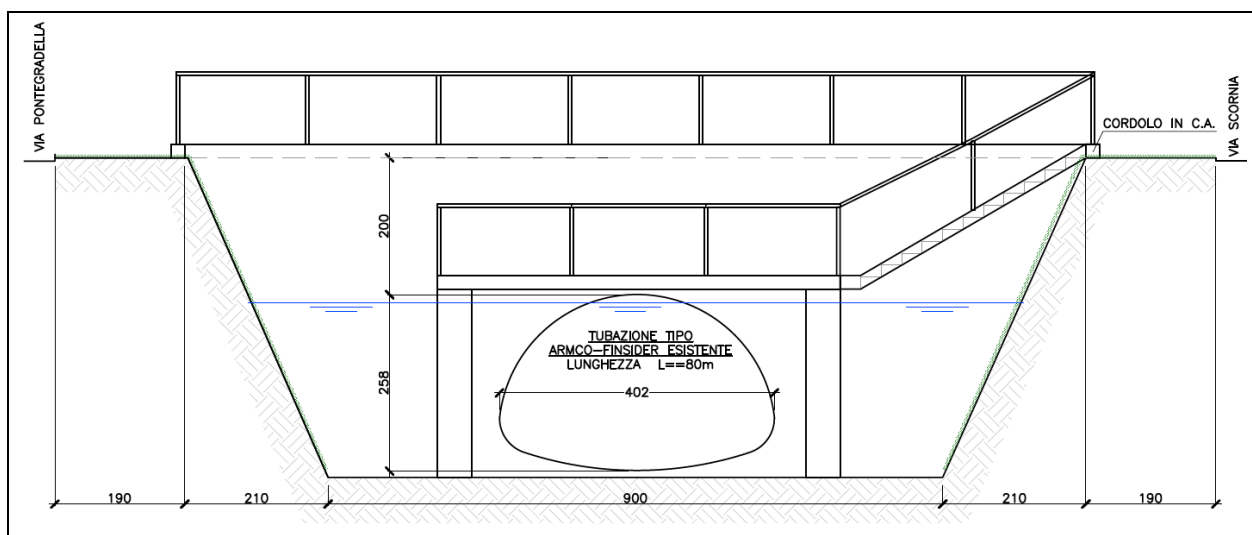


Figura 1: Sezione opera stato di fatto

La sottoscritta Ing. Elisa Maniezzo, è stata incaricata dal Consorzio di Bonifica della Pianura di Ferrara, di eseguire il progetto esecutivo di relining del manufatto esistente.

## 5. MANUFATTO ESISTENTE

Il manufatto esistente è un tubo finsider a sezione ribassata, per il quale non esiste documentazione agli atti presso gli Enti coinvolti. In considerazione del fatto che il tubo è in funzione e pertanto pieno d'acqua si è proceduto nel seguente modo:

- rilievo della sezione di imbocco
- assunzione delle dimensioni dell'opera sulla base di quanto rilevato, sulla letteratura relativa alla tipologia di opera e su quanto riscontrato in opere simili
- accantonamento di una cifra adeguata nel QE per procedere ad un rilievo di dettaglio alla apertura del cantirre, che consenta di definire l'esatto raggio di curvatura delle armature.

Per quanto riguarda spessori del guscio e sezioni resistenti, vale quanto indicato nella presente relazione relative alla seguente geometria:

Luce=4020 mm

Freccia=2580 mm

Spessore strutturale=6 mm

Dalla video ispezione condotta sul manufatto, è stato possibile verificare **l'impossibilità di agire con interventi di riparazione locale** in quanto lo stato di conservazione dello stesso è particolarmente problematico. In molti punti, infatti, si sono verificati principi di corrosione delle lastre in acciaio.



*Figura 2: Foto dello stato di fatto del tubo*



## **6. VALUTAZIONE DELLA SICUREZZA**

La valutazione della sicurezza sull'opera esistente non si rende necessaria in quanto il nuovo guscio in calcestruzzo, ricavato all'interno dell'attuale finsider, verrà progettato per sorreggere i carichi previsti dalle NTC2018 e sostituirà dal punto di vista strutturale l'attuale condotta.

## 7. INTERVENTO DI PROGETTO

### 7.1 Caratteristiche geometriche

Considerate le condizioni di degrado del manufatto e la necessità di non demolire la strada passante sopra il manufatto, l'unico intervento di progetto fattibile consiste nel relining del tubo esistente con la realizzazione di uno nuovo al suo interno.

Il nuovo tubo avrà profilo longitudinale e sezione trasversale del tutto simile a quello esistente, ma con dimensioni leggermente inferiori.

Si prevede di realizzare una **tubazione in cemento armato gettato in opera**, utilizzando il tubo esistente come guscio esterno ed un cassero interno sagomato ad hoc in polistirene.

Il nuovo manufatto dovrà avere le seguenti caratteristiche geometriche.

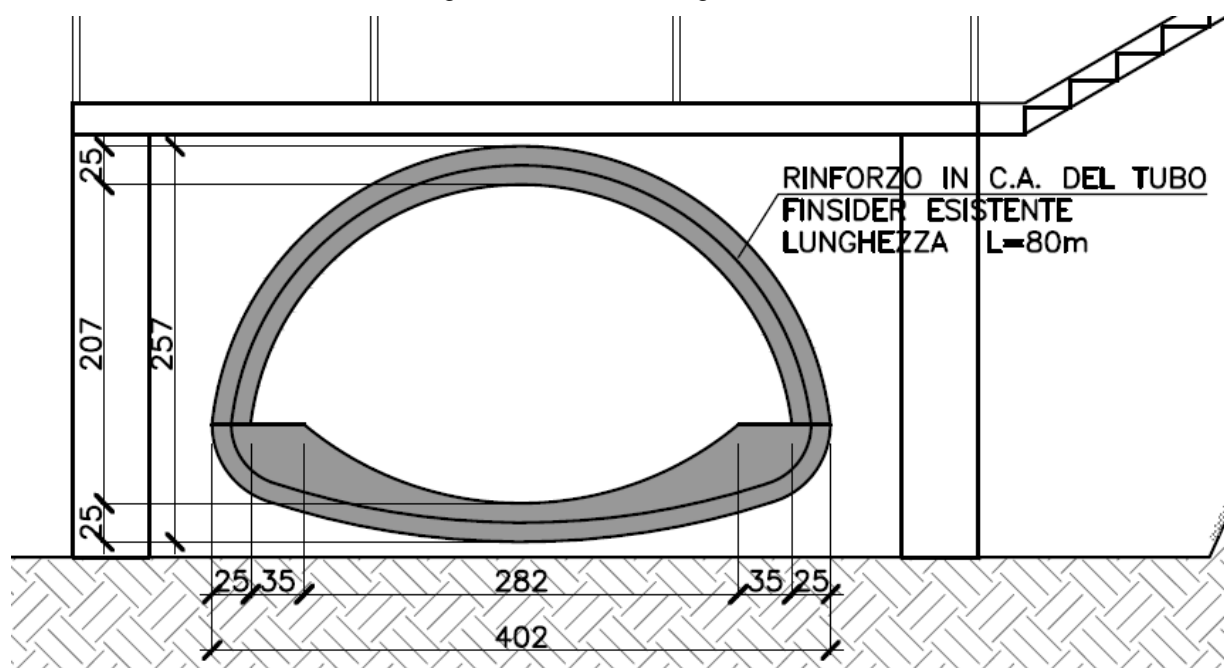


Figura 3: Sezione trasversale manufatto

La **tubazione in CALCESTRUZZO** avrà le seguenti caratteristiche geometriche:

Luce=4020 mm

Freccia=2570 mm

Spessore strutturale=250 mm

Ricoprimento su tubazione esistente: 200 cm (riferito al piano finito stradale)



## 7.2 Materiali utilizzati

### **Calcestruzzo SCC autocompattante UNI EN 206-1 UNI EN 206-9 UNI 11040**

Di seguito si riassumo le caratteristiche di resistenza:

- Classe di esposizione ambientale: XC2
- Classe di resistenza: CLASSE C32/40
- Rapporto A/C massimo: 0,60
- Classe di spandimento: SF3
- Diametro massimo degli aggregati: 15 mm

### **Calcestruzzo lavorabile a frattazzo UNI EN 206-1 UNI EN 206-9 UNI 11040**

Di seguito si riassumo le caratteristiche di resistenza:

- Classe di esposizione ambientale: XC2
- Classe di resistenza: CLASSE C32/40
- Rapporto A/C massimo: 0,60
- Classe di consistenza: S3
- Diametro massimo degli aggregati: 15 mm

### **Acciaio per cemento armato**

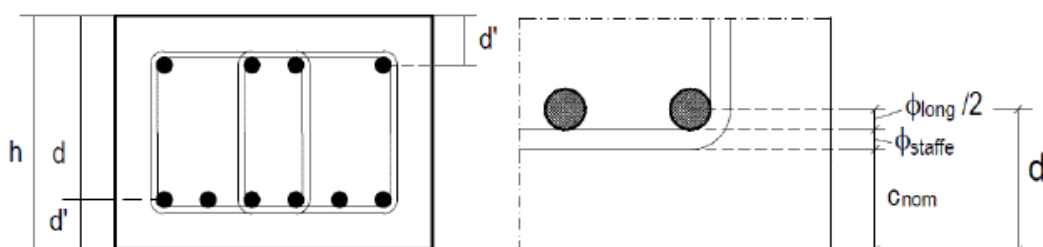
Acciaio del tipo B450C c.s. avente le seguenti caratteristiche:

- |   |  |
|---|--|
| - Tensione di snervamento caratteristica        | $f_{yk} = 450 \text{ N/mm}^2$                    |
| - Tensione caratteristica a rottura             | $f_{tk} = 540 \text{ N/mm}^2$                    |
| - Resistenza di calcolo                         | $f_{yd} = f_{yk}/\gamma = 391,30 \text{ N/mm}^2$ |
| - Deformazione caratteristica al carico massimo | $\varepsilon_{uk} = 7.5\%$                       |
| - Deformazione di progetto                      | $\varepsilon_{ud} = 6.75\%$                      |

### 7.3 Copriferro di progetto

Il calcolo del copriferro di progetto è stato condotto in ottemperanza a quanto prescritto dall'EC2.

$$c_{nom} = c_{min} + \Delta c_{dev}$$



Specificatamente:

$c_{nom}$  = copriferro minimo di progetto (ved. formula soprastante);

$c_{min,b}$  = copriferro minimo per garantire l'aderenza – tale valore è stabilito dalla tabella seguente.

prospetto 4.2 Copriferro minimo,  $c_{min,b}$ , richiesto con riferimento all'aderenza

Requisito relativo all'aderenza	
Disposizione delle armature	Copriferro minimo $c_{min,b}$ <sup>*)</sup>
Isolate	Diametro della barra
Raggruppate	Diametro equivalente ( $\phi_n$ ) (vedere punto 8.9.1)
*) Se la dimensione nominale massima dell'aggregato è maggiore di 32 mm, si raccomanda di maggiorare $c_{min,b}$ di 5 mm.	

Nel caso in oggetto le armature sono di tipo isolate.

$c_{min, dur}$  = copriferro minimo per garantire la durabilità – tale valore è stabilito dalla tabella seguente sulla base della classe di esposizione e della classe strutturale.

Requisito ambientale per $c_{min, dur}$ (mm)							
Classe strutturale	Classe di esposizione secondo il prospetto 4.1						
	X0	XC1	XC2 / XC3	XC4	XD1 / XS1	XD2 / XS2	XD3 / XS3
S1	10	10	10	15	20	25	30
S2	10	10	15	20	25	30	35
S3	10	10	20	25	30	35	40
S4	10	15	25	30	35	40	45
S5	15	20	30	35	40	45	50
S6	20	25	35	40	45	50	55

Nel caso di specie la struttura rientra nella classe di esposizione XC2.

La classe strutturale raccomandata per la struttura, avente  $V_n = 50$  anni, è S4.



$\Delta c_{dev}$  = tolleranza di esecuzione varia da 0 a 10 mm  $\rightarrow$  per il caso in oggetto è stata posta pari a 5mm.

Pertanto, nel caso in oggetto, si ha:

VERIFICA DI DURABILITA' EC 2	
Classe di esposizione	XC2
Classe strutturale	S3
Misura aggregato MAX	15
Armature isolate	si
Numero Barre	/
$c_{min,dur}$	20
$\Phi$	16
$c_{min,b}$	16
$c_{min}$	20
$\Delta c_{dev}$	10
$c_{nom}$	30
$c_{prog}$	30
VERIFICA	OK

VERIFICA DI DURABILITA' EC 2	
Classe di esposizione	XC2
Classe strutturale	S5
Misura aggregato MAX	15
Armature isolate	si
Numero Barre	/
$c_{min,dur}$	30
$\Phi$	16
$c_{min,b}$	16
$c_{min}$	30
$\Delta c_{dev}$	10
$c_{nom}$	40
$c_{prog}$	40
VERIFICA	OK

Per il manufatto di progetto si prescrive quindi un copriferro minimo  $c = 4$  cm.



## 7.4 Caratteristiche geotecniche del sito

Le caratteristiche litologiche del sottosuolo sono state dedotte dalla cartografia regionale disponibile sul portale della RER e

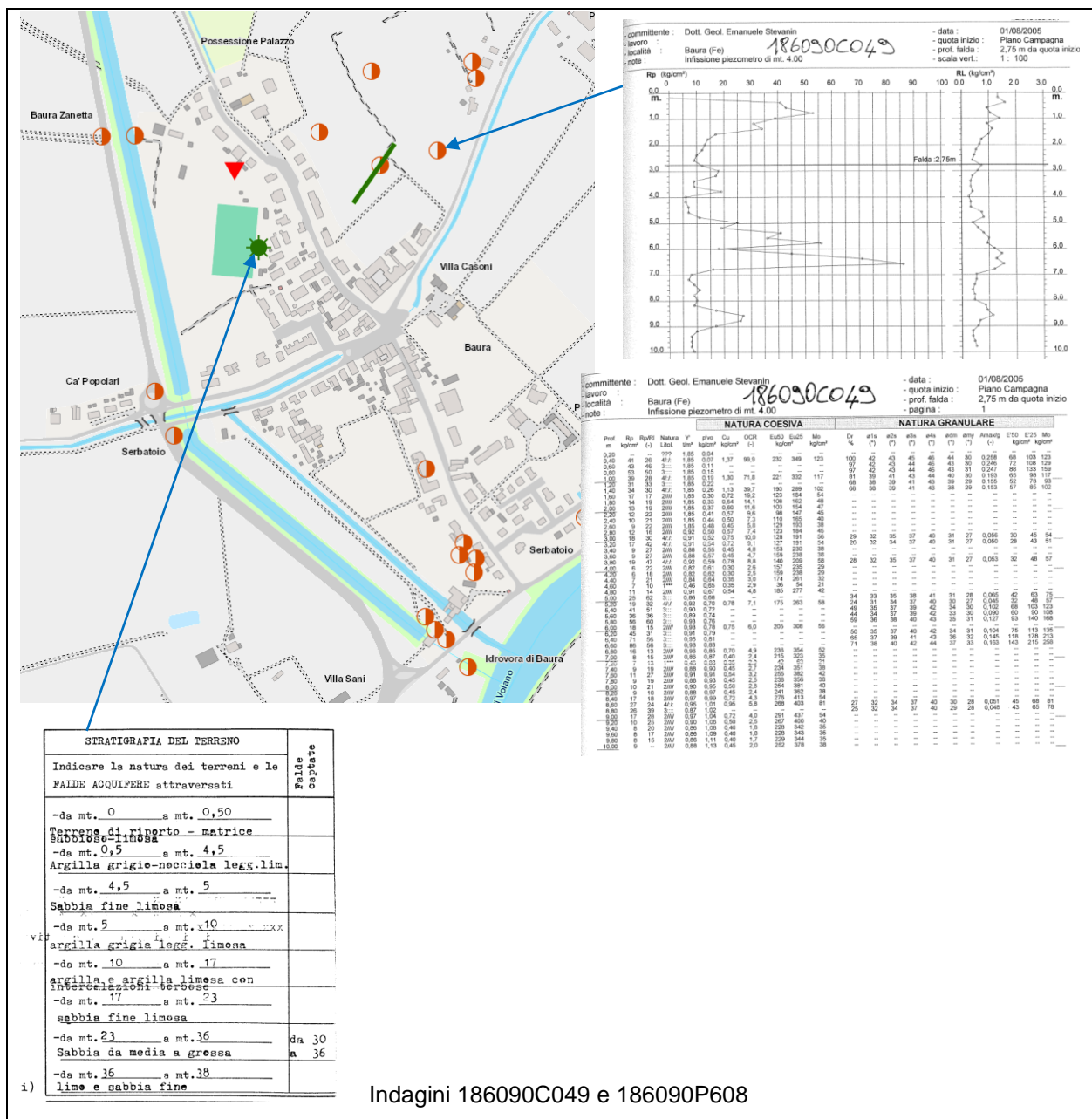


Figura 4: Banca Dati prove Geognostiche RER

Il terreno di fondazione del manufatto (piano di posa a circa 5 metri dal p.c. ha le seguenti caratteristiche:



 $\gamma_{\text{unsat}} = 17 \text{ kN/mc}$  $\gamma_{\text{sat}} = 19 \text{ kN/mc}$  $\phi = 34^\circ$  $c_u = 50 \text{ kPa}$  $E_s = 3 \text{ MPa}$ 

Calcolo del Ks				
$\mu =$	0,5			
$E_s =$	3000	kN/mq	modulo medio terreno	
$E_F =$	3,15E+07	kN/mq	modulo fondazione	
$B =$	1	m	larghezza fondazione	
$s =$	0,2	m	spessore fondazione	
$I_F =$	0,000667	m <sup>4</sup>		
$k_s =$	2211	kN/mc	0,221	kg/cmc
Prof. piano di posa	4,57	m		

Per il materiale di rinfiamento del tubo esistente si assumono le seguenti caratteristiche:

 $\gamma_{\text{unsat}} = 17 \text{ kN/mc}$  $\gamma_{\text{sat}} = 19 \text{ kN/mc}$  $\phi = 25^\circ$  $c' = 5 \text{ kN/Mq}$  $E_s = 3 \text{ MPa}$ **POSIZIONE FALDA:**

Si considera la falda coincidente con il piano campagna.

## 7.5 Caratteristiche sismiche del sito

Si riportano alcuni estratti cartografici degli studi di microzonazione sismica condotti dal Comune di Ferrara, che hanno permesso di identificare eventuali problematiche in termini di liquefazione del terreno e stabilire la categoria di sottosuolo del terreno di fondazione.

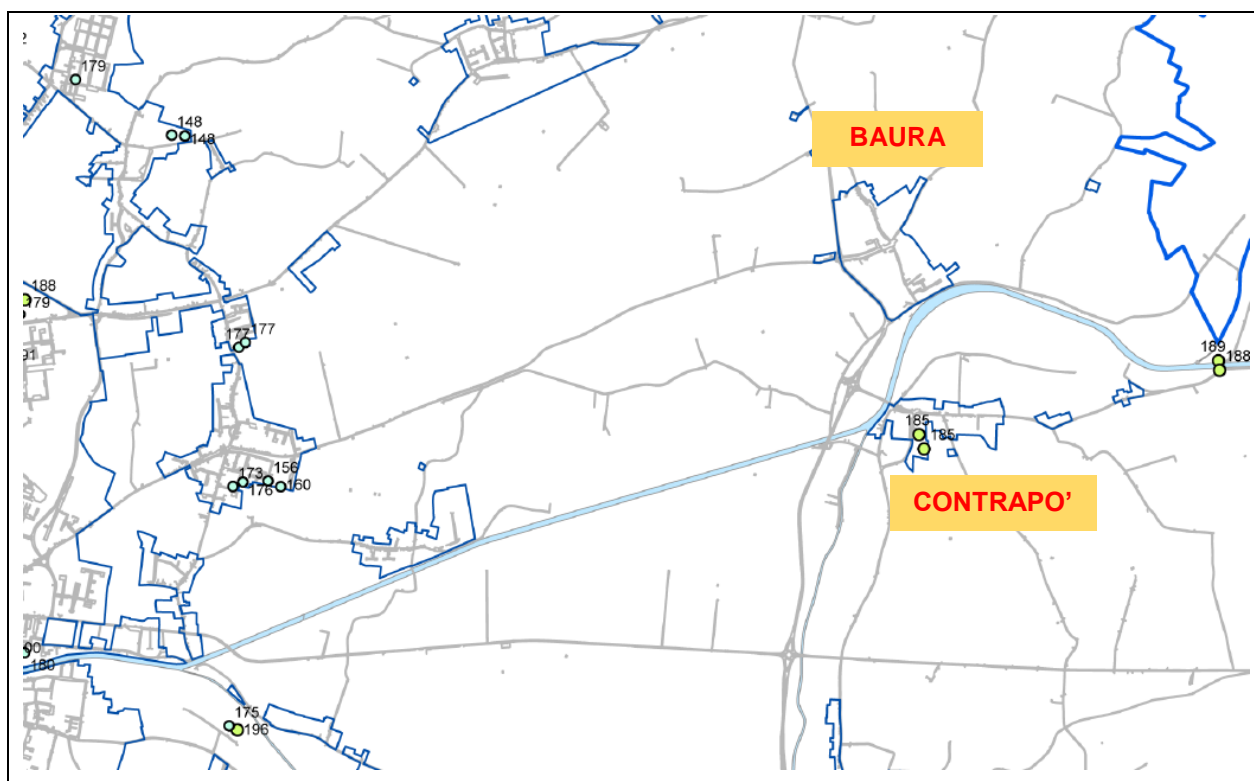


Figura 5: Mappa delle rilevazioni delle Velocità delle Onde di Taglio Vs,30

Poiché non sono disponibili indagini specifiche nell'area di intervento, si fa riferimento ai risultati ottenuti nella vicina frazione di Contrapò, in comune di Ferrara Vs,30=185 m/s.

Nella cartografia della RER (ved Figura 4) è presente uno stendimento sismico in prossimità del manufatto, che rileva Vs,30=326 m/s.

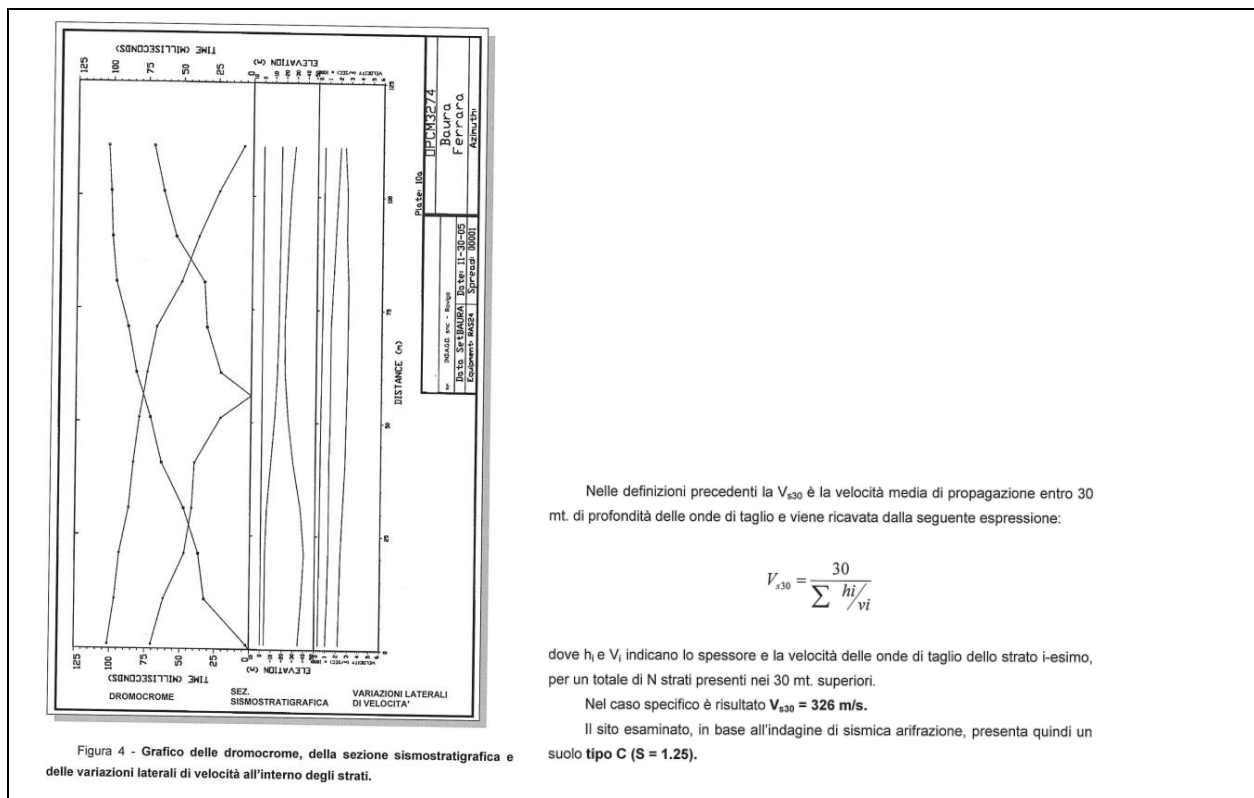


Figura 6: Stendimento sismico DB RER N. 186090H001

Per il sito in esame si assume una **Categoria Terreno C**.

Dal punto di vista del rischio potenziale di liquefazione, si evince che il manufatto si colloca in un area con rischio **BASSO**.

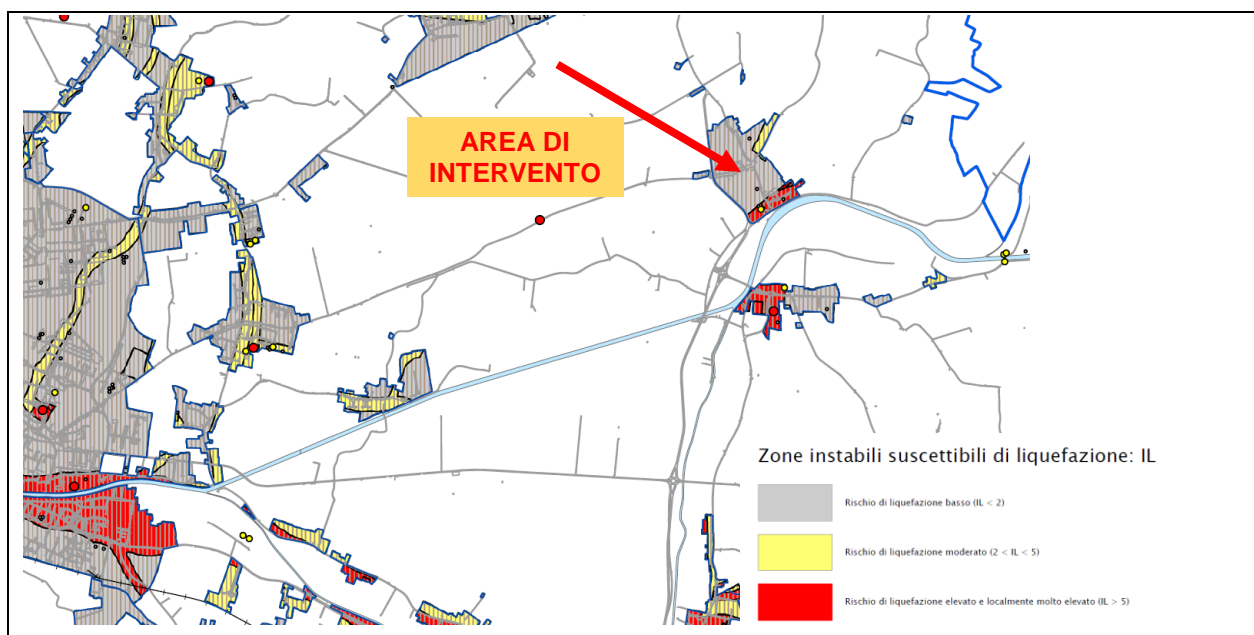


Figura 7: Mappa potenziale di liquefazione

## 7.6 Carichi di progetto

### 7.6.1 Carichi permanenti

I carichi permanenti agenti sul manufatto sono i seguenti:

1. Peso proprio della struttura (applicato direttamente dal programma)
2. Peso del terreno di ricoprimento + pacchetto stradale
3. Spinta a riposo del terreno con  $k_0=0.57$
4. Spinta della falda
5. Sottospinta idraulica
6. Acqua interna al manufatto

I valori di tali carichi sono riportati nell'Allegato A alla presente relazione.

### 7.6.2 Carichi mobili verticali

Con riferimento alle norme vigenti come azione variabile da traffico si assume quella relativa ai:

#### PONTI DI I CATEGORIA – schema di carico 1

T

ale carico è costituito da:

**Carico tandem**  $Q_{1,k}$  concentrato: ossia il mezzo convenzionale da 600kN a due assi da 300 kN ognuno, con interasse di 1,20 m lungo il senso di marcia e di larghezza 2,40m (comprese le dimensioni delle impronte).

**Carico distribuito**  $q_{1,k}$  da 9kN/m<sup>2</sup> uniformemente distribuito su tutta la sezione trasversale modellata.

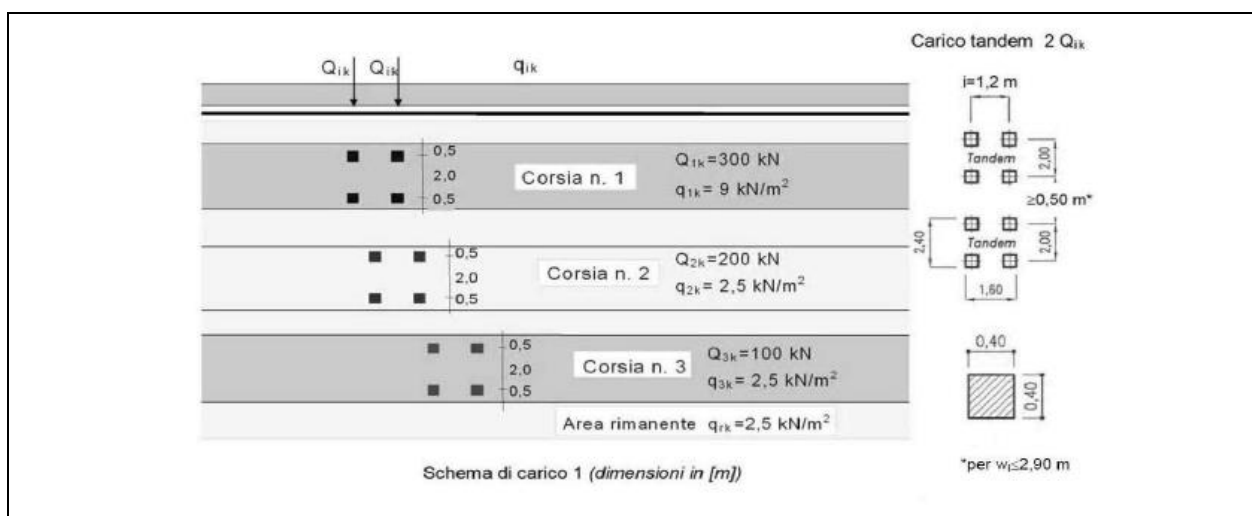


Figura 8: Variabili da traffico NTC2018

Tenendo conto della ripartizione dei carichi dovuta al terreno di ricoprimento, nel caso di carico Tandem in chiave al manufatto il carico è stato applicato con il segue schema:

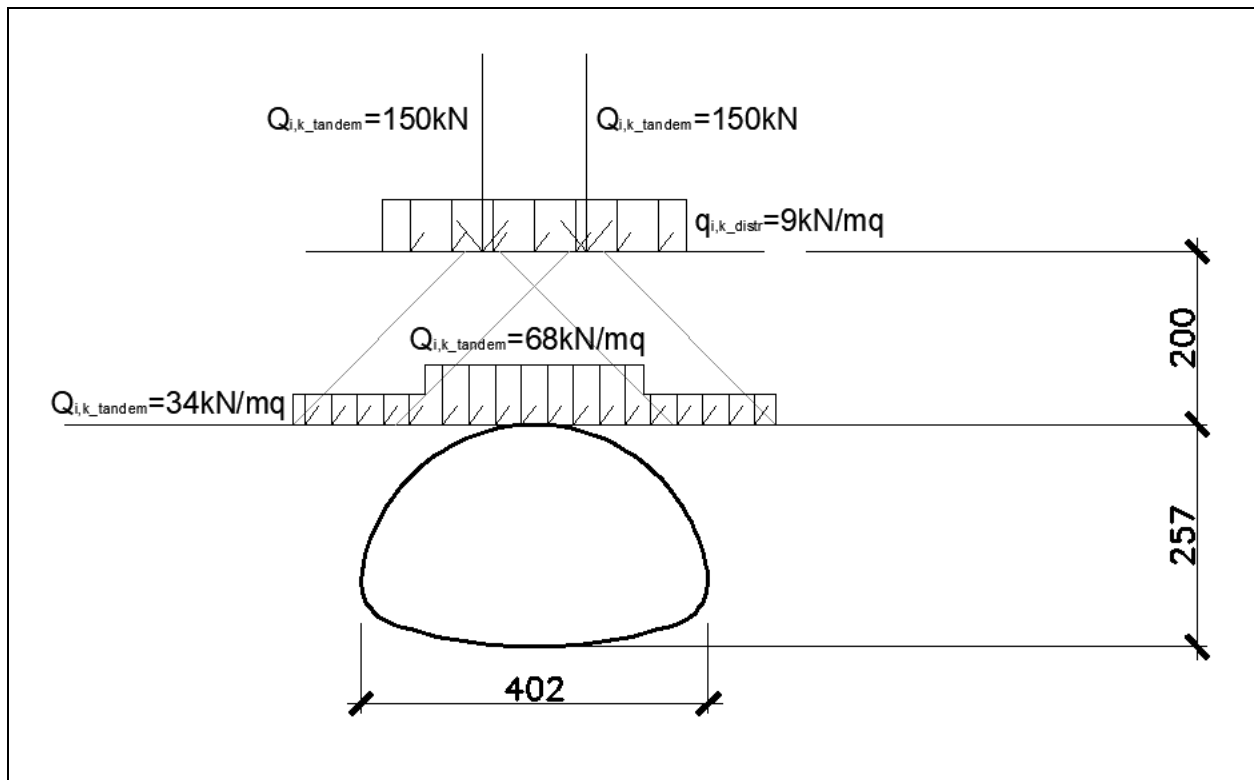


Figura 9: Schema Variabili da traffico sul manufatto

Nel caso di carico esterno al manufatto, si è assunta un spinta aggiuntiva sull'opera schematizzata come segue:

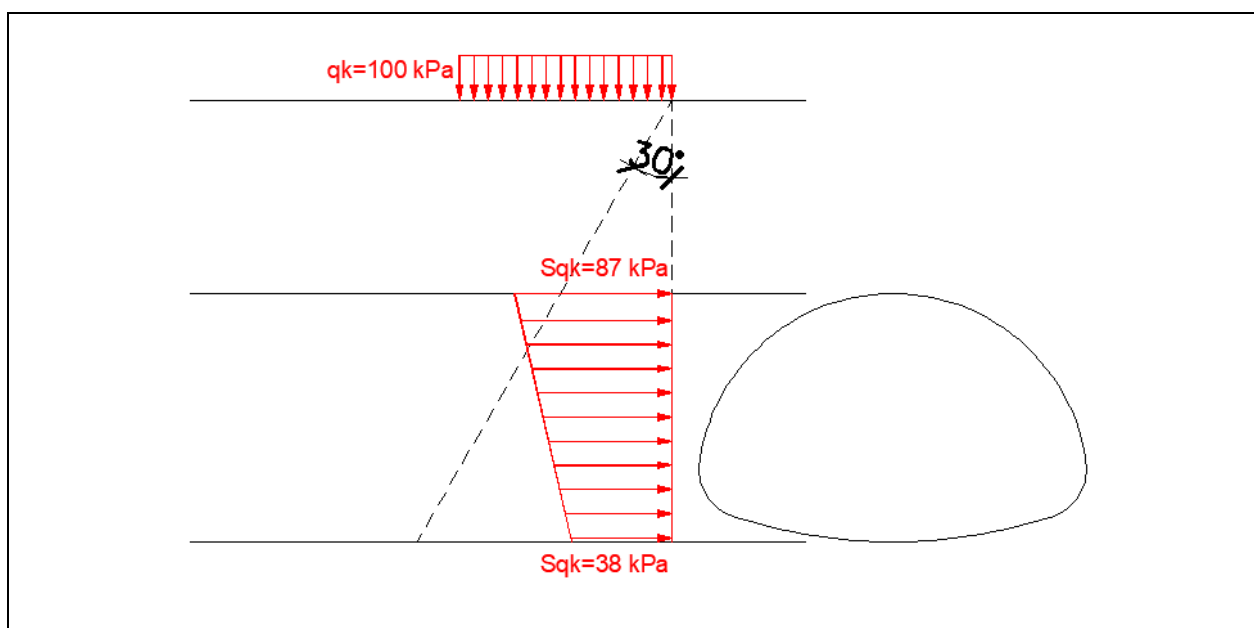


Figura 10: Spinta dei carichi mobili

### 7.6.3 Carichi sismici

L'opera è soggetta alle azioni sismiche di normativa (per maggiori dettagli si rimanda all'Allegato A) e pertanto anche alla spinta sismica sul manufatto calcolata come segue:

$$F_h = P \cdot k_h$$

$$(SLV) \quad k_h = \beta_m \cdot \frac{a_{max}}{g} = 0,513 \cdot 0,38 = 0,19$$

$$k_v = \pm 0,5 \cdot k_h = 0,09$$

P = peso proprio;

k = coefficienti sismici;

$$\beta_m = 0,38$$

Ai sensi delle NTC2018 si assume che l'incremento di spinta dovuta al sisma agisca nello stesso punto di quella statica.

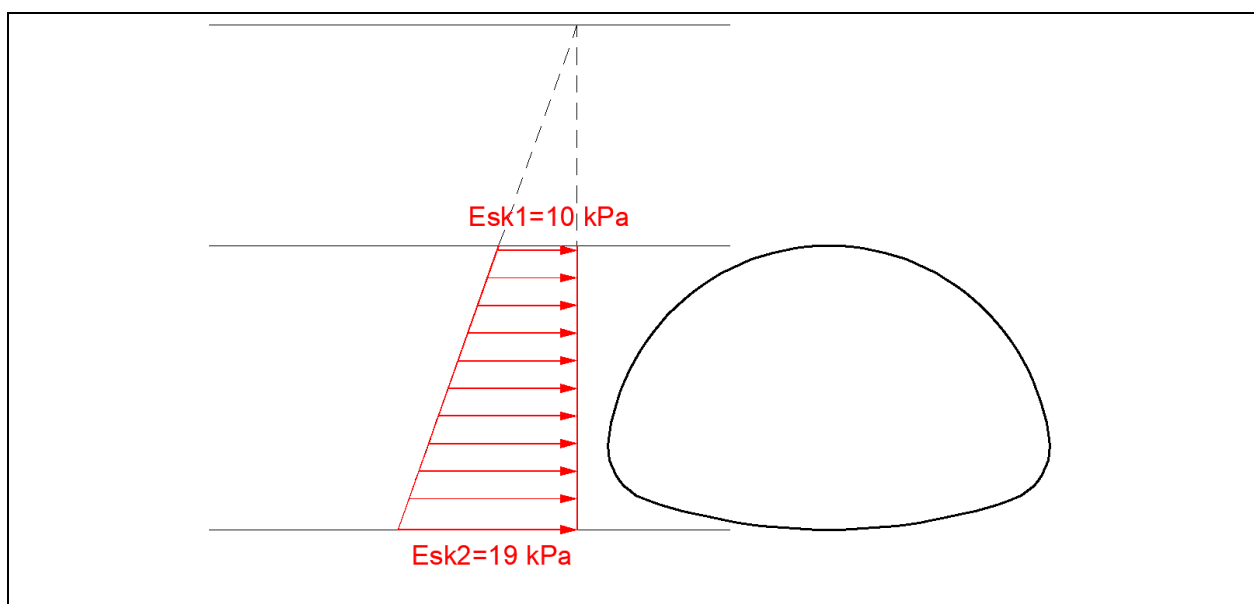


Figura 11: Azioni sul manufatto in condizioni sismiche

### 7.7 Casi di carico

I carichi precedentemente esposti sono stati applicati alla struttura come esplicitato nell'Allegato A.

## 7.8 Combinazioni di carico

Le combinazioni di carico di progetto sono quelle stabilite dalle NTC2018 al capitolo 2.5.3, relativamente i valori da utilizzare, si fa riferimento alla tabella 5.1.IV delle NTC 2018, che mette insieme il gruppo di azioni ed il modello principale:

Gruppo di azioni	Carichi sulla superficie carrabile					Carichi su marciapiedi e piste ciclabili non sormontabili
	Carichi verticali			Carichi orizzontali		Carichi verticali
	Modello principale (schemi di carico 1, 2, 3, 4 e 6)	Veicoli speciali	Folla (Schema di carico 5)	Frenatura	Forza centrifuga	Carico uniformemente distribuito
1	Valore caratteristico					Schema di carico 5 con valore di combinazione 2,5kN/m <sup>2</sup>
2a	Valore frequente			Valore caratteristico		
2b	Valore frequente				Valore caratteristico	
3 (*)						Schema di carico 5 con valore caratteristico 5,0kN/m <sup>2</sup>
4 (**)			Schema di carico 5 con valore caratteristico 5,0kN/m <sup>2</sup>			Schema di carico 5 con valore caratteristico 5,0kN/m <sup>2</sup>
5 (***)	Da definirsi per il singolo progetto	Valore caratteristico o nominale				

(\*) Ponti pedonali  
(\*\*) Da considerare solo se richiesto dal particolare progetto (ad es. ponti in zona urbana)  
(\*\*\*) Da considerare solo se si considerano veicoli speciali

Nel nostro caso, quindi si utilizzano i **valori caratteristici**.

Per quanto concerne i coefficienti parziali delle azioni si fa riferimento a quanto di seguito riportato:

Tab. 5.1.V – Coefficienti parziali di sicurezza per le combinazioni di carico agli SLU

		Coefficiente	EQU <sup>(a)</sup>	A1	A2
Azioni permanenti $g_1$ e $g_3$	favorevoli	$\gamma_{G1}$ e $\gamma_{G3}$	0,90	1,00	1,00
	sfavorevoli		1,10	1,35	1,00
Azioni permanenti non strutturali <sup>(2)</sup> $g_2$	favorevoli	$\gamma_{G2}$	0,00	0,00	0,00
	sfavorevoli		1,50	1,50	1,30
Azioni variabili da traffico	favorevoli	$\gamma_Q$	0,90	0,90	0,90
	sfavorevoli		1,35	1,35	1,15
Azioni variabili	favorevoli	$\gamma_{Qi}$	0,00	0,00	0,00
	sfavorevoli		1,50	1,50	1,30
Distorsioni e presollecitazioni di progetto	favorevoli	$\gamma_{\epsilon 1}$	0,90	1,00	1,00
	sfavorevoli		1,00 <sup>(3)</sup>	1,00 <sup>(4)</sup>	1,00
Ritiro e viscosità, Cedimenti vincolari	favorevoli	$\gamma_{\epsilon 2}, \gamma_{\epsilon 3}, \gamma_{\epsilon 4}$	0,00	0,00	0,00
	sfavorevoli		1,20	1,20	1,00



Come prescritto dalle NTC 2018, poiché si sta eseguendo una verifica strutturale che coinvolge azioni di tipo geotecnico, le verifiche nei confronti degli stati limite ultimi strutturali possono essere eseguite seguendo l'Approccio 1 Combinazione 1, utilizzando per le azioni i coefficienti della colonna A1.

Di seguito le combinazioni impiegate.

Per maggiori dettagli si rimanda all'Allegato A.

	Ggk PP	G1k Perm	G1k ko	G1k H <sub>2</sub> O int	G1k H <sub>2</sub> O est	Qk q1k	Qk Q1k	Qk Spinta traf.	Es sisma	Qk Spinta sis.
Comb. SLU A1 1	1.35	1.35	1.35	1.35	1.35	0	0	0	0	0
Comb. SLU A1 2	1	1	1	1	1	0	0	0	0	0
Comb. SLU A1 3	1.35	1.35	1.35	1.35	1.35	1.35	1.35	0	0	0
Comb. SLU A1 4	1	1	1	1	1	1.35	1.35	0	0	0
Comb. SLU A1 5	1.35	1.35	1.35	1.35	1.35	1.01	1.01	0	0	0
Comb. SLU A1 6	1	1	1	1	1	1.01	1.01	0	0	0
Comb. SLU A1 7	1.35	1.35	1.35	1.35	1.35	0	0	1.01	0	0
Comb. SLU A1 8	1	1	1	1	1	0	0	1.01	0	0
Comb. SLU A1 9	1.35	1.35	1.35	1.35	1.35	0	0	1.35	0	0
Comb. SLU A1 10	1	1	1	1	1	0	0	1.35	0	0
Comb. SLU A1 11 vuoto	1.35	1.35	1.35	0	1.35	0	0	0	0	0
Comb. SLU A1 (SLV sism.) 12	1	1	1	1	1	0	0	0	1	0
Comb. SLE(rara) 13	1	1	1	1	1	0	0	0	0	0
Comb. SLE(rara) 14	1	1	1	1	1	1	1	0	0	0
Comb. SLE(rara) 15	1	1	1	1	1	0.75	0.75	0	0	0
Comb. SLE(rara) 16	1	1	1	1	1	0	0	0.75	0	0
Comb. SLE(rara) 17	1	1	1	1	1	0	0	1	0	0
Comb. SLE(freq.) 18	1	1	1	1	1	0	0	0	0	0
Comb. SLE(freq.) 19	1	1	1	1	1	0.75	0.75	0	0	0
Comb. SLE(freq.) 20	1	1	1	1	1	0	0	0.75	0	0
Comb. SLE(perm.) 21	1	1	1	1	1	0	0	0	0	0

## 7.9 Esito del calcolo

Il calcolo completo di tutto quanto richiesto dalle NTC2018 è riportato nell'Allegato A. I risultati sono relativi ad un metro lineare di opera.

Il guscio di progetto, con spessore 25 cm in cemento armato C32/40 risulta verificata con il seguente schema di armature



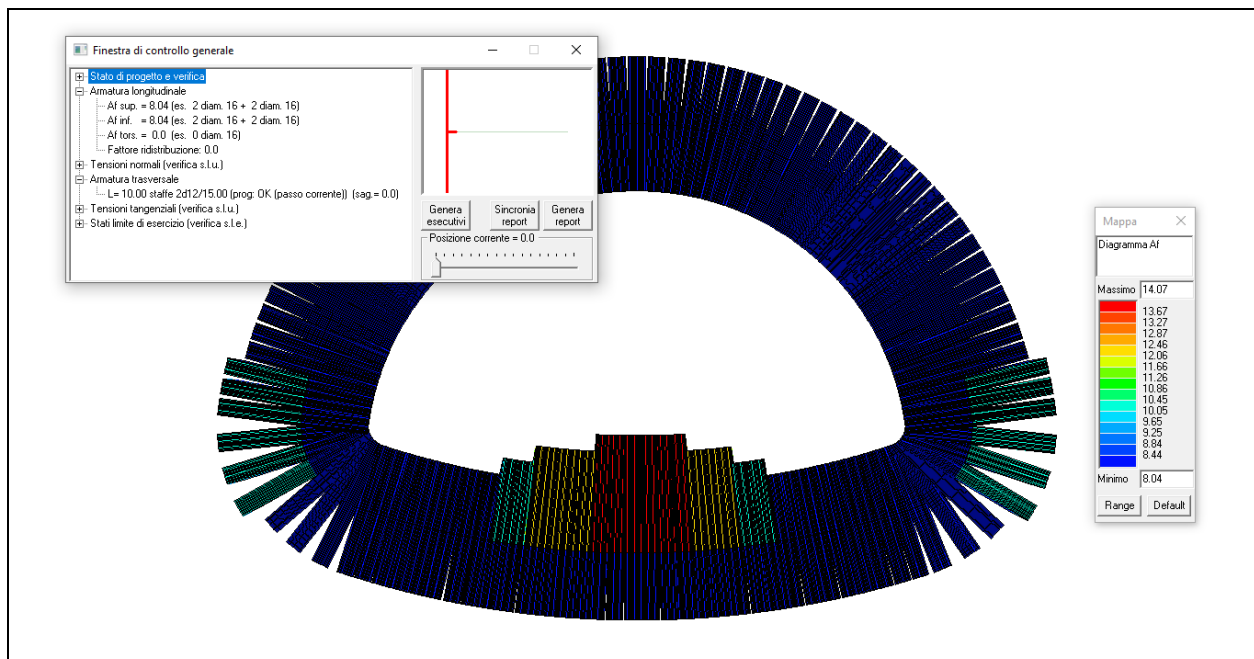


Figura 12: Armature calotta superiore

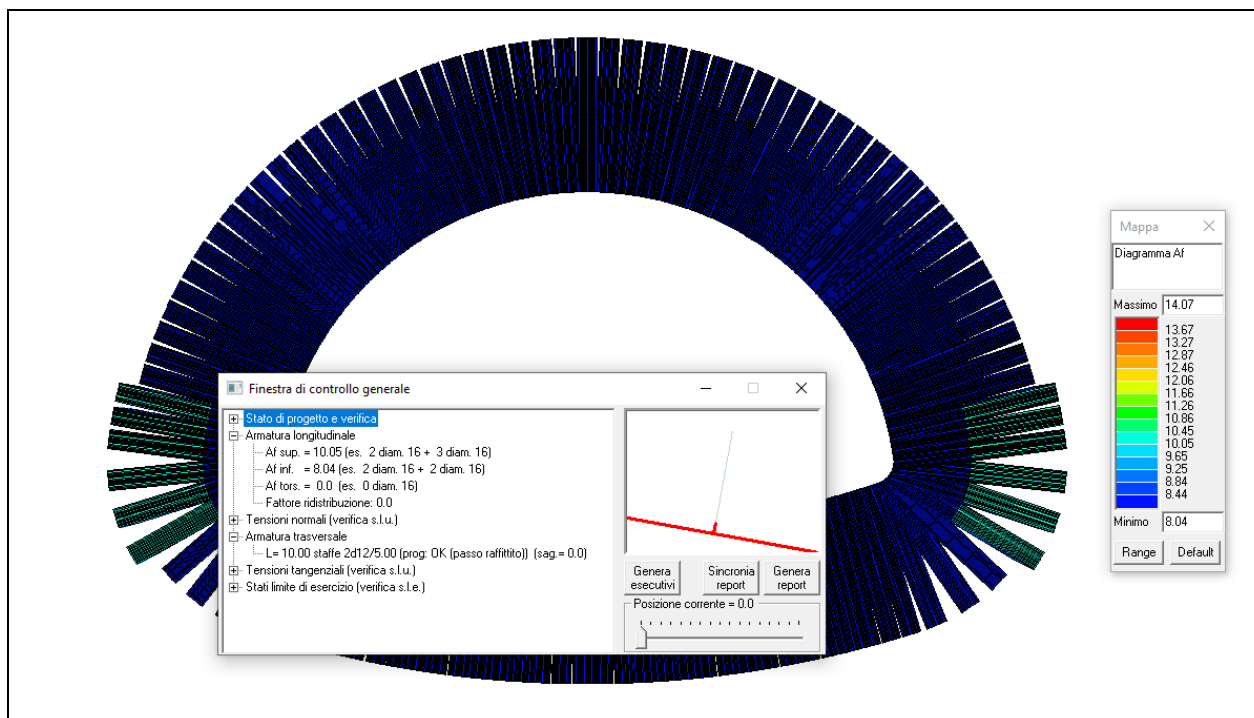


Figura 13: Armatura reni

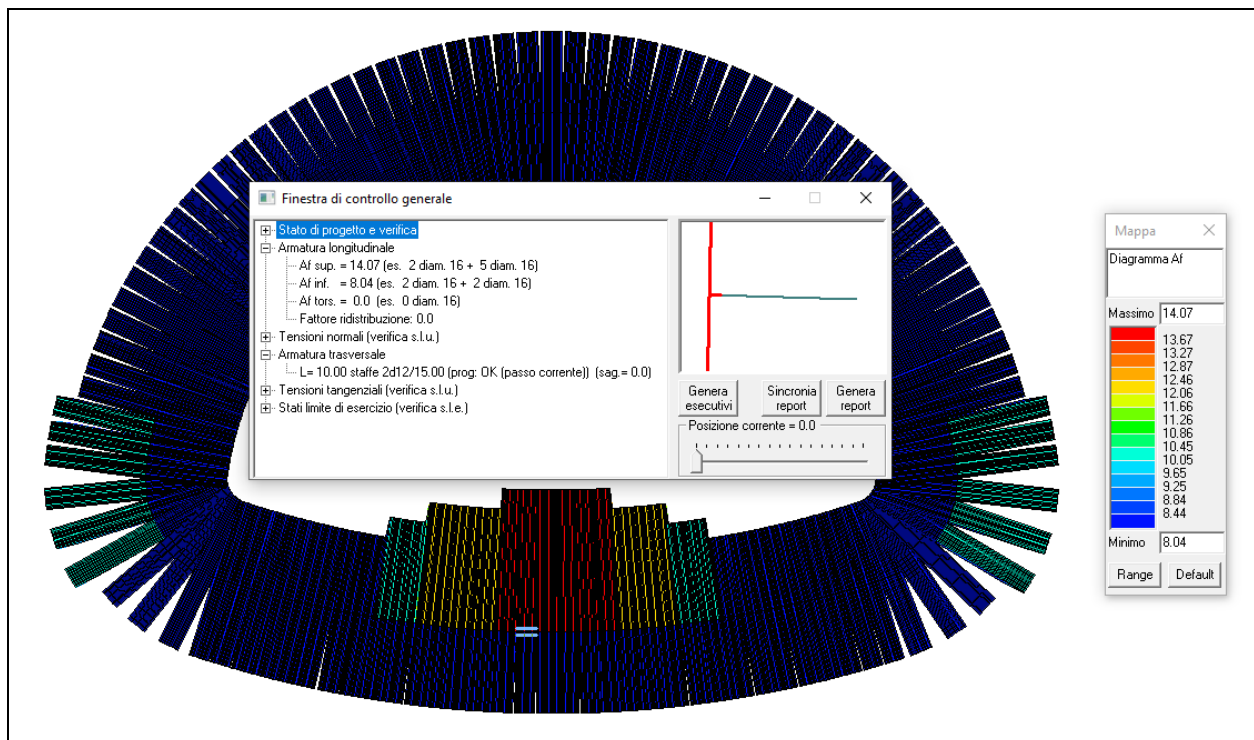


Figura 14: Armatura inferiore

Le staffe sono realizzate con i cavallotti 2 $\phi$ 12/15 per metro lineare di opera che pertanto vanno installati come indicato negli elaborati di progetto.



## **7.10 PROVE DI CONTROLLO FINALI**

Alla fine dei lavori, oltre alle normali verifiche e controlli previsti dalla vigente normativa, si dovranno prevedere controlli non distruttivi per accertare l'integrità e la continuità del guscio in calcestruzzo.

## **8. CONCLUSIONI**

A partire da quanto contenuto all'interno della presente relazione è possibile realizzare il relining del fonsider esistente utilizzando le più idonee tecniche costruttive presenti sul mercato.

Va comunque chiarito che tutte le informazioni qui contenute sono state dedotte dal progetto esecutivo dell'epoca e da informazioni presenti in letteratura.

Prima di eseguire l'intervento, l'impresa appaltatrice dovrà provvedere ad una verifica delle geometrie mediante un rilievo dello stato di fatto dell'intervento, da allegare a corredo della documentazione di progetto.

Relativamente la riduzione della sezione idraulica della tubazione è stata verificata la compatibilità idraulica da parte dello stesso Consorzio di Bonifica della Pianura di Ferrara.

**RIPRISTINO DELLA FUNZIONALITA' IDRAULICA DELLA CONDOTTA  
FINSIDER AMMALORATA COLLOCATA LUNGO IL CANALE NAVIGLIO  
IN LOCALITA' BAURA (FE)**

**PROGETTO ESECUTIVO**

**RELAZIONE DI CALCOLO**

**ALLEGATO A**

<b>Origine e Caratteristiche dei Codici di Calcolo</b>	
Codice di calcolo:	PRO_SAP PROfessional Structural Analysis Program
Versione:	PROFESSIONAL (build 2021-05-192)
Produttore- Distributore:	2S.I. Software e Servizi per l'Ingegneria s.r.l. Via Garibaldi, 90 44121 Ferrara FE ( Italy) Tel. +39 0532 200091 <a href="http://www.2si.it">www.2si.it</a>
Codice Licenza:	Licenza dsi5670

In merito al punto 10.2 delle Norme Tecniche per le Costruzioni (*Affidabilità dei codici utilizzati*), si fa riferimento al **Documento di Affidabilità** “Test di validazione del software di calcolo PRO\_SAP e dei moduli aggiuntivi PRO\_SAP Modulo Geotecnico, PRO\_CAD nodi acciaio e PRO\_MST” disponibile per il download sul sito: <https://www.2si.it/it/prodotti/affidabilita/>

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# CARATTERISTICHE MATERIALI UTILIZZATI

## LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale E
Poisson	coefficiente di contrazione trasversale $\nu$
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica
Fattore di confidenza FC m	Fattore di confidenza specifico per materiale; (è riportato solo se diverso da quello globale della struttura)
Fattore di confidenza FC a	Fattore di confidenza specifico per l'armatura (è riportato solo se diverso da quello globale della struttura)
Elasto-plastico	Materiale elastico perfettamente plastico per aste non lineari
Massima compressione	Massima tensione di compressione per aste non lineari
Massima trazione	Massima tensione di trazione per aste non lineari
Fattore attrito	Coefficiente di attrito per aste non lineari
Rapporto HRDb	Rapporto di hardening a flessione
Rapporto HRDv	Rapporto di hardening a taglio

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	cemento armato	Resistenza Rc	resistenza a compressione cubica
		Resistenza fctm	resistenza media a trazione semplice
		Coefficiente ksb	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
2	acciaio	Tensione ft	Valore della tensione di rottura
		Tensione fy	Valore della tensione di snervamento
		Resistenza fd	Resistenza di calcolo per SL CNR-UNI 10011

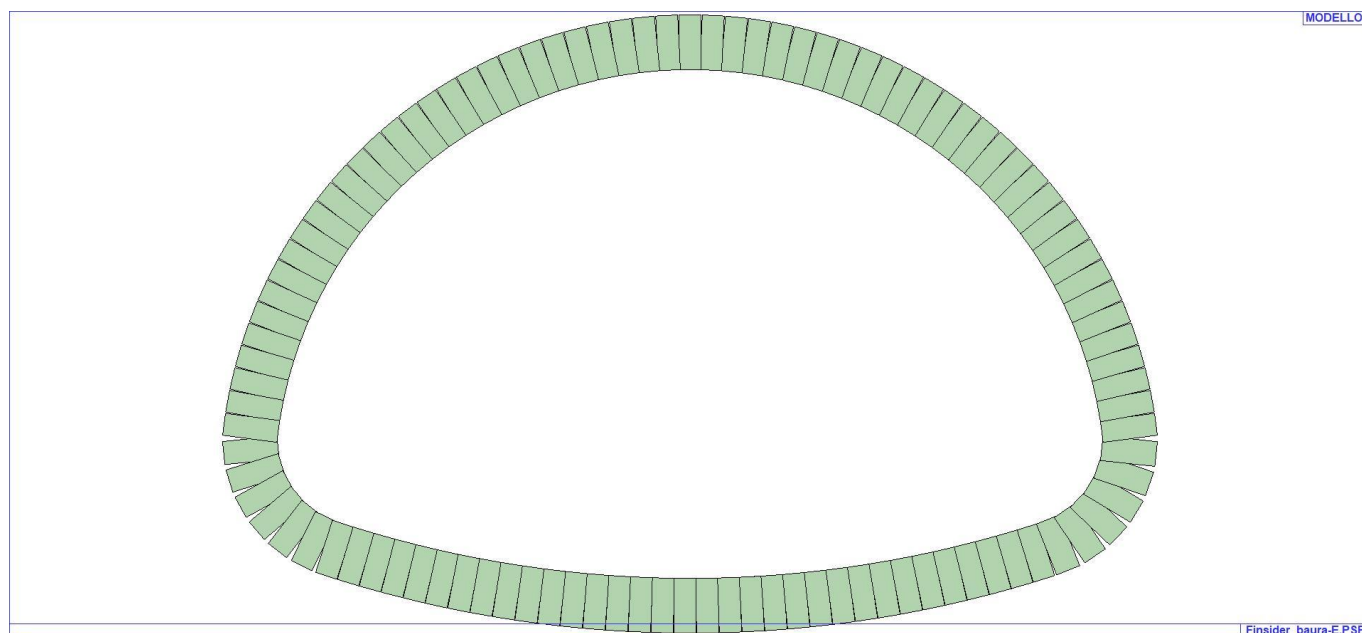
	Resistenza $f_d$ (>40)	Resistenza di calcolo per SL CNR-UNI 10011 per spessori > 40mm
	Tensione ammissibile	Tensione ammissibile CNR-UNI 10011
	Tensione ammissibile (>40)	Tensione ammissibile CNR-UNI 10011 per spessori > 40mm
3	muratura	
	Muratura consolidata	Muratura per la quale si prevedono interventi di rinforzo"
	Incremento resistenza	Incremento conseguito in termini di resistenza
	Incremento rigidezza	Incremento conseguito in termini di rigidezza
	Resistenza $f$	Valore della resistenza a compressione
	Resistenza $f_{v0}$	Valore della resistenza a taglio in assenza di tensioni normali
	Resistenza $f_h$	Valore della resistenza a compressione orizzontale
	Resistenza $f_b$	Valore della resistenza a compressione dei blocchi
	Resistenza $f_{bh}$	Valore della resistenza a compressione dei blocchi in direzione orizzontale
	Resistenza $f_{v0h}$	Valore della resistenza a taglio in assenza di tensioni normali per le travi
	Resistenza $f_t$	Valore della resistenza a trazione per fessurazione diagonale
	Resistenza $f_{vlim}$	Valore della massima resistenza a taglio
	Resistenza $f_{bt}$	Valore della resistenza a trazione dei blocchi
	Coefficiente $\mu$	Coefficiente d'attrito utilizzato per la resistenza a taglio (tipicamente 0.4)
	Coefficiente $f_i$	Coefficiente d'ingranamento utilizzato per la resistenza a taglio
	Coefficiente $k_{sb}$	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
4	legno	
	$E_{0,05}$	Modulo di elasticità corrispondente ad un frattile del 5%
	Resistenza $f_{c0}$	Valore della resistenza a compressione parallela
	Resistenza $f_{t0}$	Valore della resistenza a trazione parallela
	Resistenza $f_m$	Valore della resistenza a flessione
	Resistenza $f_v$	Valore della resistenza a taglio
	Resist. $f_{t0k}$	Resistenza caratteristica (tensione amm. per REGLES) per trazione

Resist. fmk	Resistenza caratteristica (tensione amm. per REGLES) per flessione
Resist. fvk	Resistenza caratteristica (tensione amm. per REGLES) per taglio
Modulo E0,05	Modulo elastico parallelo caratteristico
Lamellare	lamellare o massiccio

Nel tabulato si riportano sia i valori caratteristici che medi utilizzando gli uni e/o gli altri in relazione alle richieste di normativa ed alla tipologia di verifica. (Cap.7 NTC18 per materiali nuovi, Cap.8 NTC18 e relativa circolare 21/01/2019 per materiali esistenti, Linee Guida Reluis per incamiciatura CAM, CNR-DT 200 per interventi con FRP)

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt.	V. medio	Young	Poisson	G	Gamma	Alfa	Altri
		daN/cm2	daN/cm2	daN/cm2		daN/cm2	daN/cm3		
4	Calcestruzzo Classe C32/40			3.360e+05	0.20	1.400e+05	2.50e-03	1.00e-05	
	Resistenza Rc	400.0							
	Resistenza fctm		31.0						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05



## 11\_MOD\_MATERIALI\_D2

Travi c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
<b>Generalità</b>						
Progetta a filo	NO	NO	NO			
Af inf: da q*L*L /	0.0	0.0	0.0			
<b>Armatura</b>						
Minima tesa	0.31	0.20	0.31			
Minima compressa	0.31	0.20	0.31			
Massima tesa	0.78	0.78	0.78			
Da sezione	SI	SI	SI			
Usa armatura teorica	NO	NO	NO			
<b>Stati limite ultimi</b>						



<b>Travi c.a.</b>	<b>1/7/..</b>	<b>2/8/..</b>	<b>3/9/..</b>	<b>4/10/..</b>	<b>5/11/..</b>	<b>6/12/..</b>
Tensione fy [daN/cm <sup>2</sup> ]	4500.00	4500.00	4500.00			
Tensione fy staffe [daN/cm <sup>2</sup> ]	4500.00	4500.00	4500.00			
Tipo acciaio	tipo C	tipo C	tipo C			
Coefficiente gamma s	1.15	1.15	1.15			
Coefficiente gamma c	1.50	1.50	1.50			
Verifiche con N costante	SI	SI	SI			
Fattore di ridistribuzione	0.0	0.0	0.0			
<b>Modello per il confinamento</b>						
Relazione tensio-deformativa	Mander	Mander	Mander			
Incrudimento acciaio	5.000e-03	5.000e-03	5.000e-03			
Fattore lambda	1.00	1.00	1.00			
epsilon max,s	4.000e-02	4.000e-02	4.000e-02			
epsilon cu2	4.500e-03	4.500e-03	4.500e-03			
epsilon c2	0.0	0.0	0.0			
epsilon cy	0.0	0.0	0.0			
<b>Tensioni ammissibili</b>						
Tensione amm. cls [daN/cm <sup>2</sup> ]	97.50	97.50	97.50			
Tensione amm. acciaio [daN/cm <sup>2</sup> ]	2600.00	2600.00	2600.00			
Rapporto omogeneizzazione N	15.00	15.00	15.00			
Massimo rapporto area compressa/tesa	1.00	1.00	1.00			
<b>Staffe</b>						
Diametro staffe	0.0	0.0	12.00			
Passo minimo [ cm ]	4.00	5.00	5.00			
Passo massimo [ cm ]	30.00	30.00	30.00			
Passo raffittito [ cm ]	15.00	15.00	20.00			
Lunghezza zona raffittita [ cm ]	50.00	50.00	50.00			
Ctg(Teta) Max	2.50	2.50	2.50			
Percentuale sagomati	0.0	0.0	0.0			
Luce di taglio per GR [ cm ]	1.00	1.00	1.00			
Adotta scorrimento medio	NO	NO	NO			
Torsione non essenziale inclusa	SI	SI	SI			

# MODELLAZIONE DELLE SEZIONI

## LEGENDA TABELLA DATI SEZIONI

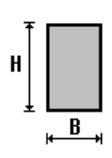
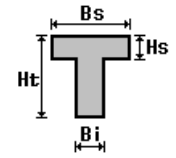
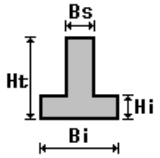
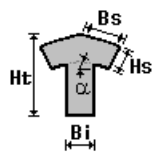
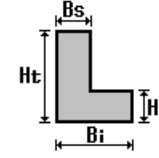
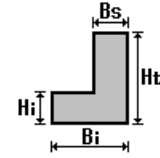
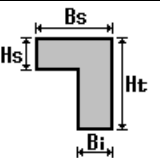
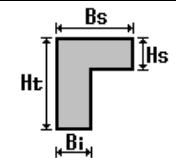
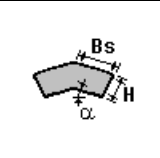
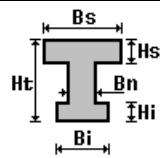
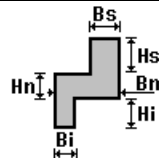
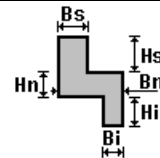
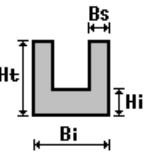
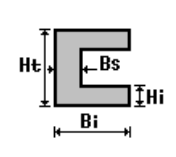
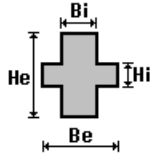
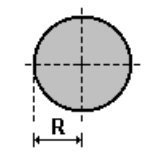
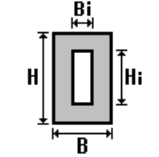
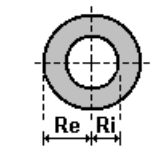
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

<b>Area</b>	area della sezione
<b>A V2</b>	area della sezione/fattore di taglio (per il taglio in direzione 2)
<b>A V3</b>	area della sezione/fattore di taglio (per il taglio in direzione 3)
<b>Jt</b>	fattore torsionale di rigidezza
<b>J2-2</b>	momento d'inerzia della sezione riferito all'asse 2
<b>J3-3</b>	momento d'inerzia della sezione riferito all'asse 3
<b>W2-2</b>	modulo di resistenza della sezione riferito all'asse 2
<b>W3-3</b>	modulo di resistenza della sezione riferito all'asse 3
<b>Wp2-2</b>	modulo di resistenza plastico della sezione riferito all'asse 2
<b>Wp3-3</b>	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

 rettangolare	 a T	 a T rovescia	 a T di colmo	 a L	 a L specchiata
 a L specchiata rovescia	 a L rovescia	 a L di colmo	 a doppio T	 a quattro specchiata	 a quattro
 a U	 a C	 a croce	 circolare	 rettangolare cava	 circolare cava

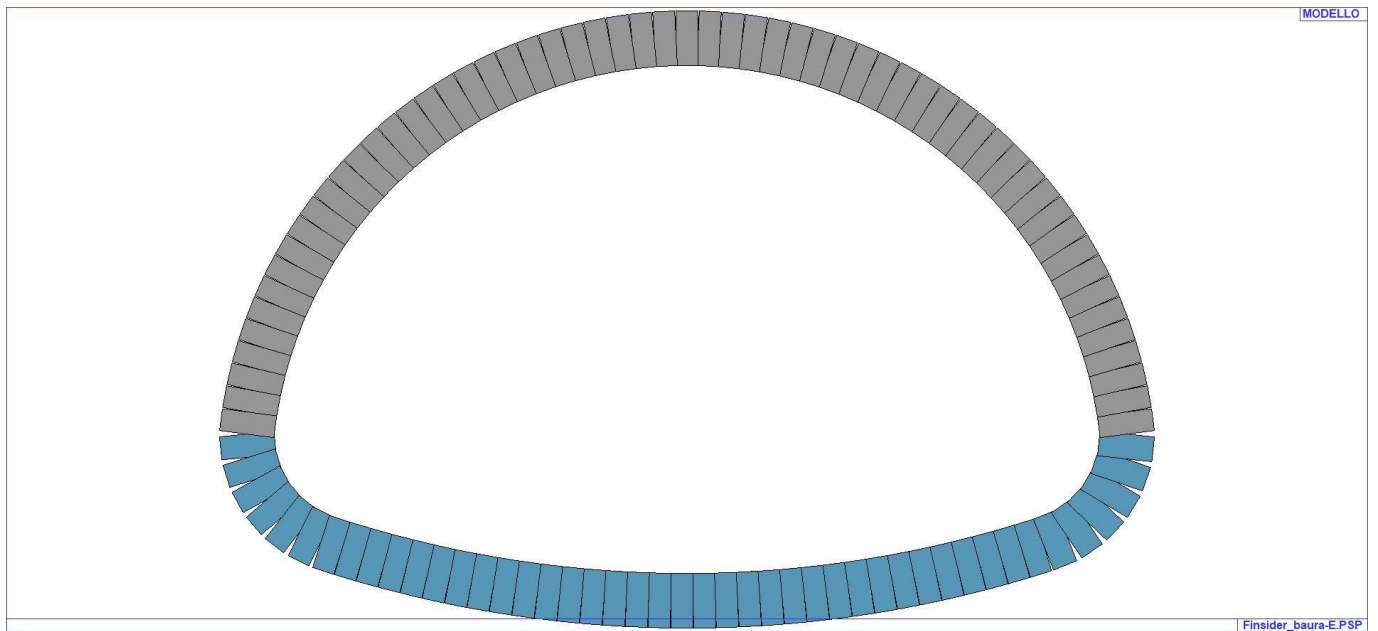
Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):

i valori dimensionali con prefisso B sono riferiti all'asse 2

i valori dimensionali con prefisso H sono riferiti all'asse 3

Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	ARCO SUP	2500.00	2083.33	2083.33	4.388e+05	2.083e+06	1.302e+05	4.167e+04	1.042e+04	6.250e+04	1.563e+04
2	ARCO INF	2500.00	2083.33	2083.33	4.388e+05	2.083e+06	1.302e+05	4.167e+04	1.042e+04	6.250e+04	1.563e+04



13\_MOD\_SEZIONI

Finsider\_baura-E.PSP

# MODELLAZIONE STRUTTURA: NODI

## LEGENDA TABELLA DATI NODI

Il programma utilizza per la modellazione nodi strutturali.

Ogni nodo è individuato dalle coordinate cartesiane nel sistema di riferimento globale (X Y Z).

Ad ogni nodo è eventualmente associato un codice di vincolamento rigido, un codice di fondazione speciale, ed un set di sei molle (tre per le traslazioni, tre per le rotazioni). Le tabelle sottoriportate riflettono le succitate possibilità. In particolare per ogni nodo viene indicato in tabella:

<b>Nodo</b>	numero del nodo.
<b>X</b>	valore della coordinata X
<b>Y</b>	valore della coordinata Y
<b>Z</b>	valore della coordinata Z

Per i nodi ai quali sia associato un codice di vincolamento rigido, un codice di fondazione speciale o un set di molle viene indicato in tabella:

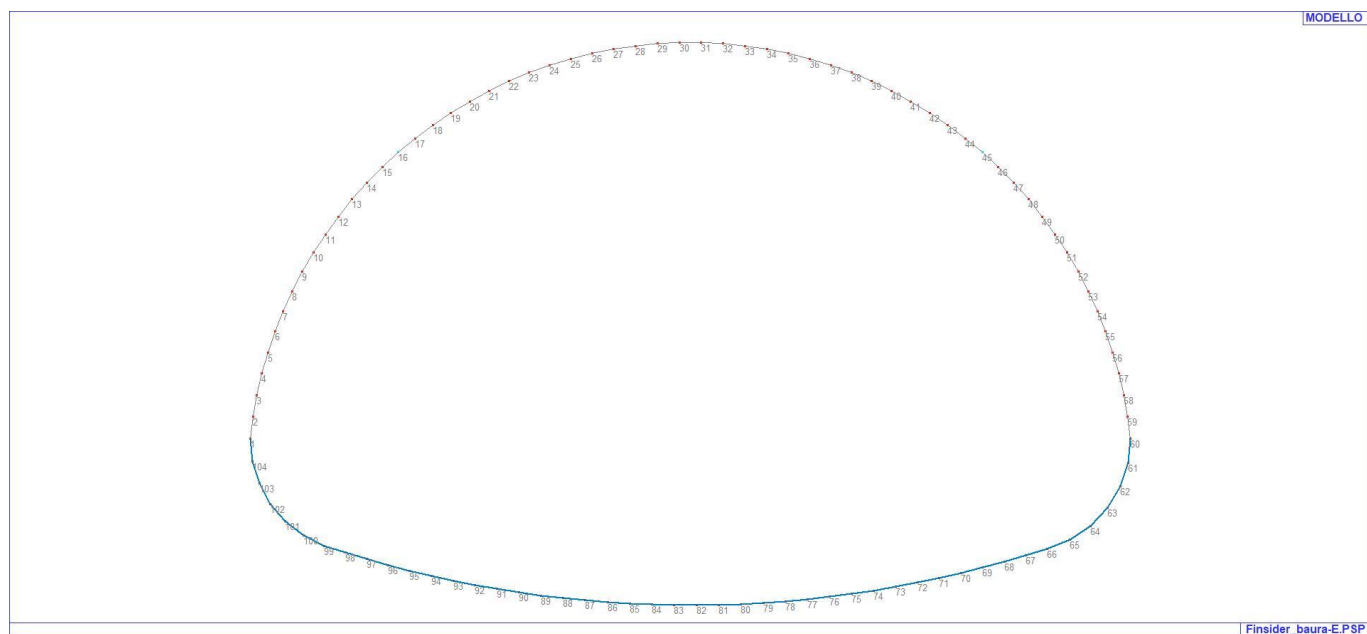
<b>Nodo</b>	numero del nodo.
<b>X</b>	valore della coordinata X
<b>Y</b>	valore della coordinata Y
<b>Z</b>	valore della coordinata Z
<b>Note</b>	eventuale codice di vincolo (es. v=110010 sei valori relativi ai sei gradi di libertà previsti per il nodo TxTyTzRxRyRz, il valore 1 indica che lo spostamento o rotazione relativo è impedito, il valore 0 indica che lo spostamento o rotazione relativo è libero).
<b>Note</b>	(FS = 1, 2,...) eventuale codice del tipo di fondazione speciale (1, 2,... fanno riferimento alle tipologie: plinto, palo, plinto su pali,...) che è collegato al nodo. (ISO = "id SIGLA") indice e sigla identificativa dell' eventuale isolatore sismico assegnato al nodo
<b>Rig. TX</b>	valore della rigidezza dei vincoli elastici eventualmente applicati al nodo, nello specifico TX (idem per TY, TZ, RX, RY, RZ).

Per strutture sismicamente isolate viene inoltre inserita la tabella delle caratteristiche per gli isolatori utilizzati; le caratteristiche sono indicate in conformità al cap. 7.10 del D.M. 14/01/08

## TABELLA DATI NODI

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
	cm	cm	cm		cm	cm	cm		cm	cm	cm
1	-4.1	0.0	276.2	2	-2.7	0.0	286.1	3	-0.9	0.0	296.0
4	1.4	0.0	305.8	5	4.1	0.0	315.4	6	7.4	0.0	324.9
7	11.1	0.0	334.3	8	15.3	0.0	343.4	9	19.9	0.0	352.3
10	25.0	0.0	361.0	11	30.5	0.0	369.4	12	36.4	0.0	377.6
13	42.6	0.0	385.4	14	49.3	0.0	392.9	15	56.4	0.0	400.1
16	63.7	0.0	406.9	17	71.5	0.0	413.3	18	79.5	0.0	419.4
19	87.8	0.0	425.0	20	96.4	0.0	430.2	21	105.2	0.0	435.0
22	114.3	0.0	439.3	23	123.5	0.0	443.2	24	133.0	0.0	446.6
25	142.6	0.0	449.6	26	152.3	0.0	452.1	27	162.2	0.0	454.0
28	172.1	0.0	455.5	29	182.1	0.0	456.5	30	192.2	0.0	457.0
31	202.2	0.0	457.0	32	212.2	0.0	456.5	33	222.2	0.0	455.5
34	232.2	0.0	454.0	35	242.0	0.0	452.1	36	251.8	0.0	449.6
37	261.4	0.0	446.6	38	270.8	0.0	443.2	39	280.1	0.0	439.3
40	289.1	0.0	435.0	41	298.0	0.0	430.2	42	306.6	0.0	425.0
43	314.9	0.0	419.4	44	322.9	0.0	413.3	45	330.6	0.0	406.9
46	338.0	0.0	400.1	47	345.0	0.0	392.9	48	351.7	0.0	385.4
49	358.0	0.0	377.6	50	363.9	0.0	369.4	51	369.4	0.0	361.0
52	374.5	0.0	352.3	53	379.1	0.0	343.4	54	383.3	0.0	334.3

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
55	387.0	0.0	324.9	56	390.2	0.0	315.4	57	393.0	0.0	305.8
58	395.3	0.0	296.0	59	397.1	0.0	286.1	60	398.4	0.0	276.2
61	397.2	0.0	264.9	62	393.6	0.0	254.2	63	387.8	0.0	244.5
64	380.0	0.0	236.2	65	370.6	0.0	229.9	66	360.1	0.0	225.7
67	350.4	0.0	222.6	68	340.7	0.0	219.8	69	330.8	0.0	217.1
70	321.0	0.0	214.6	71	311.0	0.0	212.4	72	301.1	0.0	210.3
73	291.1	0.0	208.4	74	281.1	0.0	206.7	75	271.0	0.0	205.2
76	260.9	0.0	203.8	77	250.8	0.0	202.7	78	240.7	0.0	201.8
79	230.5	0.0	201.0	80	220.3	0.0	200.5	81	210.2	0.0	200.2
82	200.0	0.0	200.0	83	189.8	0.0	200.0	84	179.7	0.0	200.3
85	169.5	0.0	200.7	86	159.3	0.0	201.3	87	149.2	0.0	202.2
88	139.1	0.0	203.2	89	129.0	0.0	204.4	90	118.9	0.0	205.8
91	108.8	0.0	207.4	92	98.8	0.0	209.2	93	88.8	0.0	211.1
94	78.9	0.0	213.4	95	69.0	0.0	215.7	96	59.1	0.0	218.3
97	49.3	0.0	221.0	98	39.6	0.0	224.0	99	29.9	0.0	227.1
100	20.5	0.0	231.8	101	12.1	0.0	238.3	102	5.3	0.0	246.3
103	0.2	0.0	255.6	104	-3.0	0.0	265.6				



14\_MOD\_NUMERAZIONE\_NODI

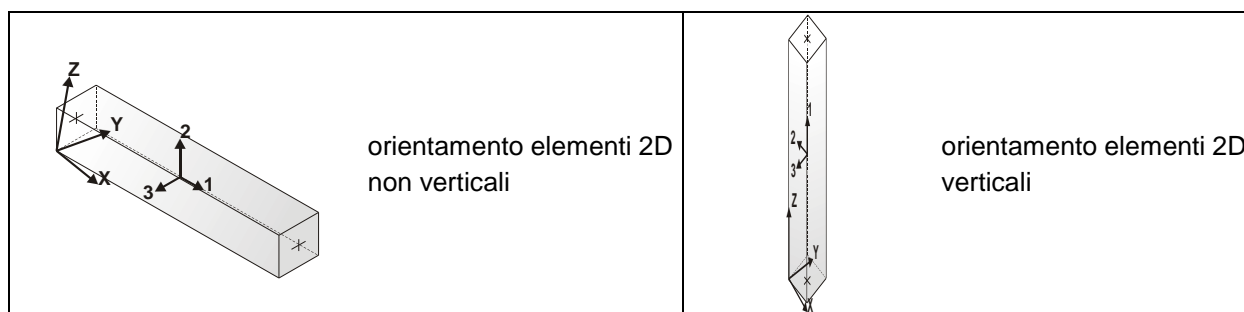
# MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

## TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.

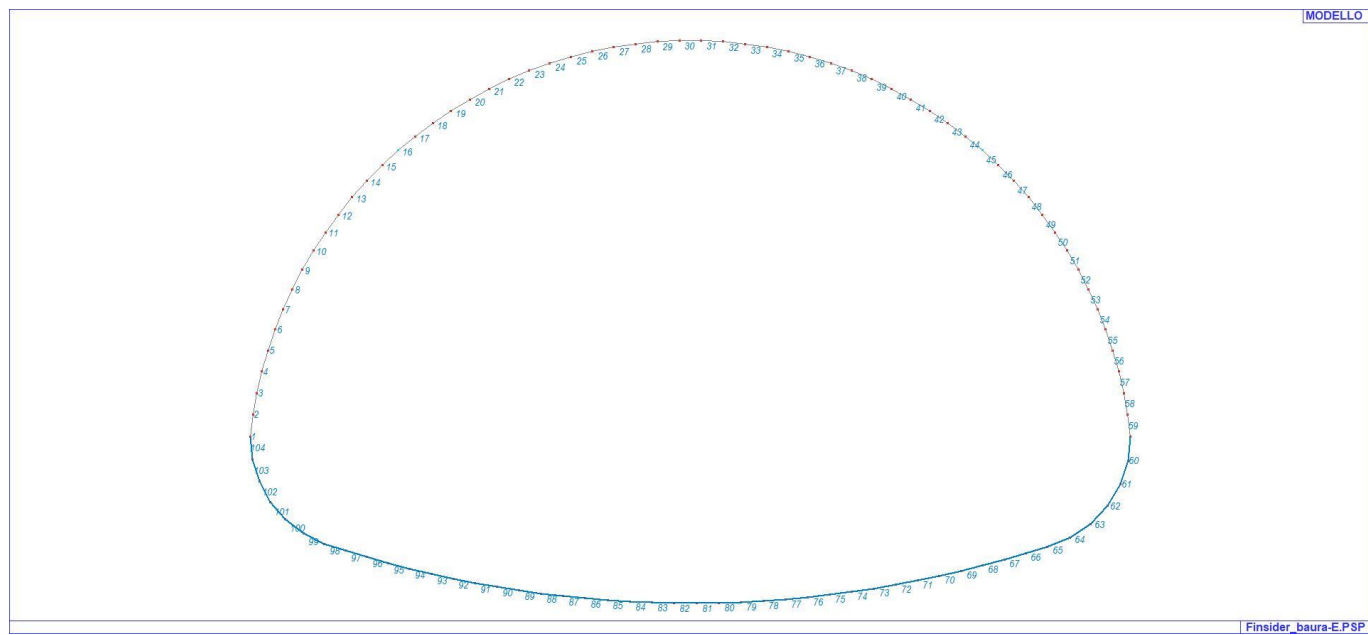


In particolare per ogni elemento viene indicato in tabella:

<b>Elem.</b>	numero dell'elemento
<b>Note</b>	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
<b>Nodo I (J)</b>	numero del nodo iniziale (finale)
<b>Mat.</b>	codice del materiale assegnato all'elemento
<b>Sez.</b>	codice della sezione assegnata all'elemento
<b>Rotaz.</b>	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
<b>Svincolo I (J)</b>	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
<b>Wink V</b>	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
<b>Wink O</b>	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

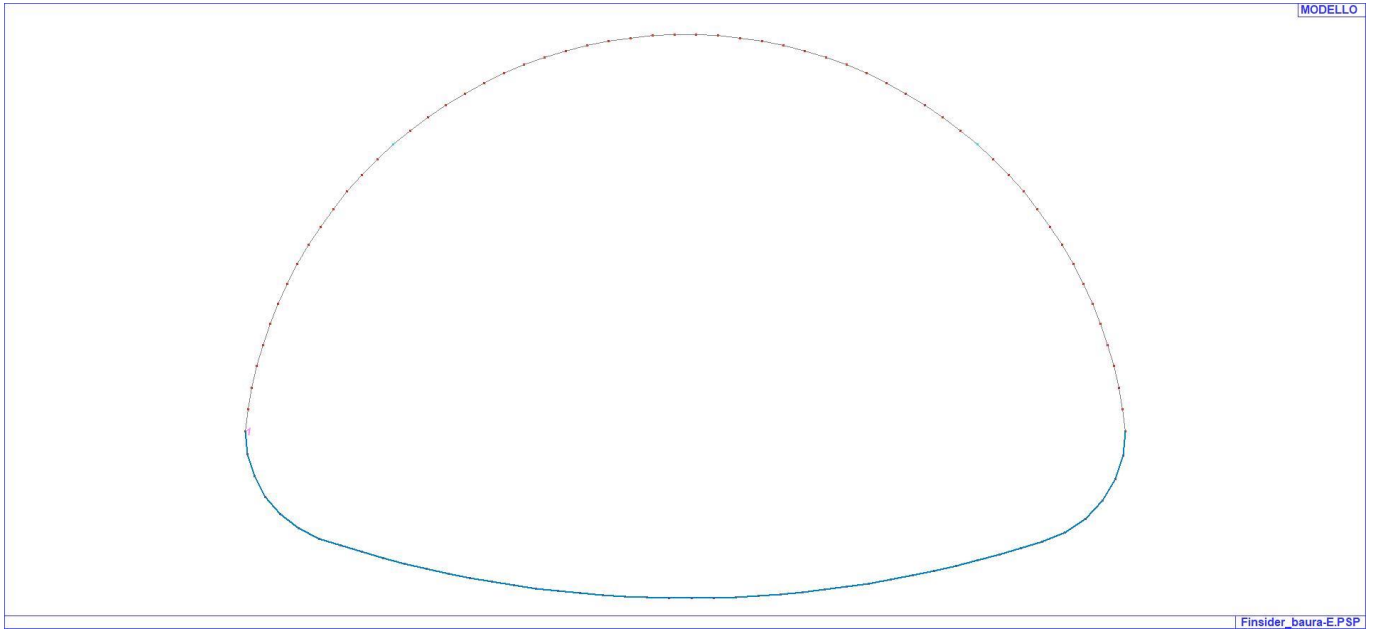
Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz.	Svincolo I	Svincolo J	Wink V	Wink O
							gradi			daN/cm3	daN/cm3
1	Trave	1	2	4	1	3					
2	Trave	2	3	4	1	3					
3	Trave	3	4	4	1	3					
4	Trave	4	5	4	1	3					
5	Trave	5	6	4	1	3					
6	Trave	6	7	4	1	3					
7	Trave	7	8	4	1	3					
8	Trave	8	9	4	1	3					
9	Trave	9	10	4	1	3					
10	Trave	10	11	4	1	3					
11	Trave	11	12	4	1	3					
12	Trave	12	13	4	1	3					
13	Trave	13	14	4	1	3					
14	Trave	14	15	4	1	3					
15	Trave	15	16	4	1	3					
16	Trave	16	17	4	1	3					
17	Trave	17	18	4	1	3					
18	Trave	18	19	4	1	3					
19	Trave	19	20	4	1	3					
20	Trave	20	21	4	1	3					
21	Trave	21	22	4	1	3					
22	Trave	22	23	4	1	3					
23	Trave	23	24	4	1	3					
24	Trave	24	25	4	1	3					
25	Trave	25	26	4	1	3					
26	Trave	26	27	4	1	3					
27	Trave	27	28	4	1	3					
28	Trave	28	29	4	1	3					
29	Trave	29	30	4	1	3					
30	Trave	30	31	4	1	3					
31	Trave	31	32	4	1	3					
32	Trave	32	33	4	1	3					
33	Trave	33	34	4	1	3					
34	Trave	34	35	4	1	3					
35	Trave	35	36	4	1	3					
36	Trave	36	37	4	1	3					
37	Trave	37	38	4	1	3					
38	Trave	38	39	4	1	3					
39	Trave	39	40	4	1	3					
40	Trave	40	41	4	1	3					
41	Trave	41	42	4	1	3					
42	Trave	42	43	4	1	3					
43	Trave	43	44	4	1	3					
44	Trave	44	45	4	1	3					
45	Trave	45	46	4	1	3					
46	Trave	46	47	4	1	3					
47	Trave	47	48	4	1	3					
48	Trave	48	49	4	1	3					
49	Trave	49	50	4	1	3					
50	Trave	50	51	4	1	3					
51	Trave	51	52	4	1	3					
52	Trave	52	53	4	1	3					
53	Trave	53	54	4	1	3					
54	Trave	54	55	4	1	3					
55	Trave	55	56	4	1	3					
56	Trave	56	57	4	1	3					
57	Trave	57	58	4	1	3					
58	Trave	58	59	4	1	3					
59	Trave	59	60	4	1	3					
60	Trave f.	61	60	4	2	3				0.21	1.00
61	Trave f.	62	61	4	2	3				0.21	1.00
62	Trave f.	63	62	4	2	3				0.21	1.00
63	Trave f.	64	63	4	2	3				0.21	1.00
64	Trave f.	65	64	4	2	3				0.21	1.00
65	Trave f.	66	65	4	2	3				0.21	1.00
66	Trave f.	67	66	4	2	3				0.21	1.00
67	Trave f.	68	67	4	2	3				0.21	1.00
68	Trave f.	69	68	4	2	3				0.21	1.00
69	Trave f.	70	69	4	2	3				0.21	1.00
70	Trave f.	71	70	4	2	3				0.21	1.00

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz.	Svincolo I	Svincolo J	Wink V	Wink O
71	Trave f.	72	71	4	2	3				0.21	1.00
72	Trave f.	73	72	4	2	3				0.21	1.00
73	Trave f.	74	73	4	2	3				0.21	1.00
74	Trave f.	75	74	4	2	3				0.21	1.00
75	Trave f.	76	75	4	2	3				0.21	1.00
76	Trave f.	77	76	4	2	3				0.21	1.00
77	Trave f.	78	77	4	2	3				0.21	1.00
78	Trave f.	79	78	4	2	3				0.21	1.00
79	Trave f.	80	79	4	2	3				0.21	1.00
80	Trave f.	81	80	4	2	3				0.21	1.00
81	Trave f.	82	81	4	2	3				0.21	1.00
82	Trave f.	83	82	4	2	3				0.21	1.00
83	Trave f.	84	83	4	2	3				0.21	1.00
84	Trave f.	85	84	4	2	3				0.21	1.00
85	Trave f.	86	85	4	2	3				0.21	1.00
86	Trave f.	87	86	4	2	3				0.21	1.00
87	Trave f.	88	87	4	2	3				0.21	1.00
88	Trave f.	89	88	4	2	3				0.21	1.00
89	Trave f.	90	89	4	2	3				0.21	1.00
90	Trave f.	91	90	4	2	3				0.21	1.00
91	Trave f.	92	91	4	2	3				0.21	1.00
92	Trave f.	93	92	4	2	3				0.21	1.00
93	Trave f.	94	93	4	2	3				0.21	1.00
94	Trave f.	95	94	4	2	3				0.21	1.00
95	Trave f.	96	95	4	2	3				0.21	1.00
96	Trave f.	97	96	4	2	3				0.21	1.00
97	Trave f.	98	97	4	2	3				0.21	1.00
98	Trave f.	99	98	4	2	3				0.21	1.00
99	Trave f.	100	99	4	2	3				0.21	1.00
100	Trave f.	101	100	4	2	3				0.21	1.00
101	Trave f.	102	101	4	2	3				0.21	1.00
102	Trave f.	103	102	4	2	3				0.21	1.00
103	Trave f.	104	103	4	2	3				0.21	1.00
104	Trave f.	1	104	4	2	3				0.21	1.00



15\_MOD\_NUMERAZIONE\_D2





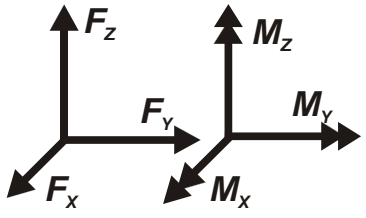
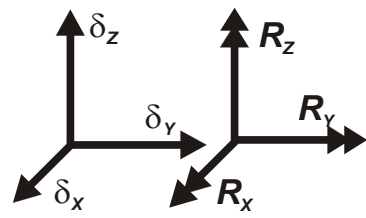
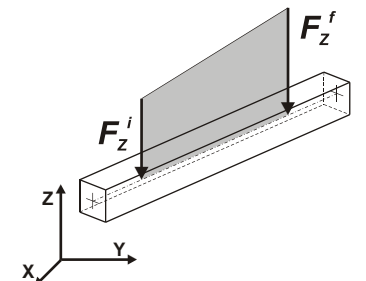
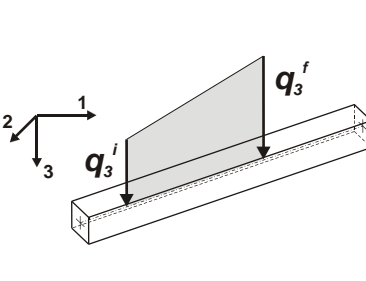
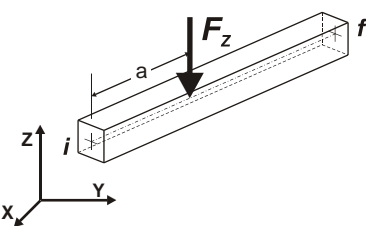
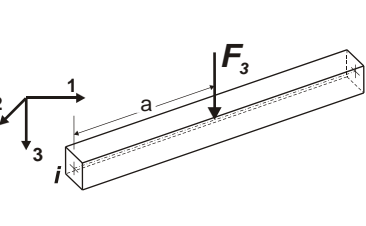
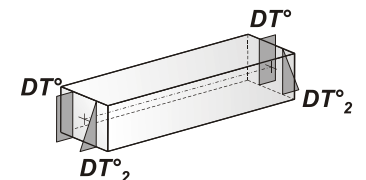
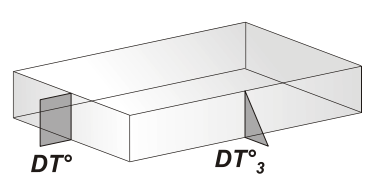
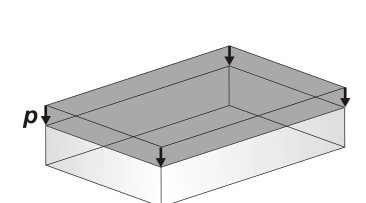
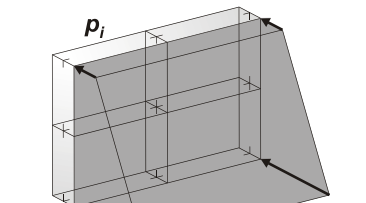
15\_MOD\_NUMERAZIONE\_D2\_TRAVATE

# MODELLAZIONE DELLE AZIONI

## LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

<b>1</b>	<b>carico concentrato nodale</b> 6 dati (forza $F_x$ , $F_y$ , $F_z$ , momento $M_x$ , $M_y$ , $M_z$ )
<b>2</b>	<b>spostamento nodale impresso</b> 6 dati (spostamento $T_x$ , $T_y$ , $T_z$ , rotazione $R_x$ , $R_y$ , $R_z$ )
<b>3</b>	<b>carico distribuito globale su elemento tipo trave</b> 7 dati ( $f_x$ , $f_y$ , $f_z$ , $m_x$ , $m_y$ , $m_z$ , ascissa di inizio carico) 7 dati ( $f_x$ , $f_y$ , $f_z$ , $m_x$ , $m_y$ , $m_z$ , ascissa di fine carico)
<b>4</b>	<b>carico distribuito locale su elemento tipo trave</b> 7 dati ( $f_1$ , $f_2$ , $f_3$ , $m_1$ , $m_2$ , $m_3$ , ascissa di inizio carico) 7 dati ( $f_1$ , $f_2$ , $f_3$ , $m_1$ , $m_2$ , $m_3$ , ascissa di fine carico)
<b>5</b>	<b>carico concentrato globale su elemento tipo trave</b> 7 dati ( $F_x$ , $F_y$ , $F_z$ , $M_x$ , $M_y$ , $M_z$ , ascissa di carico)
<b>6</b>	<b>carico concentrato locale su elemento tipo trave</b> 7 dati ( $F_1$ , $F_2$ , $F_3$ , $M_1$ , $M_2$ , $M_3$ , ascissa di carico)
<b>7</b>	<b>variazione termica applicata ad elemento tipo trave</b> 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
<b>8</b>	<b>carico di pressione uniforme su elemento tipo piastra</b> 1 dato (pressione)
<b>9</b>	<b>carico di pressione variabile su elemento tipo piastra</b> 4 dati (pressione, quota, pressione, quota)
<b>10</b>	<b>variazione termica applicata ad elemento tipo piastra</b> 2 dati (variazioni termiche: media e differenza nello spessore)
<b>11</b>	<b>carico variabile generale su elementi tipo trave e piastra</b> 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
<b>12</b>	<b>gruppo di carichi con impronta su piastra</b> 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

 <p>Carico concentrato nodale</p>	 <p>Spostamento impresso</p>
 <p>Carico distribuito globale</p>	 <p>Carico distribuito locale</p>
 <p>Carico concentrato globale</p>	 <p>Carico concentrato locale</p>
 <p>Carico termico 2D</p>	 <p>Carico termico 3D</p>
 <p>Carico pressione uniforme</p>	 <p>Carico pressione variabile</p>

**Tipo** carico distribuito globale su trave

Id	Tipo	Pos.	fx	fy	fz	mx	my	mz
		cm	daN/cm	daN/cm	daN/cm	daN	daN	daN
1	qik	0.0	0.0	0.0	-9.00	0.0	0.0	0.0
		0.0	0.0	0.0	-9.00	0.0	0.0	0.0
2	Qik tandem	0.0	0.0	0.0	-68.00	0.0	0.0	0.0
		0.0	0.0	0.0	-68.00	0.0	0.0	0.0
3	Peso terrapieno	0.0	0.0	0.0	-42.00	0.0	0.0	0.0
		0.0	0.0	0.0	-42.00	0.0	0.0	0.0
4	Acqua interna	0.0	0.0	0.0	-15.00	0.0	0.0	0.0
		0.0	0.0	0.0	-15.00	0.0	0.0	0.0
9	Sottospinta	0.0	0.0	0.0	45.70	0.0	0.0	0.0
		0.0	0.0	0.0	45.70	0.0	0.0	0.0

<b>Tipo</b>	<b>carico variabile generale</b>
-------------	----------------------------------

<b>Id</b>	<b>Tipo</b>	<b>ascissa</b>	<b>valore</b>	<b>ascissa</b>	<b>valore</b>
		cm	daN/cm2	cm	daN/cm2
5	Sterre Sx				
	Z - Z Qx Area L2=1.00	246.31	43.00	406.88	27.00
6	Sterre Dx				
	Z - Z Qx Area L2=1.00	246.31	-43.00	406.88	-27.00
7	Sw Sx				
	Z - Z Qx Area L2=1.00	246.31	40.00	406.88	25.00
8	Sw Dx				
	Z - Z Qx Area L2=1.00	246.31	-40.00	406.88	-25.00
10	Spinta traffico				
	Z - Z Qx Area L2=1.00	246.31	38.00	406.88	87.00
11	Sovraspinta sismica				
	Z - Z Qx Area L2=1.00	246.31	10.00	406.88	19.00

# SCHEMATIZZAZIONE DEI CASI DI CARICO

## LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	<b>Sigla</b>	<b>Tipo</b>	<b>Descrizione</b>
<b>1</b>	<b>Ggk</b>	A	caso di carico comprensivo del peso proprio struttura
<b>2</b>	<b>Gk</b>	NA	caso di carico con azioni permanenti
<b>3</b>	<b>Qk</b>	NA	caso di carico con azioni variabili
<b>4</b>	<b>Gsk</b>	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
<b>5</b>	<b>Qsk</b>	A	caso di carico comprensivo dei carichi variabili sui solai
<b>6</b>	<b>Qnk</b>	A	caso di carico comprensivo dei carichi di neve sulle coperture
<b>7</b>	<b>Qtk</b>	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
<b>8</b>	<b>Qvk</b>	NA	caso di carico comprensivo di azioni da vento sulla struttura
<b>9</b>	<b>Esk</b>	SA	caso di carico sismico con analisi statica equivalente
<b>10</b>	<b>Edk</b>	SA	caso di carico sismico con analisi dinamica
<b>11</b>	<b>Etk</b>	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
<b>12</b>	<b>Pk</b>	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

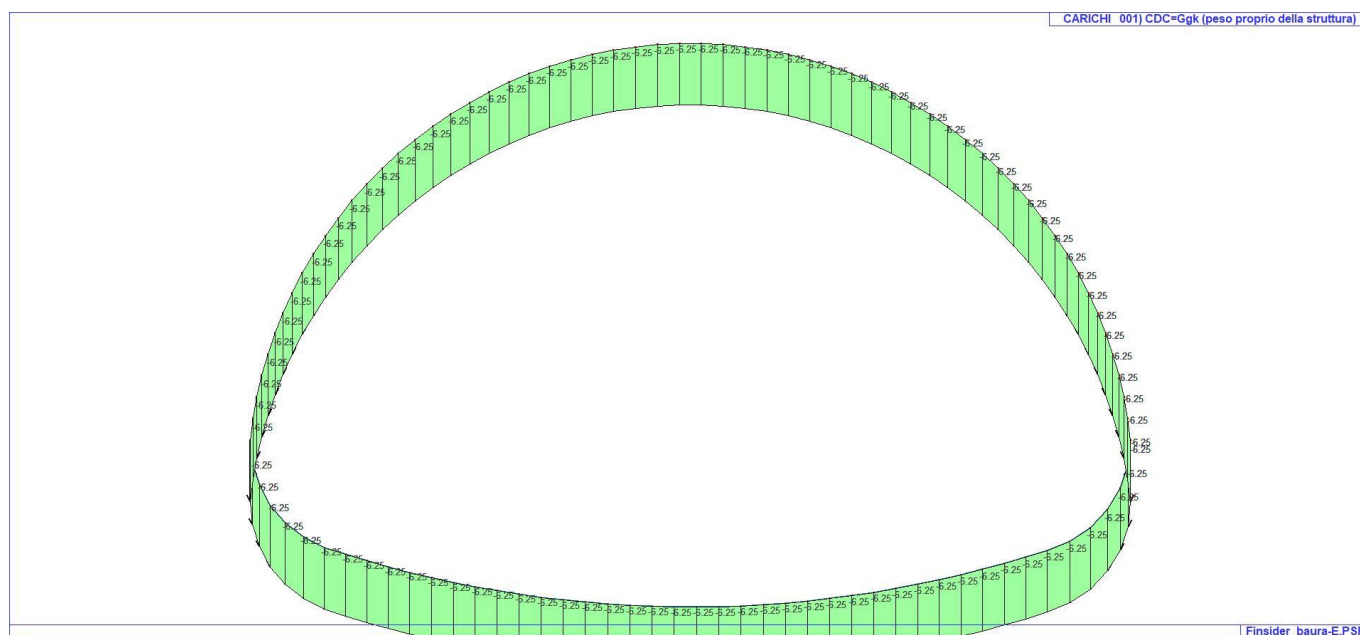
*Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).*

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

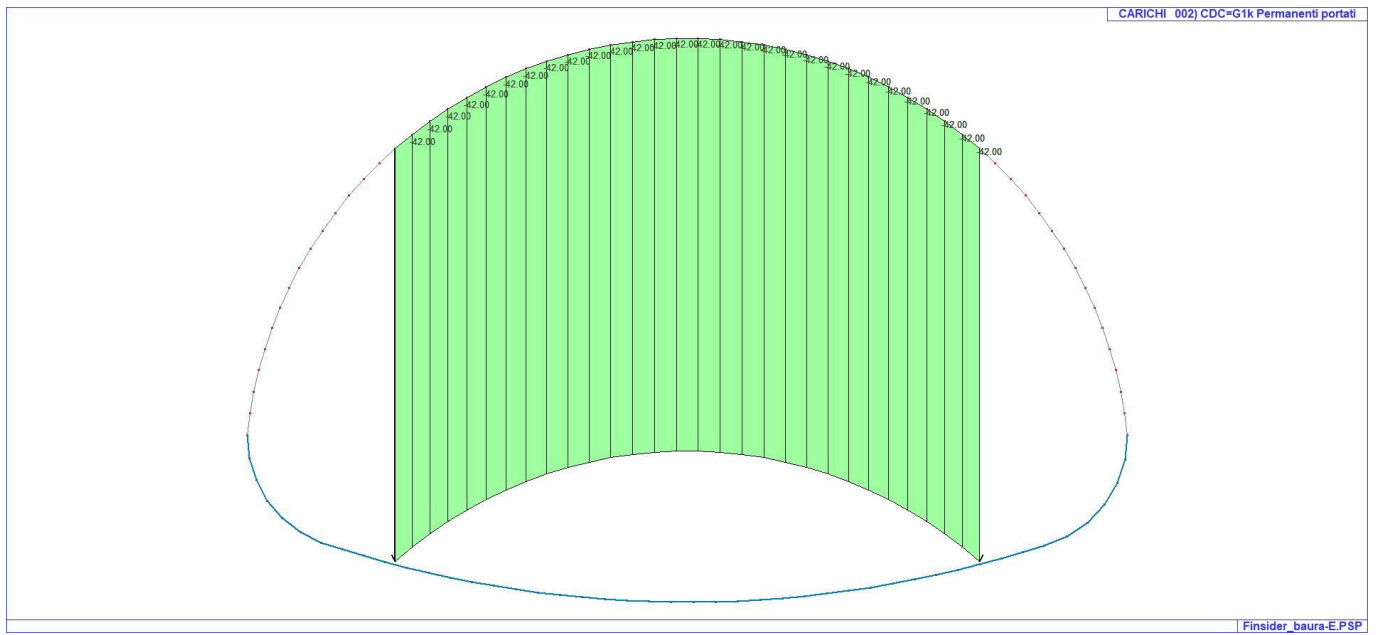
Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

<b>CDC</b>	<b>Tipo</b>	<b>Sigla Id</b>	<b>Note</b>
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gk	CDC=G1k Permanenti portati	Azioni applicate: D2 :da 16 a 44 Azione : Peso terrapieno
3	Gk	CDC=G1k Spinta a riposo	Azioni applicate: D2 :da 1 a 15 Azione : Sterre Sx D2 :da 45 a 62 Azione : Sterre Dx

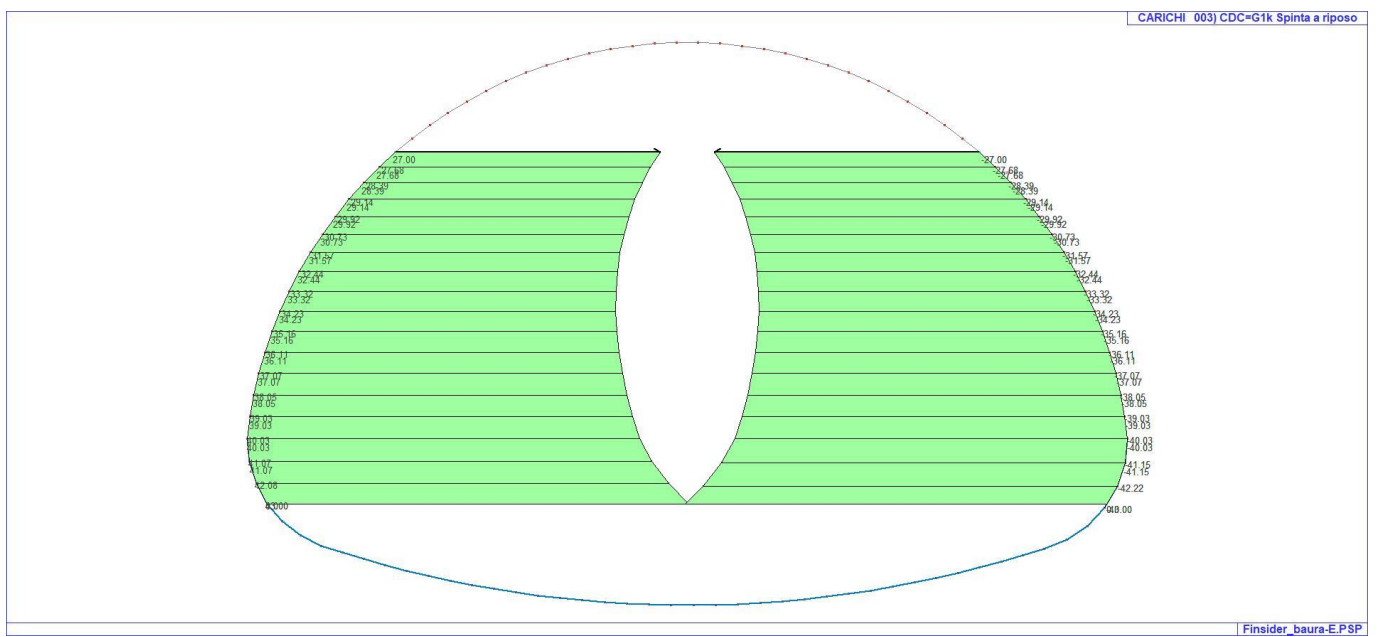
CDC	Tipo	Sigla Id	Note
			D2 :da 102 a 104 Azione : Sterre Sx
4	Gk	CDC=G1k Acqua interna	Azioni applicate:
			D2 :da 63 a 101 Azione : Acqua interna
5	Gk	CDC=G1k Spinta idraulica/sottospinta	Azioni applicate:
			D2 :da 1 a 15 Azione : Sw Sx
			D2 :da 45 a 62 Azione : Sw Dx
			D2 :da 63 a 101 Azione : Sottospinta
			D2 :da 102 a 104 Azione : Sw Sx
6	Qk	CDC=Qk carico stradale q1k	Azioni applicate:
			D2 :da 16 a 44 Azione : qik
7	Qk	CDC=Qk carico stradale Q1k	Azioni applicate:
			D2 :da 16 a 44 Azione : Qik tandem
8	Qk	CDC=Qk Spinta traffico	Azioni applicate:
			D2 :da 1 a 15 Azione : Spinta traffico
			D2 :da 102 a 104 Azione : Spinta traffico
9	Esk	CDC=Es (statico SLU) alfa=0.0 (ecc. 0)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:0.80 per 10 CDC=Qk Spinta sismica
10	Qk	CDC=Qk Spinta sismica	Azioni applicate:
			D2 :da 1 a 15 Azione : Sovraspinta sismica
			D2 :da 102 a 104 Azione : Sovraspinta sismica



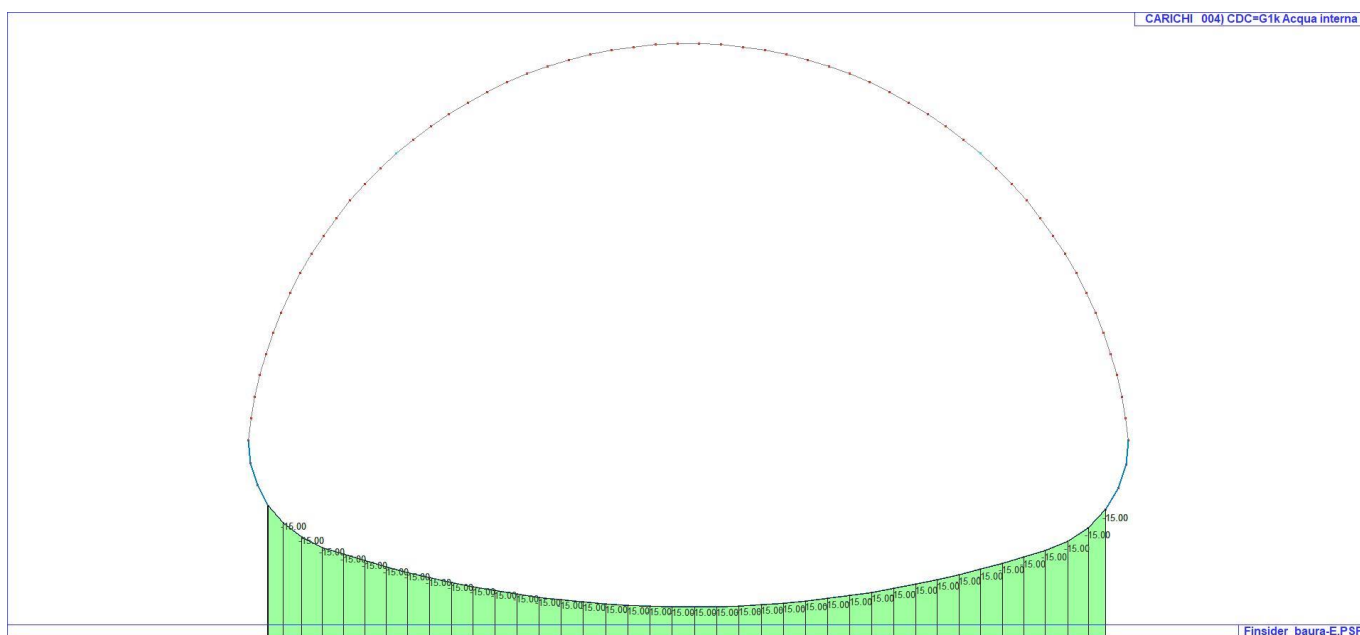
22\_CDC\_001\_CDC=Ggk (peso proprio della struttura)



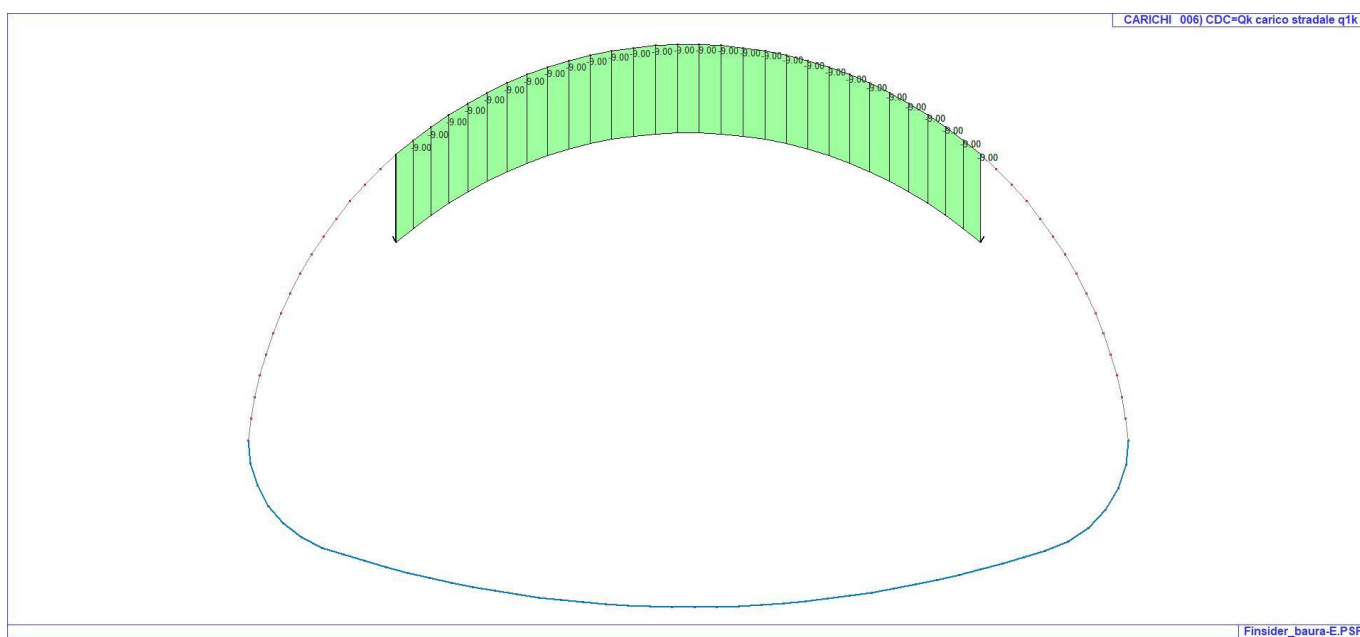
22\_CDC\_002\_CDC=G1k Permanenti portati



22\_CDC\_003\_CDC=G1k Spinta a riposo

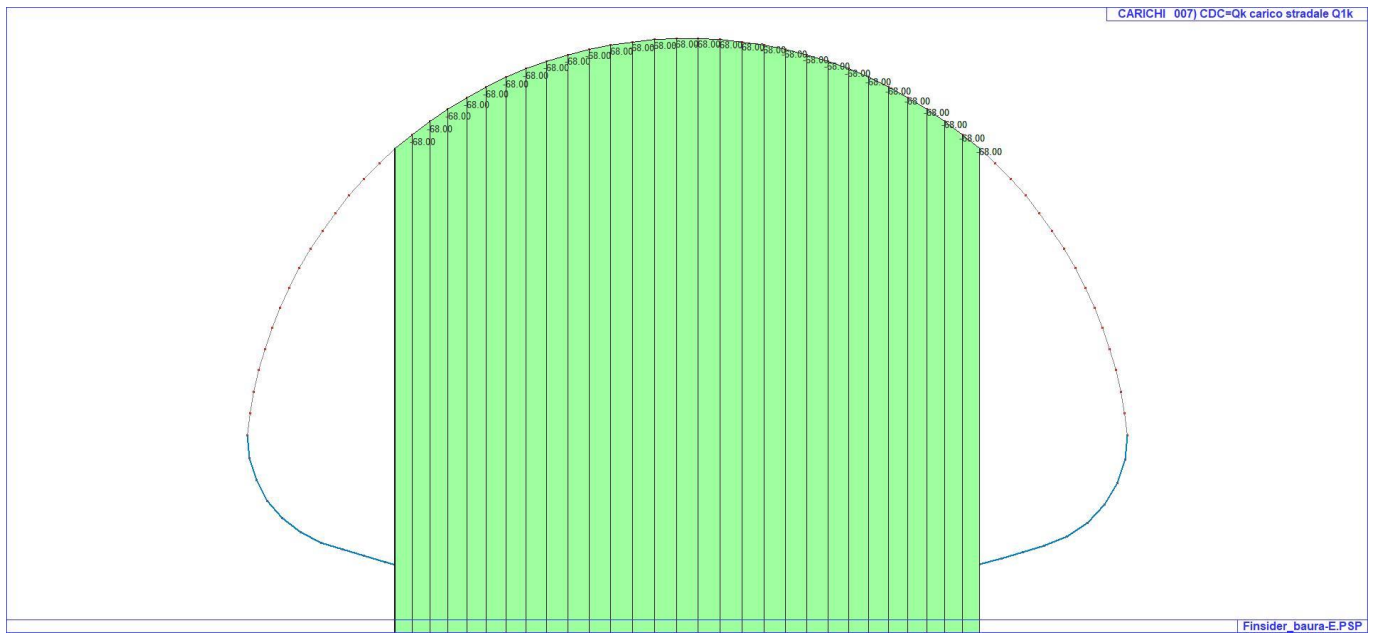


22\_CDC\_004\_CDC=G1k Acqua interna

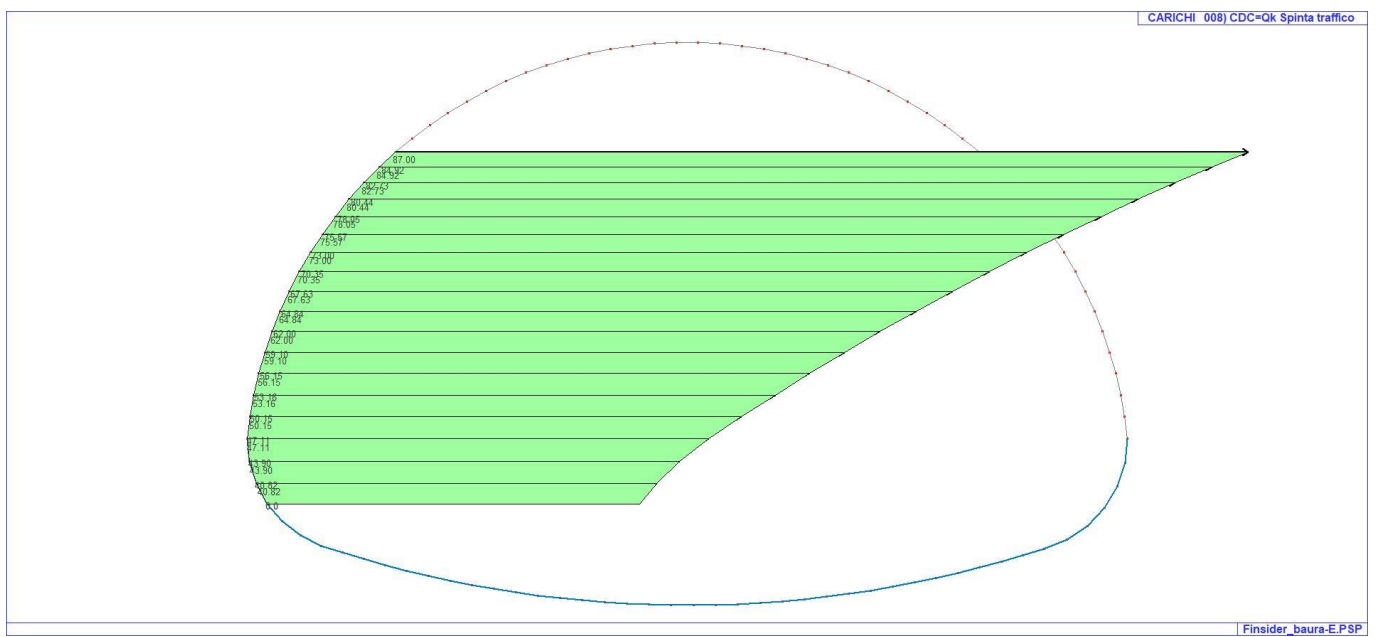


22\_CDC\_006\_CDC=Qk carico stradale q1k

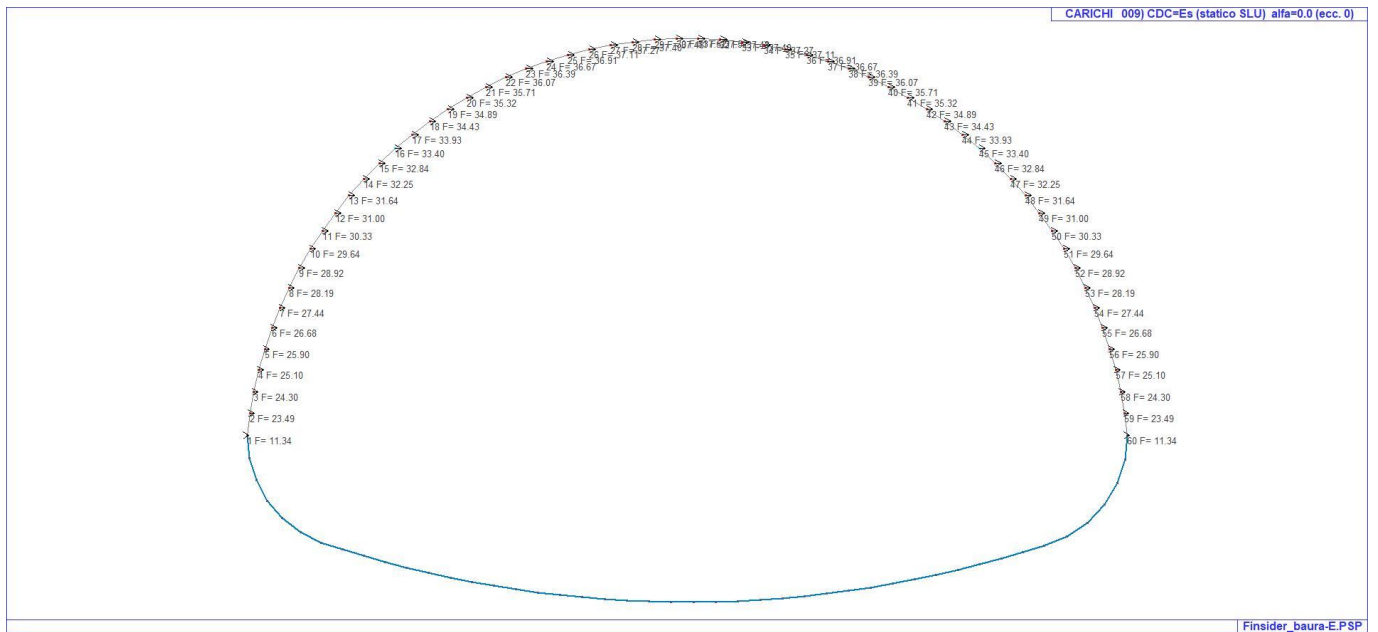




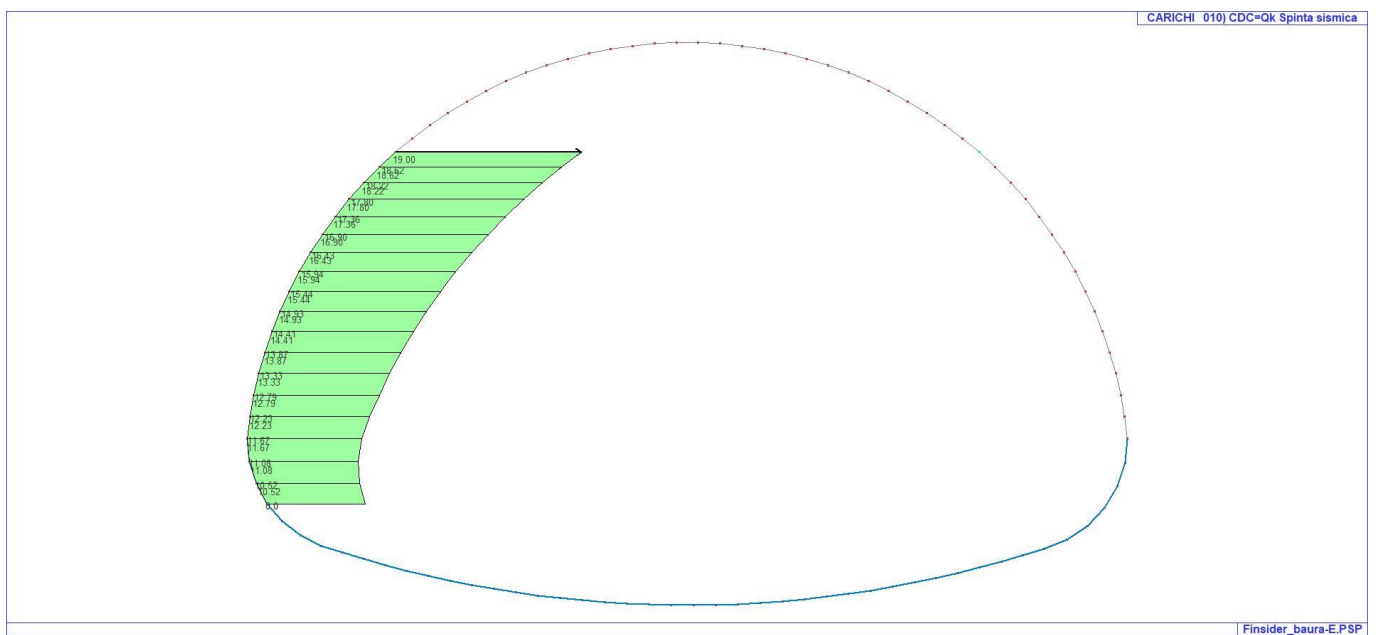
22\_CDC\_007\_CDC=Qk carico stradale Q1k



22\_CDC\_008\_CDC=Qk Spinta traffico



22\_CDC\_009\_CDC=Es (statico SLU) alfa=0.0 (ecc. 0)



22\_CDC\_010\_CDC=Qk Spinta sismica

# DEFINIZIONE DELLE COMBINAZIONI

## LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente. Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni: Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

### Combinazione fondamentale SLU

$$\gamma G_1 \cdot G_1 + \gamma G_2 \cdot G_2 + \gamma P \cdot P + \gamma Q_1 \cdot Q_{k1} + \gamma Q_2 \cdot \psi_{02} \cdot Q_{k2} + \gamma Q_3 \cdot \psi_{03} \cdot Q_{k3} + \dots$$

### Combinazione caratteristica (rara) SLE

$$G_1 + G_2 + P + Q_{k1} + \psi_{02} \cdot Q_{k2} + \psi_{03} \cdot Q_{k3} + \dots$$

### Combinazione frequente SLE

$$G_1 + G_2 + P + \psi_{11} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

### Combinazione quasi permanente SLE

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \psi_{23} \cdot Q_{k3} + \dots$$

### Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

### Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G_1 + G_2 + P + \psi_{21} \cdot Q_{k1} + \psi_{22} \cdot Q_{k2} + \dots$$

Dove:

NTC 2008 Tabella 2.5.I

Destinazione d'uso/azione	$\psi_0$	$\psi_1$	$\psi_2$
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30kN$ )	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30kN$ )	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota $\leq 1000$ m	0,50	0,20	0,00
Neve a quota $> 1000$ m	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti A1 e combinazione 2 con coefficienti A2),
- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2008 Tabella 2.6.I

Coefficiente	<b>EQU</b>	<b>A1</b>	<b>A2</b>
$\gamma_f$			

<i>Carichi permanenti</i>	<i>Favorevoli</i>	$\gamma G1$	0,9	1,0	1,0
	<i>Sfavorevoli</i>		1,1	1,3	1,0
<i>Carichi permanenti non strutturali</i>	<i>Favorevoli</i>	$\gamma G2$	0,0	0,0	0,0
(Non compiutamente definiti)	<i>Sfavorevoli</i>		1,5	1,5	1,3
<i>Carichi variabili</i>	<i>Favorevoli</i>	$\gamma Qi$	0,0	0,0	0,0
	<i>Sfavorevoli</i>		1,5	1,5	1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11 vuoto	
12	SLU	Comb. SLU A1 (SLV sism.) 12	
13	SLE(r)	Comb. SLE(rara) 13	
14	SLE(r)	Comb. SLE(rara) 14	
15	SLE(r)	Comb. SLE(rara) 15	
16	SLE(r)	Comb. SLE(rara) 16	
17	SLE(r)	Comb. SLE(rara) 17	
18	SLE(f)	Comb. SLE(freq.) 18	
19	SLE(f)	Comb. SLE(freq.) 19	
20	SLE(f)	Comb. SLE(freq.) 20	
21	SLE(p)	Comb. SLE(perm.) 21	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.35	1.35	1.35	1.35	1.35	0.0	0.0	0.0	0.0	0.0				
2	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0				
3	1.35	1.35	1.35	1.35	1.35	1.35	1.35	0.0	0.0	0.0				
4	1.00	1.00	1.00	1.00	1.00	1.35	1.35	0.0	0.0	0.0				
5	1.35	1.35	1.35	1.35	1.35	1.01	1.01	0.0	0.0	0.0				
6	1.00	1.00	1.00	1.00	1.00	1.01	1.01	0.0	0.0	0.0				
7	1.35	1.35	1.35	1.35	1.35	0.0	0.0	1.01	0.0	0.0				
8	1.00	1.00	1.00	1.00	1.00	0.0	0.0	1.01	0.0	0.0				
9	1.35	1.35	1.35	1.35	1.35	0.0	0.0	1.35	0.0	0.0				
10	1.00	1.00	1.00	1.00	1.00	0.0	0.0	1.35	0.0	0.0				
11	1.35	1.35	1.35	0.0	1.35	0.0	0.0	0.0	0.0	0.0				
12	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	1.00	0.0				
13	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0				
14	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0				
15	1.00	1.00	1.00	1.00	1.00	0.75	0.75	0.0	0.0	0.0				
16	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.75	0.0	0.0				
17	1.00	1.00	1.00	1.00	1.00	0.0	0.0	1.00	0.0	0.0				
18	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0				
19	1.00	1.00	1.00	1.00	1.00	0.75	0.75	0.0	0.0	0.0				
20	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.75	0.0	0.0				
21	1.00	1.00	1.00	1.00	1.00	0.0	0.0	0.0	0.0	0.0				

# AZIONE SISMICA

## VALUTAZIONE DELL' AZIONE SISMICA

L'azione sismica sulle costruzioni è valutata a partire dalla "pericolosità sismica di base", in condizioni ideali di sito di riferimento rigido con superficie topografica orizzontale.

Allo stato attuale, la pericolosità sismica su reticolo di riferimento nell'intervallo di riferimento è fornita dai dati pubblicati sul sito <http://esse1.mi.ingv.it/>. Per punti non coincidenti con il reticolo di riferimento e periodi di ritorno non contemplati direttamente si opera come indicato nell' allegato alle NTC (rispettivamente media pesata e interpolazione).

L' azione sismica viene definita in relazione ad un periodo di riferimento  $V_r$  che si ricava, per ciascun tipo di costruzione, moltiplicandone la vita nominale per il coefficiente d'uso (vedi tabella Parametri della struttura). Fissato il periodo di riferimento  $V_r$  e la probabilità di superamento  $P_{ver}$  associata a ciascuno degli stati limite considerati, si ottiene il periodo di ritorno  $T_r$  e i relativi parametri di pericolosità sismica (vedi tabella successiva):

ag: accelerazione orizzontale massima del terreno;

Fo: valore massimo del fattore di amplificazione dello spettro in accelerazione orizzontale;

T\*c: periodo di inizio del tratto a velocità costante dello spettro in accelerazione orizzontale;

Parametri della struttura					
Classe d'uso	Vita $V_n$ [anni]	Coeff. Uso	Periodo $V_r$ [anni]	Tipo di suolo	Categoria topografica
II	50.0	1.0	50.0	C	T1

Individuati su reticolo di riferimento i parametri di pericolosità sismica si valutano i parametri spettrali riportati in tabella:

S è il coefficiente che tiene conto della categoria di sottosuolo e delle condizioni topografiche mediante la relazione seguente  $S = S_s \cdot S_t$  (3.2.5)

Fo è il fattore che quantifica l'amplificazione spettrale massima, su sito di riferimento rigido orizzontale

Fv è il fattore che quantifica l'amplificazione spettrale massima verticale, in termini di accelerazione orizzontale massima del terreno ag su sito di riferimento rigido orizzontale

Tb è il periodo corrispondente all'inizio del tratto dello spettro ad accelerazione costante.

Tc è il periodo corrispondente all'inizio del tratto dello spettro a velocità costante.

Td è il periodo corrispondente all'inizio del tratto dello spettro a spostamento costante.

Id nodo	Longitudine	Latitudine	Distanza
			Km
Loc.	11.618	44.836	
15402	11.588	44.820	2.950
15403	11.659	44.821	3.626
15181	11.657	44.871	4.943
15180	11.587	44.870	4.487

SL	$P_{ver}$	$T_r$	ag	Fo	T*c
		Anni	g		sec
SLO	81.0	30.1	0.037	2.550	0.250
SLD	63.0	50.3	0.046	2.507	0.277
SLV	10.0	474.6	0.132	2.597	0.272
SLC	5.0	974.8	0.178	2.557	0.280

SL	ag	S	Fo	Fv	Tb	Tc	Td
	g				sec	sec	sec
SLO	0.037	1.500	2.550	0.659	0.138	0.415	1.747
SLD	0.046	1.500	2.507	0.725	0.148	0.444	1.784
SLV	0.132	1.494	2.597	1.274	0.146	0.439	2.128
SLC	0.178	1.427	2.557	1.455	0.149	0.447	2.311

# RISULTATI ANALISI SISMICHE

## LEGENDA TABELLA ANALISI SISMICHE

Il programma consente l'analisi di diverse configurazioni sismiche.

Sono previsti, infatti, i seguenti casi di carico:

- 9. Esk** caso di carico sismico con analisi statica equivalente
- 10. Edk** caso di carico sismico con analisi dinamica

Ciascun caso di carico è caratterizzato da un angolo di ingresso e da una configurazione di masse determinante la forza sismica complessiva (si rimanda al capitolo relativo ai casi di carico per chiarimenti inerenti questo aspetto).

Nella colonna Note, in funzione della norma in uso sono riportati i parametri fondamentali che caratterizzano l'azione sismica: in particolare possono essere presenti i seguenti valori:

<b>Angolo di ingresso</b>	Angolo di ingresso dell'azione sismica orizzontale
<b>Fattore di importanza</b>	Fattore di importanza dell'edificio, in base alla categoria di appartenenza
<b>Zona sismica</b>	Zona sismica
<b>Accelerazione ag</b>	Accelerazione orizzontale massima sul suolo
<b>Categoria suolo</b>	Categoria di profilo stratigrafico del suolo di fondazione
<b>Fattore di struttura q</b>	Fattore dipendente dalla tipologia strutturale
<b>Fattore di sito S</b>	Fattore dipendente dalla stratigrafia e dal profilo topografico
<b>Classe di duttilità CD</b>	Classe di duttilità della struttura – "A" duttilità alta, "B" duttilità bassa
<b>Fattore riduz. SLD</b>	Fattore di riduzione dello spettro elastico per lo stato limite di danno
<b>Periodo proprio T1</b>	Periodo proprio di vibrazione della struttura
<b>Coefficiente Lambda</b>	Coefficiente dipendente dal periodo proprio T1 e dal numero di piani della struttura
<b>Ordinata spettro Sd(T1)</b>	Valore delle ordinate dello spettro di progetto per lo stato limite ultimo, componente orizzontale (verticale Svd)
<b>Ordinata spettro Se(T1)</b>	Valore delle ordinate dello spettro elastico ridotta del fattore SLD per lo stato limite di danno, componente orizzontale (verticale Sve)
<b>Ordinata spettro S (Tb-Tc)</b>	Valore dell' ordinata dello spettro in uso nel tratto costante
<b>numero di modi considerati</b>	Numero di modi di vibrare della struttura considerati nell'analisi dinamica

Per ciascun caso di carico sismico viene riportato l'insieme di dati sotto riportati (le masse sono espresse in unità di forza):

- a) **analisi sismica statica equivalente:**
  - quota, posizione del centro di applicazione e azione orizzontale risultante, posizione del baricentro delle rigidezze, rapporto  $r/L_s$  (per strutture a nucleo), indici di regolarità  $e/r$  secondo EC8 4.2.3.2
  - azione sismica complessiva
- b) **analisi sismica dinamica con spettro di risposta:**
  - quota, posizione del centro di massa e massa risultante, posizione del baricentro delle rigidezze,

- rapporto  $r/L_s$  (per strutture a nucleo) , indici di regolarità e/r secondo EC8 4.2.3.2
- frequenza, periodo, accelerazione spettrale, massa eccitata nelle tre direzioni globali per tutti i modi
- massa complessiva ed aliquota di massa complessiva eccitata.

Per ciascuna combinazione sismica definita SLD o SLO viene riportato il livello di deformazione  $\epsilon_T$  (dr) degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso anche in unità  $1000 \cdot \epsilon_T/h$  da confrontare direttamente con i valori forniti nella norma ( es. 5 per edifici con tamponamenti collegati rigidamente alla struttura, 10.0 per edifici con tamponamenti collegati elasticamente, 3 per edifici in muratura ordinaria, 4 per edifici in muratura armata).

Qualora si applichi il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") l'analisi sismica dinamica può essere comprensiva di sollecitazione verticale contemporanea a quella orizzontale, nel qual caso è effettuata una sovrapposizione degli effetti in ragione della radice dei quadrati degli effetti stessi. Per ciascuna combinazione sismica - analisi effettuate con il D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento") - viene riportato il livello di deformazione  $\epsilon_T$ ,  $\epsilon_P$  e  $\epsilon_D$  degli elementi strutturali verticali. Per semplicità di consultazione il livello è espresso in unità  $1000 \cdot \epsilon_T/h$  da confrontare direttamente con il valore 2 o 4 per la verifica.

Per gli edifici sismicamente isolati si riportano di seguito le verifiche condotte sui dispositivi di isolamento. Le verifiche sono effettuate secondo l' allegato 10.A dell'Ordinanza 3274 e smi. In particolare la tabella, per ogni combinazione SLU (SLC per il DM 14-01-2008) sismica riporta il codice di verifica e i valori utilizzati per la verifica: spostamento  $d_E$ , area ridotta e dimensione  $A_2$ , azione verticale, deformazioni di taglio dell' elastomero e tensioni nell' acciaio.

<b>Nodo</b>	Nodo di appoggio dell' isolatore
<b>Cmb</b>	Combinazione oggetto della verifica
<b>Verif.</b>	Codice di verifica ok – verifica positiva , NV – verifica negativa, ND – verifica non completata
<b>dE</b>	Spostamento relativo tra le due facce (amplificato del 20% per Ordinanza 3274 e smi) combinato con la regola del 30%
<b>Ang fi</b>	Angolo utilizzato per il calcolo dell' area ridotta $A_r$ (per dispositivi circolari)
<b>V</b>	Azione verticale agente
<b>Ar</b>	Area ridotta efficace
<b>Dim A2</b>	Dimensione utile per il calcolo della deformazione per rotazione
<b>Sig s</b>	Tensione nell' inserto in acciaio
<b>Gam c(a,s,t)</b>	Deformazioni di taglio dell' elastomero
<b>Vcr</b>	Carico critico per instabilità

Affinché la verifica sia positiva deve essere:

- 1)  $V > 0$
- 2)  $\text{Sig } s < f_{yk}$
- 3)  $\text{Gam } t < 5$
- 4)  $\text{Gam } s < \text{Gam}^*$  (caratteristica dell' elastomero)
- 5)  $\text{Gam } s < 2$
- 6)  $V < 0.5 V_{cr}$

CDC	Tipo	Sigla Id	Note
9	Esk	CDC=Es (statico SLU) $\alpha=0.0$ (ecc. 0)	
			categoria suolo: C
			fattore di sito $S = 1.494$
			ordinata spettro (tratto $T_b-T_c$ ) = 0.513 g
			angolo di ingresso: 0.0
			eccentricità aggiuntiva: nulla
			periodo proprio $T_1$ : 0.171 sec.
			fattore $q$ : 1.000
			amplificazione ND (non dissipativi): 1.000
			fattore per spost. $\mu_d$ : 1.000
			classe di duttilità CD: B
			coefficiente $\Lambda$ : 1.000



CDC	Tipo	Sigla Id	Note
			ordinata spettro Sd(T1): 0.513

Quota	Forza Sismica	Tot. parziale	M Sismica x g	Pos. GX	Pos. GY	E agg. X-X	E agg. Y-Y	Pos. KX	Pos. KY	rapp. r/Ls	rapp. ex/rx	rapp. ey/ry
cm	daN	daN	daN	cm	cm	cm	cm	cm	cm			
457.03	75.04	75.04	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
456.53	74.96	149.99	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
455.54	74.79	224.79	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
454.05	74.55	299.34	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
452.06	74.22	373.56	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
449.60	73.82	447.38	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
446.65	73.33	520.71	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
443.23	72.77	593.48	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
439.34	72.13	665.61	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
435.00	71.42	737.03	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
430.21	70.63	807.67	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
424.99	69.78	877.45	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
419.35	68.85	946.30	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
413.31	67.86	1014.16	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
406.88	66.80	1080.96	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
400.07	65.69	1146.65	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
392.90	64.51	1211.16	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
385.39	63.28	1274.43	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
377.56	61.99	1336.42	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
369.43	60.65	1397.08	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
361.01	59.27	1456.35	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
352.33	57.85	1514.20	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
343.41	56.38	1570.58	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
334.28	54.88	1625.47	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
324.94	53.35	1678.82	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
315.44	51.79	1730.61	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
305.78	50.20	1780.81	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
296.00	48.60	1829.41	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
286.12	46.98	1876.39	125.59	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
276.15	22.67	1899.06	62.79	197.18	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Risulta	1899.06		3704.81									

# RISULTATI NODALI

## LEGENDA RISULTATI NODALI

Il controllo dei risultati delle analisi condotte, per quanto concerne i nodi strutturali, è possibile in relazione alle tabelle sottoriportate.

Una prima tabella riporta infatti per ogni nodo e per ogni combinazione (o caso di carico) gli spostamenti nodali.

Una seconda tabella riporta per ogni nodo a cui sia associato un vincolo rigido e/o elastico o una fondazione speciale e per ogni combinazione (o caso di carico) i valori delle azioni esercitate dalla struttura sui vincoli (reazioni vincolari cambiate di segno).

Una terza tabella, infine riassume per ogni nodo le sei combinazioni in cui si attingono i valori minimi e massimi della reazione Fz, della reazione Mx e della reazione My.

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		cm	cm	cm			
1	3	-0.11	0.0	-2.37	0.0	-7.78e-04	0.0
1	10	1.08	0.0	1.04	0.0	8.15e-03	0.0
1	12	0.15	0.0	-0.16	0.0	1.29e-03	0.0
1	14	-0.08	0.0	-1.75	0.0	-5.76e-04	0.0
1	17	0.80	0.0	0.67	0.0	6.03e-03	0.0
1	19	-0.06	0.0	-1.41	0.0	-4.35e-04	0.0
1	20	0.59	0.0	0.40	0.0	4.52e-03	0.0
1	21	-0.01	0.0	-0.39	0.0	-1.15e-05	0.0
2	3	-0.11	0.0	-2.37	0.0	-5.66e-04	0.0
2	10	1.16	0.0	1.03	0.0	8.17e-03	0.0
2	12	0.16	0.0	-0.16	0.0	1.33e-03	0.0
2	14	-0.08	0.0	-1.75	0.0	-4.19e-04	0.0
2	17	0.86	0.0	0.66	0.0	6.06e-03	0.0
2	19	-0.07	0.0	-1.41	0.0	-3.08e-04	0.0
2	20	0.64	0.0	0.40	0.0	4.55e-03	0.0
2	21	-0.01	0.0	-0.39	0.0	2.67e-05	0.0
3	3	-0.12	0.0	-2.37	0.0	-3.60e-04	0.0
3	10	1.24	0.0	1.02	0.0	8.16e-03	0.0
3	12	0.17	0.0	-0.16	0.0	1.36e-03	0.0
3	14	-0.09	0.0	-1.75	0.0	-2.66e-04	0.0
3	17	0.92	0.0	0.65	0.0	6.06e-03	0.0
3	19	-0.07	0.0	-1.41	0.0	-1.85e-04	0.0
3	20	0.68	0.0	0.39	0.0	4.56e-03	0.0
3	21	-0.01	0.0	-0.39	0.0	5.84e-05	0.0
4	3	-0.12	0.0	-2.37	0.0	-1.59e-04	0.0
4	10	1.32	0.0	1.00	0.0	8.12e-03	0.0
4	12	0.19	0.0	-0.17	0.0	1.38e-03	0.0
4	14	-0.09	0.0	-1.75	0.0	-1.18e-04	0.0
4	17	0.98	0.0	0.64	0.0	6.04e-03	0.0
4	19	-0.07	0.0	-1.41	0.0	-6.73e-05	0.0
4	20	0.73	0.0	0.38	0.0	4.55e-03	0.0
4	21	-0.01	0.0	-0.39	0.0	8.46e-05	0.0
5	3	-0.12	0.0	-2.37	0.0	3.41e-05	0.0
5	10	1.40	0.0	0.97	0.0	8.07e-03	0.0
5	12	0.20	0.0	-0.17	0.0	1.40e-03	0.0
5	14	-0.09	0.0	-1.75	0.0	2.53e-05	0.0
5	17	1.03	0.0	0.62	0.0	6.01e-03	0.0
5	19	-0.07	0.0	-1.41	0.0	4.54e-05	0.0
5	20	0.77	0.0	0.37	0.0	4.53e-03	0.0
5	21	-0.01	0.0	-0.39	0.0	1.06e-04	0.0
6	3	-0.12	0.0	-2.37	0.0	2.20e-04	0.0
6	10	1.48	0.0	0.95	0.0	8.00e-03	0.0
6	12	0.21	0.0	-0.17	0.0	1.41e-03	0.0
6	14	-0.09	0.0	-1.75	0.0	1.63e-04	0.0
6	17	1.09	0.0	0.60	0.0	5.96e-03	0.0
6	19	-0.07	0.0	-1.41	0.0	1.53e-04	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
6	20	0.82	0.0	0.35	0.0	4.50e-03	0.0
6	21	-0.01	0.0	-0.39	0.0	1.23e-04	0.0
7	3	-0.12	0.0	-2.37	0.0	3.97e-04	0.0
7	10	1.55	0.0	0.92	0.0	7.92e-03	0.0
7	12	0.23	0.0	-0.18	0.0	1.42e-03	0.0
7	14	-0.09	0.0	-1.75	0.0	2.94e-04	0.0
7	17	1.15	0.0	0.58	0.0	5.90e-03	0.0
7	19	-0.07	0.0	-1.41	0.0	2.55e-04	0.0
7	20	0.86	0.0	0.34	0.0	4.46e-03	0.0
7	21	-8.95e-03	0.0	-0.39	0.0	1.37e-04	0.0
8	3	-0.11	0.0	-2.37	0.0	5.64e-04	0.0
8	10	1.62	0.0	0.89	0.0	7.83e-03	0.0
8	12	0.24	0.0	-0.19	0.0	1.43e-03	0.0
8	14	-0.08	0.0	-1.76	0.0	4.18e-04	0.0
8	17	1.20	0.0	0.55	0.0	5.84e-03	0.0
8	19	-0.06	0.0	-1.42	0.0	3.51e-04	0.0
8	20	0.90	0.0	0.32	0.0	4.42e-03	0.0
8	21	-7.65e-03	0.0	-0.40	0.0	1.49e-04	0.0
9	3	-0.11	0.0	-2.37	0.0	7.21e-04	0.0
9	10	1.69	0.0	0.85	0.0	7.73e-03	0.0
9	12	0.25	0.0	-0.19	0.0	1.43e-03	0.0
9	14	-0.08	0.0	-1.76	0.0	5.34e-04	0.0
9	17	1.25	0.0	0.53	0.0	5.77e-03	0.0
9	19	-0.06	0.0	-1.42	0.0	4.40e-04	0.0
9	20	0.94	0.0	0.30	0.0	4.36e-03	0.0
9	21	-6.30e-03	0.0	-0.40	0.0	1.58e-04	0.0
10	3	-0.10	0.0	-2.38	0.0	8.67e-04	0.0
10	10	1.76	0.0	0.81	0.0	7.62e-03	0.0
10	12	0.26	0.0	-0.20	0.0	1.42e-03	0.0
10	14	-0.07	0.0	-1.76	0.0	6.42e-04	0.0
10	17	1.30	0.0	0.50	0.0	5.69e-03	0.0
10	19	-0.06	0.0	-1.42	0.0	5.23e-04	0.0
10	20	0.98	0.0	0.27	0.0	4.31e-03	0.0
10	21	-4.92e-03	0.0	-0.40	0.0	1.65e-04	0.0
11	3	-0.09	0.0	-2.38	0.0	9.99e-04	0.0
11	10	1.82	0.0	0.77	0.0	7.52e-03	0.0
11	12	0.28	0.0	-0.21	0.0	1.42e-03	0.0
11	14	-0.07	0.0	-1.77	0.0	7.40e-04	0.0
11	17	1.35	0.0	0.47	0.0	5.61e-03	0.0
11	19	-0.05	0.0	-1.42	0.0	5.98e-04	0.0
11	20	1.01	0.0	0.25	0.0	4.25e-03	0.0
11	21	-3.55e-03	0.0	-0.40	0.0	1.71e-04	0.0
12	3	-0.08	0.0	-2.39	0.0	1.12e-03	0.0
12	10	1.88	0.0	0.72	0.0	7.41e-03	0.0
12	12	0.29	0.0	-0.22	0.0	1.41e-03	0.0
12	14	-0.06	0.0	-1.77	0.0	8.28e-04	0.0
12	17	1.39	0.0	0.43	0.0	5.53e-03	0.0
12	19	-0.05	0.0	-1.43	0.0	6.65e-04	0.0
12	20	1.05	0.0	0.23	0.0	4.19e-03	0.0
12	21	-2.19e-03	0.0	-0.40	0.0	1.76e-04	0.0
13	3	-0.07	0.0	-2.40	0.0	1.22e-03	0.0
13	10	1.94	0.0	0.68	0.0	7.30e-03	0.0
13	12	0.30	0.0	-0.22	0.0	1.41e-03	0.0
13	14	-0.06	0.0	-1.78	0.0	9.04e-04	0.0
13	17	1.44	0.0	0.40	0.0	5.46e-03	0.0
13	19	-0.04	0.0	-1.43	0.0	7.23e-04	0.0
13	20	1.08	0.0	0.20	0.0	4.14e-03	0.0
13	21	-8.51e-04	0.0	-0.40	0.0	1.80e-04	0.0
14	3	-0.06	0.0	-2.41	0.0	1.31e-03	0.0
14	9	2.00	0.0	0.49	0.0	7.27e-03	0.0
14	12	0.31	0.0	-0.23	0.0	1.40e-03	0.0
14	14	-0.05	0.0	-1.78	0.0	9.68e-04	0.0
14	17	1.48	0.0	0.36	0.0	5.38e-03	0.0
14	19	-0.04	0.0	-1.44	0.0	7.71e-04	0.0
14	20	1.11	0.0	0.17	0.0	4.08e-03	0.0
14	21	4.48e-04	0.0	-0.40	0.0	1.83e-04	0.0
15	3	-0.06	0.0	-2.42	0.0	1.37e-03	0.0
15	9	2.05	0.0	0.44	0.0	7.17e-03	0.0
15	12	0.32	0.0	-0.24	0.0	1.39e-03	0.0
15	14	-0.04	0.0	-1.79	0.0	1.02e-03	0.0
15	17	1.52	0.0	0.33	0.0	5.31e-03	0.0
15	19	-0.03	0.0	-1.44	0.0	8.09e-04	0.0
15	20	1.14	0.0	0.14	0.0	4.03e-03	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
15	21	1.70e-03	0.0	-0.40	0.0	1.85e-04	0.0
16	3	-0.05	0.0	-2.43	0.0	1.42e-03	0.0
16	9	2.10	0.0	0.39	0.0	7.09e-03	0.0
16	12	0.33	0.0	-0.25	0.0	1.38e-03	0.0
16	14	-0.03	0.0	-1.80	0.0	1.05e-03	0.0
16	17	1.55	0.0	0.29	0.0	5.25e-03	0.0
16	19	-0.02	0.0	-1.45	0.0	8.35e-04	0.0
16	20	1.16	0.0	0.11	0.0	3.98e-03	0.0
16	21	2.89e-03	0.0	-0.40	0.0	1.87e-04	0.0
17	3	-0.04	0.0	-2.44	0.0	1.44e-03	0.0
17	9	2.14	0.0	0.33	0.0	7.01e-03	0.0
17	12	0.34	0.0	-0.27	0.0	1.37e-03	0.0
17	14	-0.03	0.0	-1.81	0.0	1.07e-03	0.0
17	17	1.59	0.0	0.25	0.0	5.19e-03	0.0
17	19	-0.02	0.0	-1.46	0.0	8.49e-04	0.0
17	20	1.19	0.0	0.08	0.0	3.94e-03	0.0
17	21	4.01e-03	0.0	-0.41	0.0	1.87e-04	0.0
18	3	-0.03	0.0	-2.45	0.0	1.45e-03	0.0
18	9	2.18	0.0	0.28	0.0	6.94e-03	0.0
18	12	0.34	0.0	-0.28	0.0	1.36e-03	0.0
18	14	-0.02	0.0	-1.82	0.0	1.07e-03	0.0
18	17	1.62	0.0	0.20	0.0	5.14e-03	0.0
18	19	-0.01	0.0	-1.46	0.0	8.50e-04	0.0
18	20	1.21	0.0	0.05	0.0	3.90e-03	0.0
18	21	5.06e-03	0.0	-0.41	0.0	1.86e-04	0.0
19	3	-0.02	0.0	-2.46	0.0	1.43e-03	0.0
19	9	2.22	0.0	0.22	0.0	6.88e-03	0.0
19	12	0.35	0.0	-0.29	0.0	1.34e-03	0.0
19	14	-0.01	0.0	-1.83	0.0	1.06e-03	0.0
19	17	1.65	0.0	0.16	0.0	5.10e-03	0.0
19	19	-9.48e-03	0.0	-1.47	0.0	8.39e-04	0.0
19	20	1.24	0.0	0.02	0.0	3.87e-03	0.0
19	21	6.03e-03	0.0	-0.41	0.0	1.83e-04	0.0
20	3	-0.01	0.0	-2.48	0.0	1.39e-03	0.0
20	9	2.26	0.0	0.16	0.0	6.83e-03	0.0
20	12	0.36	0.0	-0.30	0.0	1.33e-03	0.0
20	14	-9.24e-03	0.0	-1.83	0.0	1.03e-03	0.0
20	17	1.67	0.0	0.12	0.0	5.06e-03	0.0
20	19	-5.21e-03	0.0	-1.48	0.0	8.16e-04	0.0
20	20	1.26	0.0	-0.01	0.0	3.84e-03	0.0
20	21	6.89e-03	0.0	-0.41	0.0	1.78e-04	0.0
21	3	-6.03e-03	0.0	-2.49	0.0	1.33e-03	0.0
21	9	2.29	0.0	0.10	0.0	6.78e-03	0.0
21	12	0.37	0.0	-0.31	0.0	1.31e-03	0.0
21	14	-4.47e-03	0.0	-1.84	0.0	9.84e-04	0.0
21	17	1.70	0.0	0.07	0.0	5.03e-03	0.0
21	19	-1.44e-03	0.0	-1.49	0.0	7.81e-04	0.0
21	20	1.27	0.0	-0.05	0.0	3.81e-03	0.0
21	21	7.65e-03	0.0	-0.41	0.0	1.72e-04	0.0
22	3	-5.17e-04	0.0	-2.50	0.0	1.25e-03	0.0
22	9	2.32	0.0	0.04	0.0	6.75e-03	0.0
22	12	0.37	0.0	-0.32	0.0	1.29e-03	0.0
22	14	-3.83e-04	0.0	-1.85	0.0	9.25e-04	0.0
22	17	1.72	0.0	0.03	0.0	5.00e-03	0.0
22	19	1.79e-03	0.0	-1.49	0.0	7.35e-04	0.0
22	20	1.29	0.0	-0.08	0.0	3.79e-03	0.0
22	21	8.30e-03	0.0	-0.41	0.0	1.64e-04	0.0
23	3	4.06e-03	0.0	-2.51	0.0	1.15e-03	0.0
23	9	2.34	0.0	-0.02	0.0	6.72e-03	0.0
23	12	0.38	0.0	-0.33	0.0	1.27e-03	0.0
23	14	3.01e-03	0.0	-1.86	0.0	8.54e-04	0.0
23	17	1.74	0.0	-0.02	0.0	4.97e-03	0.0
23	19	4.46e-03	0.0	-1.50	0.0	6.79e-04	0.0
23	20	1.30	0.0	-0.12	0.0	3.77e-03	0.0
23	21	8.84e-03	0.0	-0.42	0.0	1.54e-04	0.0
24	3	7.70e-03	0.0	-2.52	0.0	1.04e-03	0.0
24	9	2.37	0.0	-0.09	0.0	6.69e-03	0.0
24	12	0.38	0.0	-0.35	0.0	1.26e-03	0.0
24	14	5.71e-03	0.0	-1.87	0.0	7.71e-04	0.0
24	17	1.75	0.0	-0.06	0.0	4.96e-03	0.0
24	19	6.60e-03	0.0	-1.51	0.0	6.13e-04	0.0
24	20	1.32	0.0	-0.15	0.0	3.75e-03	0.0
24	21	9.27e-03	0.0	-0.42	0.0	1.42e-04	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
25	3	0.01	0.0	-2.53	0.0	9.13e-04	0.0
25	9	2.39	0.0	-0.15	0.0	6.67e-03	0.0
25	12	0.38	0.0	-0.36	0.0	1.24e-03	0.0
25	14	7.75e-03	0.0	-1.88	0.0	6.77e-04	0.0
25	17	1.77	0.0	-0.11	0.0	4.94e-03	0.0
25	19	8.21e-03	0.0	-1.51	0.0	5.40e-04	0.0
25	20	1.33	0.0	-0.19	0.0	3.74e-03	0.0
25	21	9.58e-03	0.0	-0.42	0.0	1.29e-04	0.0
26	3	0.01	0.0	-2.54	0.0	7.74e-04	0.0
26	9	2.40	0.0	-0.22	0.0	6.66e-03	0.0
26	12	0.39	0.0	-0.37	0.0	1.21e-03	0.0
26	14	9.20e-03	0.0	-1.88	0.0	5.74e-04	0.0
26	17	1.78	0.0	-0.16	0.0	4.93e-03	0.0
26	19	9.35e-03	0.0	-1.52	0.0	4.59e-04	0.0
26	20	1.34	0.0	-0.23	0.0	3.73e-03	0.0
26	21	9.80e-03	0.0	-0.42	0.0	1.14e-04	0.0
27	3	0.01	0.0	-2.55	0.0	6.25e-04	0.0
27	9	2.42	0.0	-0.28	0.0	6.65e-03	0.0
27	12	0.39	0.0	-0.38	0.0	1.19e-03	0.0
27	14	0.01	0.0	-1.89	0.0	4.63e-04	0.0
27	17	1.79	0.0	-0.21	0.0	4.93e-03	0.0
27	19	0.01	0.0	-1.52	0.0	3.72e-04	0.0
27	20	1.34	0.0	-0.26	0.0	3.72e-03	0.0
27	21	9.93e-03	0.0	-0.42	0.0	9.82e-05	0.0
28	3	0.01	0.0	-2.55	0.0	4.67e-04	0.0
28	9	2.43	0.0	-0.35	0.0	6.65e-03	0.0
28	12	0.39	0.0	-0.39	0.0	1.17e-03	0.0
28	14	0.01	0.0	-1.89	0.0	3.46e-04	0.0
28	17	1.80	0.0	-0.26	0.0	4.93e-03	0.0
28	19	0.01	0.0	-1.52	0.0	2.80e-04	0.0
28	20	1.35	0.0	-0.30	0.0	3.72e-03	0.0
28	21	9.97e-03	0.0	-0.42	0.0	8.13e-05	0.0
29	3	0.01	0.0	-2.56	0.0	3.04e-04	0.0
29	9	2.43	0.0	-0.41	0.0	6.66e-03	0.0
29	12	0.39	0.0	-0.41	0.0	1.15e-03	0.0
29	14	0.01	0.0	-1.89	0.0	2.25e-04	0.0
29	17	1.80	0.0	-0.31	0.0	4.93e-03	0.0
29	19	0.01	0.0	-1.53	0.0	1.85e-04	0.0
29	20	1.35	0.0	-0.34	0.0	3.71e-03	0.0
29	21	9.96e-03	0.0	-0.42	0.0	6.38e-05	0.0
30	3	0.01	0.0	-2.56	0.0	1.37e-04	0.0
30	9	2.44	0.0	-0.48	0.0	6.67e-03	0.0
30	12	0.39	0.0	-0.42	0.0	1.13e-03	0.0
30	14	0.01	0.0	-1.90	0.0	1.02e-04	0.0
30	17	1.80	0.0	-0.36	0.0	4.94e-03	0.0
30	19	0.01	0.0	-1.53	0.0	8.77e-05	0.0
30	20	1.36	0.0	-0.37	0.0	3.72e-03	0.0
30	21	9.90e-03	0.0	-0.42	0.0	4.58e-05	0.0
31	3	0.01	0.0	-2.56	0.0	-3.08e-05	0.0
31	9	2.44	0.0	-0.55	0.0	6.68e-03	0.0
31	12	0.39	0.0	-0.43	0.0	1.12e-03	0.0
31	14	0.01	0.0	-1.90	0.0	-2.28e-05	0.0
31	17	1.80	0.0	-0.41	0.0	4.95e-03	0.0
31	19	0.01	0.0	-1.53	0.0	-1.02e-05	0.0
31	20	1.36	0.0	-0.41	0.0	3.72e-03	0.0
31	21	9.81e-03	0.0	-0.42	0.0	2.77e-05	0.0
32	3	0.01	0.0	-2.56	0.0	-1.98e-04	0.0
32	9	2.43	0.0	-0.62	0.0	6.70e-03	0.0
32	12	0.39	0.0	-0.44	0.0	1.10e-03	0.0
32	14	0.01	0.0	-1.90	0.0	-1.46e-04	0.0
32	17	1.80	0.0	-0.46	0.0	4.97e-03	0.0
32	19	0.01	0.0	-1.53	0.0	-1.07e-04	0.0
32	20	1.35	0.0	-0.45	0.0	3.73e-03	0.0
32	21	9.72e-03	0.0	-0.42	0.0	9.77e-06	0.0
33	3	0.01	0.0	-2.56	0.0	-3.61e-04	0.0
33	9	2.42	0.0	-0.68	0.0	6.73e-03	0.0
33	12	0.39	0.0	-0.45	0.0	1.08e-03	0.0
33	14	0.01	0.0	-1.89	0.0	-2.67e-04	0.0
33	17	1.80	0.0	-0.51	0.0	4.98e-03	0.0
33	19	0.01	0.0	-1.53	0.0	-2.02e-04	0.0
33	20	1.35	0.0	-0.49	0.0	3.74e-03	0.0
33	21	9.63e-03	0.0	-0.42	0.0	-7.77e-06	0.0
34	3	0.01	0.0	-2.55	0.0	-5.18e-04	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
34	9	2.41	0.0	-0.75	0.0	6.76e-03	0.0
34	12	0.39	0.0	-0.46	0.0	1.07e-03	0.0
34	14	0.01	0.0	-1.89	0.0	-3.84e-04	0.0
34	17	1.79	0.0	-0.56	0.0	5.01e-03	0.0
34	19	0.01	0.0	-1.52	0.0	-2.94e-04	0.0
34	20	1.34	0.0	-0.52	0.0	3.75e-03	0.0
34	21	9.57e-03	0.0	-0.42	0.0	-2.46e-05	0.0
35	3	0.02	0.0	-2.55	0.0	-6.68e-04	0.0
35	9	2.40	0.0	-0.82	0.0	6.79e-03	0.0
35	12	0.39	0.0	-0.47	0.0	1.06e-03	0.0
35	14	0.01	0.0	-1.89	0.0	-4.95e-04	0.0
35	17	1.78	0.0	-0.60	0.0	5.03e-03	0.0
35	19	0.01	0.0	-1.52	0.0	-3.81e-04	0.0
35	20	1.34	0.0	-0.56	0.0	3.76e-03	0.0
35	21	9.55e-03	0.0	-0.42	0.0	-4.05e-05	0.0
36	3	0.02	0.0	-2.54	0.0	-8.07e-04	0.0
36	9	2.38	0.0	-0.88	0.0	6.83e-03	0.0
36	12	0.38	0.0	-0.48	0.0	1.05e-03	0.0
36	14	0.01	0.0	-1.88	0.0	-5.98e-04	0.0
36	17	1.77	0.0	-0.65	0.0	5.06e-03	0.0
36	19	0.01	0.0	-1.52	0.0	-4.62e-04	0.0
36	20	1.33	0.0	-0.60	0.0	3.78e-03	0.0
36	21	9.58e-03	0.0	-0.42	0.0	-5.52e-05	0.0
37	3	0.02	0.0	-2.53	0.0	-9.34e-04	0.0
37	9	2.36	0.0	-0.95	0.0	6.88e-03	0.0
37	12	0.38	0.0	-0.49	0.0	1.04e-03	0.0
37	14	0.01	0.0	-1.87	0.0	-6.92e-04	0.0
37	17	1.75	0.0	-0.70	0.0	5.09e-03	0.0
37	19	0.01	0.0	-1.51	0.0	-5.36e-04	0.0
37	20	1.32	0.0	-0.63	0.0	3.80e-03	0.0
37	21	9.68e-03	0.0	-0.42	0.0	-6.85e-05	0.0
38	3	0.02	0.0	-2.52	0.0	-1.05e-03	0.0
38	9	2.34	0.0	-1.01	0.0	6.92e-03	0.0
38	12	0.38	0.0	-0.50	0.0	1.04e-03	0.0
38	14	0.02	0.0	-1.87	0.0	-7.75e-04	0.0
38	17	1.73	0.0	-0.75	0.0	5.13e-03	0.0
38	19	0.02	0.0	-1.51	0.0	-6.01e-04	0.0
38	20	1.30	0.0	-0.67	0.0	3.83e-03	0.0
38	21	9.86e-03	0.0	-0.42	0.0	-8.02e-05	0.0
39	3	0.03	0.0	-2.51	0.0	-1.14e-03	0.0
39	9	2.31	0.0	-1.08	0.0	6.98e-03	0.0
39	12	0.37	0.0	-0.51	0.0	1.04e-03	0.0
39	14	0.02	0.0	-1.86	0.0	-8.46e-04	0.0
39	17	1.71	0.0	-0.80	0.0	5.17e-03	0.0
39	19	0.02	0.0	-1.50	0.0	-6.57e-04	0.0
39	20	1.29	0.0	-0.70	0.0	3.85e-03	0.0
39	21	0.01	0.0	-0.42	0.0	-9.02e-05	0.0
40	3	0.03	0.0	-2.50	0.0	-1.22e-03	0.0
40	9	2.28	0.0	-1.14	0.0	7.03e-03	0.0
40	12	0.37	0.0	-0.52	0.0	1.04e-03	0.0
40	14	0.02	0.0	-1.85	0.0	-9.05e-04	0.0
40	17	1.69	0.0	-0.85	0.0	5.21e-03	0.0
40	19	0.02	0.0	-1.49	0.0	-7.03e-04	0.0
40	20	1.27	0.0	-0.74	0.0	3.88e-03	0.0
40	21	0.01	0.0	-0.42	0.0	-9.84e-05	0.0
41	3	0.04	0.0	-2.49	0.0	-1.28e-03	0.0
41	9	2.25	0.0	-1.20	0.0	7.08e-03	0.0
41	12	0.36	0.0	-0.53	0.0	1.04e-03	0.0
41	14	0.03	0.0	-1.84	0.0	-9.49e-04	0.0
41	17	1.67	0.0	-0.89	0.0	5.25e-03	0.0
41	19	0.02	0.0	-1.49	0.0	-7.38e-04	0.0
41	20	1.25	0.0	-0.77	0.0	3.91e-03	0.0
41	21	0.01	0.0	-0.42	0.0	-1.05e-04	0.0
42	3	0.05	0.0	-2.48	0.0	-1.32e-03	0.0
42	9	2.21	0.0	-1.26	0.0	7.14e-03	0.0
42	12	0.36	0.0	-0.54	0.0	1.05e-03	0.0
42	14	0.03	0.0	-1.83	0.0	-9.79e-04	0.0
42	17	1.64	0.0	-0.94	0.0	5.29e-03	0.0
42	19	0.03	0.0	-1.48	0.0	-7.61e-04	0.0
42	20	1.23	0.0	-0.81	0.0	3.94e-03	0.0
42	21	0.01	0.0	-0.42	0.0	-1.09e-04	0.0
43	3	0.05	0.0	-2.46	0.0	-1.34e-03	0.0
43	9	2.17	0.0	-1.32	0.0	7.20e-03	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
43	12	0.35	0.0	-0.55	0.0	1.06e-03	0.0
43	14	0.04	0.0	-1.83	0.0	-9.93e-04	0.0
43	17	1.61	0.0	-0.98	0.0	5.33e-03	0.0
43	19	0.03	0.0	-1.47	0.0	-7.73e-04	0.0
43	20	1.21	0.0	-0.84	0.0	3.97e-03	0.0
43	21	0.01	0.0	-0.42	0.0	-1.12e-04	0.0
44	3	0.06	0.0	-2.45	0.0	-1.34e-03	0.0
44	9	2.13	0.0	-1.38	0.0	7.26e-03	0.0
44	12	0.35	0.0	-0.56	0.0	1.07e-03	0.0
44	14	0.04	0.0	-1.82	0.0	-9.91e-04	0.0
44	17	1.58	0.0	-1.02	0.0	5.38e-03	0.0
44	19	0.04	0.0	-1.47	0.0	-7.71e-04	0.0
44	20	1.18	0.0	-0.87	0.0	4.01e-03	0.0
44	21	0.01	0.0	-0.42	0.0	-1.13e-04	0.0
45	3	0.07	0.0	-2.44	0.0	-1.31e-03	0.0
45	9	2.08	0.0	-1.44	0.0	7.32e-03	0.0
45	12	0.34	0.0	-0.56	0.0	1.08e-03	0.0
45	14	0.05	0.0	-1.81	0.0	-9.72e-04	0.0
45	17	1.54	0.0	-1.06	0.0	5.42e-03	0.0
45	19	0.04	0.0	-1.46	0.0	-7.57e-04	0.0
45	20	1.16	0.0	-0.90	0.0	4.04e-03	0.0
45	21	0.01	0.0	-0.41	0.0	-1.13e-04	0.0
46	3	0.08	0.0	-2.43	0.0	-1.27e-03	0.0
46	9	2.03	0.0	-1.49	0.0	7.38e-03	0.0
46	12	0.33	0.0	-0.57	0.0	1.09e-03	0.0
46	14	0.06	0.0	-1.80	0.0	-9.38e-04	0.0
46	17	1.50	0.0	-1.10	0.0	5.46e-03	0.0
46	19	0.05	0.0	-1.45	0.0	-7.31e-04	0.0
46	20	1.13	0.0	-0.93	0.0	4.07e-03	0.0
46	21	0.01	0.0	-0.41	0.0	-1.11e-04	0.0
47	3	0.09	0.0	-2.42	0.0	-1.20e-03	0.0
47	9	1.98	0.0	-1.54	0.0	7.43e-03	0.0
47	12	0.32	0.0	-0.58	0.0	1.11e-03	0.0
47	14	0.06	0.0	-1.80	0.0	-8.88e-04	0.0
47	17	1.46	0.0	-1.14	0.0	5.50e-03	0.0
47	19	0.05	0.0	-1.45	0.0	-6.93e-04	0.0
47	20	1.10	0.0	-0.96	0.0	4.10e-03	0.0
47	21	0.01	0.0	-0.41	0.0	-1.09e-04	0.0
48	3	0.10	0.0	-2.42	0.0	-1.11e-03	0.0
48	9	1.92	0.0	-1.59	0.0	7.48e-03	0.0
48	12	0.31	0.0	-0.59	0.0	1.12e-03	0.0
48	14	0.07	0.0	-1.79	0.0	-8.25e-04	0.0
48	17	1.42	0.0	-1.18	0.0	5.54e-03	0.0
48	19	0.06	0.0	-1.44	0.0	-6.45e-04	0.0
48	20	1.07	0.0	-0.99	0.0	4.13e-03	0.0
48	21	0.02	0.0	-0.41	0.0	-1.06e-04	0.0
49	3	0.10	0.0	-2.41	0.0	-1.01e-03	0.0
49	9	1.86	0.0	-1.64	0.0	7.53e-03	0.0
49	12	0.31	0.0	-0.59	0.0	1.14e-03	0.0
49	14	0.08	0.0	-1.78	0.0	-7.48e-04	0.0
49	17	1.38	0.0	-1.22	0.0	5.58e-03	0.0
49	19	0.06	0.0	-1.44	0.0	-5.87e-04	0.0
49	20	1.04	0.0	-1.01	0.0	4.16e-03	0.0
49	21	0.02	0.0	-0.41	0.0	-1.02e-04	0.0
50	3	0.11	0.0	-2.40	0.0	-8.92e-04	0.0
50	9	1.80	0.0	-1.68	0.0	7.57e-03	0.0
50	12	0.30	0.0	-0.60	0.0	1.15e-03	0.0
50	14	0.08	0.0	-1.78	0.0	-6.61e-04	0.0
50	17	1.33	0.0	-1.25	0.0	5.61e-03	0.0
50	19	0.07	0.0	-1.44	0.0	-5.20e-04	0.0
50	20	1.00	0.0	-1.04	0.0	4.18e-03	0.0
50	21	0.02	0.0	-0.41	0.0	-9.70e-05	0.0
51	3	0.12	0.0	-2.40	0.0	-7.59e-04	0.0
51	9	1.74	0.0	-1.73	0.0	7.61e-03	0.0
51	12	0.29	0.0	-0.61	0.0	1.17e-03	0.0
51	14	0.09	0.0	-1.78	0.0	-5.62e-04	0.0
51	17	1.29	0.0	-1.28	0.0	5.64e-03	0.0
51	19	0.07	0.0	-1.43	0.0	-4.45e-04	0.0
51	20	0.97	0.0	-1.06	0.0	4.21e-03	0.0
51	21	0.02	0.0	-0.41	0.0	-9.09e-05	0.0
52	3	0.12	0.0	-2.39	0.0	-6.14e-04	0.0
52	9	1.67	0.0	-1.76	0.0	7.65e-03	0.0
52	12	0.28	0.0	-0.61	0.0	1.19e-03	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
52	14	0.09	0.0	-1.77	0.0	-4.55e-04	0.0
52	17	1.24	0.0	-1.31	0.0	5.67e-03	0.0
52	19	0.07	0.0	-1.43	0.0	-3.62e-04	0.0
52	20	0.93	0.0	-1.08	0.0	4.23e-03	0.0
52	21	0.02	0.0	-0.41	0.0	-8.35e-05	0.0
53	3	0.13	0.0	-2.39	0.0	-4.57e-04	0.0
53	9	1.60	0.0	-1.80	0.0	7.68e-03	0.0
53	12	0.27	0.0	-0.62	0.0	1.20e-03	0.0
53	14	0.10	0.0	-1.77	0.0	-3.38e-04	0.0
53	17	1.19	0.0	-1.33	0.0	5.69e-03	0.0
53	19	0.08	0.0	-1.43	0.0	-2.72e-04	0.0
53	20	0.89	0.0	-1.10	0.0	4.25e-03	0.0
53	21	0.02	0.0	-0.41	0.0	-7.44e-05	0.0
54	3	0.13	0.0	-2.39	0.0	-2.89e-04	0.0
54	9	1.53	0.0	-1.83	0.0	7.71e-03	0.0
54	12	0.25	0.0	-0.62	0.0	1.22e-03	0.0
54	14	0.10	0.0	-1.77	0.0	-2.14e-04	0.0
54	17	1.13	0.0	-1.36	0.0	5.71e-03	0.0
54	19	0.08	0.0	-1.43	0.0	-1.76e-04	0.0
54	20	0.85	0.0	-1.12	0.0	4.27e-03	0.0
54	21	0.02	0.0	-0.41	0.0	-6.30e-05	0.0
55	3	0.13	0.0	-2.39	0.0	-1.12e-04	0.0
55	9	1.46	0.0	-1.86	0.0	7.73e-03	0.0
55	12	0.24	0.0	-0.63	0.0	1.24e-03	0.0
55	14	0.10	0.0	-1.77	0.0	-8.27e-05	0.0
55	17	1.08	0.0	-1.38	0.0	5.73e-03	0.0
55	19	0.08	0.0	-1.43	0.0	-7.42e-05	0.0
55	20	0.81	0.0	-1.14	0.0	4.28e-03	0.0
55	21	0.02	0.0	-0.41	0.0	-4.89e-05	0.0
56	3	0.13	0.0	-2.39	0.0	7.42e-05	0.0
56	9	1.38	0.0	-1.89	0.0	7.75e-03	0.0
56	12	0.23	0.0	-0.63	0.0	1.26e-03	0.0
56	14	0.10	0.0	-1.77	0.0	5.49e-05	0.0
56	17	1.03	0.0	-1.40	0.0	5.74e-03	0.0
56	19	0.08	0.0	-1.43	0.0	3.33e-05	0.0
56	20	0.77	0.0	-1.15	0.0	4.30e-03	0.0
56	21	0.02	0.0	-0.41	0.0	-3.15e-05	0.0
57	3	0.13	0.0	-2.39	0.0	2.68e-04	0.0
57	9	1.31	0.0	-1.91	0.0	7.77e-03	0.0
57	12	0.22	0.0	-0.63	0.0	1.29e-03	0.0
57	14	0.10	0.0	-1.77	0.0	1.98e-04	0.0
57	17	0.97	0.0	-1.41	0.0	5.75e-03	0.0
57	19	0.08	0.0	-1.43	0.0	1.46e-04	0.0
57	20	0.73	0.0	-1.16	0.0	4.31e-03	0.0
57	21	0.02	0.0	-0.41	0.0	-1.01e-05	0.0
58	3	0.13	0.0	-2.39	0.0	4.68e-04	0.0
58	9	1.23	0.0	-1.92	0.0	7.78e-03	0.0
58	12	0.21	0.0	-0.64	0.0	1.32e-03	0.0
58	14	0.10	0.0	-1.77	0.0	3.47e-04	0.0
58	17	0.91	0.0	-1.43	0.0	5.76e-03	0.0
58	19	0.08	0.0	-1.43	0.0	2.64e-04	0.0
58	20	0.69	0.0	-1.17	0.0	4.33e-03	0.0
58	21	0.02	0.0	-0.41	0.0	1.61e-05	0.0
59	3	0.12	0.0	-2.39	0.0	6.75e-04	0.0
59	9	1.16	0.0	-1.94	0.0	7.79e-03	0.0
59	12	0.19	0.0	-0.64	0.0	1.35e-03	0.0
59	14	0.09	0.0	-1.77	0.0	5.00e-04	0.0
59	17	0.86	0.0	-1.44	0.0	5.77e-03	0.0
59	19	0.07	0.0	-1.43	0.0	3.87e-04	0.0
59	20	0.65	0.0	-1.18	0.0	4.34e-03	0.0
59	21	0.02	0.0	-0.41	0.0	4.79e-05	0.0
60	3	0.12	0.0	-2.39	0.0	8.87e-04	0.0
60	9	1.08	0.0	-1.95	0.0	7.80e-03	0.0
60	12	0.18	0.0	-0.64	0.0	1.38e-03	0.0
60	14	0.09	0.0	-1.77	0.0	6.57e-04	0.0
60	17	0.80	0.0	-1.44	0.0	5.78e-03	0.0
60	19	0.07	0.0	-1.43	0.0	5.14e-04	0.0
60	20	0.60	0.0	-1.18	0.0	4.36e-03	0.0
60	21	0.02	0.0	-0.41	0.0	8.61e-05	0.0
61	3	0.10	0.0	-2.39	0.0	1.12e-03	0.0
61	9	0.99	0.0	-1.94	0.0	7.81e-03	0.0
61	12	0.16	0.0	-0.64	0.0	1.43e-03	0.0
61	14	0.08	0.0	-1.77	0.0	8.33e-04	0.0



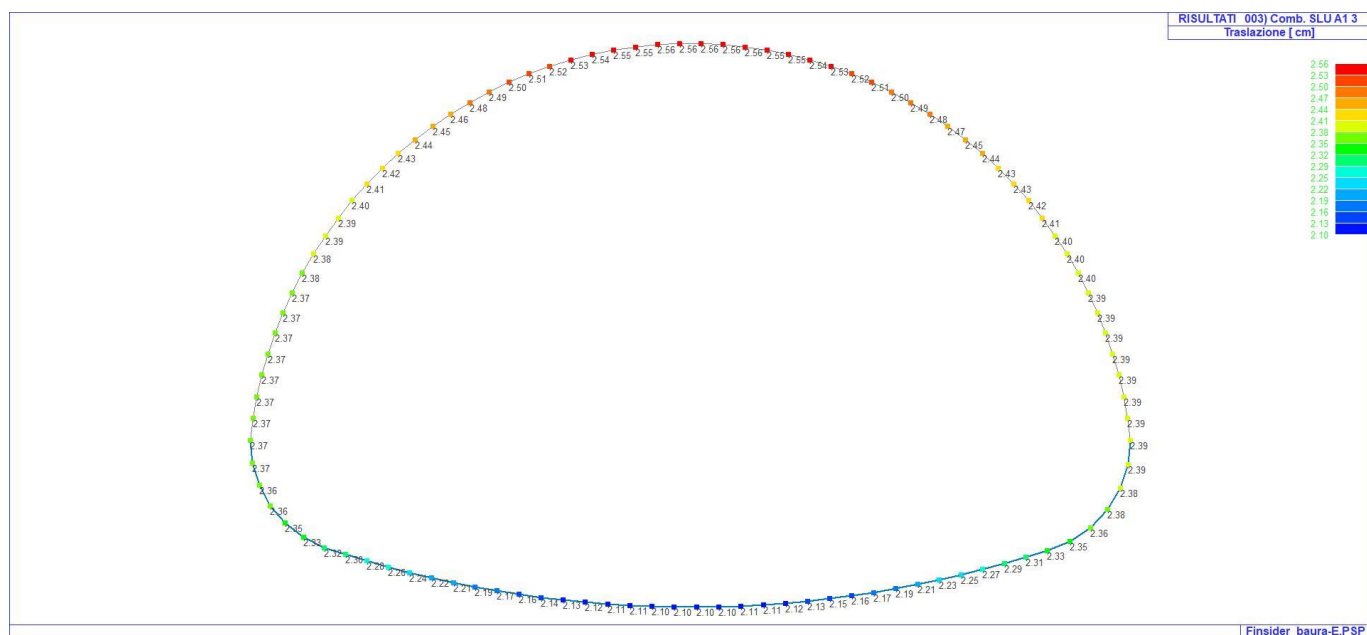
Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
61	17	0.73	0.0	-1.44	0.0	5.79e-03	0.0
61	19	0.06	0.0	-1.43	0.0	6.59e-04	0.0
61	20	0.55	0.0	-1.18	0.0	4.38e-03	0.0
61	21	0.02	0.0	-0.41	0.0	1.36e-04	0.0
62	3	0.09	0.0	-2.38	0.0	1.35e-03	0.0
62	9	0.91	0.0	-1.91	0.0	7.82e-03	0.0
62	12	0.15	0.0	-0.63	0.0	1.47e-03	0.0
62	14	0.07	0.0	-1.77	0.0	1.00e-03	0.0
62	17	0.67	0.0	-1.42	0.0	5.79e-03	0.0
62	19	0.06	0.0	-1.43	0.0	7.97e-04	0.0
62	20	0.51	0.0	-1.16	0.0	4.39e-03	0.0
62	21	0.02	0.0	-0.41	0.0	1.90e-04	0.0
63	3	0.08	0.0	-2.37	0.0	1.55e-03	0.0
63	9	0.83	0.0	-1.87	0.0	7.81e-03	0.0
63	12	0.13	0.0	-0.63	0.0	1.52e-03	0.0
63	14	0.06	0.0	-1.76	0.0	1.15e-03	0.0
63	17	0.62	0.0	-1.38	0.0	5.78e-03	0.0
63	19	0.05	0.0	-1.42	0.0	9.23e-04	0.0
63	20	0.47	0.0	-1.14	0.0	4.40e-03	0.0
63	21	0.01	0.0	-0.40	0.0	2.46e-04	0.0
64	3	0.06	0.0	-2.36	0.0	1.72e-03	0.0
64	9	0.77	0.0	-1.80	0.0	7.79e-03	0.0
64	12	0.12	0.0	-0.61	0.0	1.56e-03	0.0
64	14	0.05	0.0	-1.75	0.0	1.28e-03	0.0
64	17	0.57	0.0	-1.34	0.0	5.77e-03	0.0
64	19	0.04	0.0	-1.41	0.0	1.03e-03	0.0
64	20	0.43	0.0	-1.10	0.0	4.40e-03	0.0
64	21	0.01	0.0	-0.40	0.0	3.00e-04	0.0
65	3	0.05	0.0	-2.34	0.0	1.86e-03	0.0
65	9	0.72	0.0	-1.73	0.0	7.76e-03	0.0
65	12	0.11	0.0	-0.60	0.0	1.59e-03	0.0
65	14	0.04	0.0	-1.74	0.0	1.38e-03	0.0
65	17	0.53	0.0	-1.28	0.0	5.75e-03	0.0
65	19	0.03	0.0	-1.40	0.0	1.12e-03	0.0
65	20	0.40	0.0	-1.06	0.0	4.40e-03	0.0
65	21	0.01	0.0	-0.40	0.0	3.48e-04	0.0
66	3	0.05	0.0	-2.32	0.0	1.95e-03	0.0
66	9	0.68	0.0	-1.65	0.0	7.72e-03	0.0
66	12	0.10	0.0	-0.58	0.0	1.62e-03	0.0
66	14	0.03	0.0	-1.72	0.0	1.45e-03	0.0
66	17	0.51	0.0	-1.22	0.0	5.72e-03	0.0
66	19	0.03	0.0	-1.39	0.0	1.18e-03	0.0
66	20	0.38	0.0	-1.02	0.0	4.38e-03	0.0
66	21	9.35e-03	0.0	-0.40	0.0	3.87e-04	0.0
67	3	0.04	0.0	-2.31	0.0	2.00e-03	0.0
67	9	0.66	0.0	-1.58	0.0	7.67e-03	0.0
67	12	0.10	0.0	-0.57	0.0	1.63e-03	0.0
67	14	0.03	0.0	-1.71	0.0	1.48e-03	0.0
67	17	0.49	0.0	-1.17	0.0	5.68e-03	0.0
67	19	0.02	0.0	-1.38	0.0	1.21e-03	0.0
67	20	0.37	0.0	-0.97	0.0	4.36e-03	0.0
67	21	8.20e-03	0.0	-0.39	0.0	4.13e-04	0.0
68	3	0.03	0.0	-2.29	0.0	2.02e-03	0.0
68	9	0.64	0.0	-1.50	0.0	7.61e-03	0.0
68	12	0.09	0.0	-0.55	0.0	1.63e-03	0.0
68	14	0.02	0.0	-1.69	0.0	1.50e-03	0.0
68	17	0.47	0.0	-1.11	0.0	5.64e-03	0.0
68	19	0.02	0.0	-1.37	0.0	1.23e-03	0.0
68	20	0.36	0.0	-0.93	0.0	4.33e-03	0.0
68	21	7.06e-03	0.0	-0.39	0.0	4.30e-04	0.0
69	3	0.03	0.0	-2.27	0.0	2.01e-03	0.0
69	9	0.62	0.0	-1.43	0.0	7.54e-03	0.0
69	10	0.62	0.0	-1.29	0.0	7.39e-03	0.0
69	12	0.09	0.0	-0.53	0.0	1.63e-03	0.0
69	14	0.02	0.0	-1.68	0.0	1.49e-03	0.0
69	17	0.46	0.0	-1.06	0.0	5.59e-03	0.0
69	19	0.02	0.0	-1.35	0.0	1.23e-03	0.0
69	20	0.35	0.0	-0.89	0.0	4.30e-03	0.0
69	21	5.96e-03	0.0	-0.38	0.0	4.39e-04	0.0
70	3	0.02	0.0	-2.25	0.0	1.97e-03	0.0
70	9	0.60	0.0	-1.35	0.0	7.47e-03	0.0
70	12	0.09	0.0	-0.52	0.0	1.62e-03	0.0
70	14	0.02	0.0	-1.66	0.0	1.46e-03	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
70	17	0.45	0.0	-1.00	0.0	5.53e-03	0.0
70	19	0.01	0.0	-1.34	0.0	1.20e-03	0.0
70	20	0.34	0.0	-0.85	0.0	4.26e-03	0.0
70	21	4.93e-03	0.0	-0.38	0.0	4.40e-04	0.0
71	3	0.02	0.0	-2.23	0.0	1.91e-03	0.0
71	9	0.58	0.0	-1.28	0.0	7.40e-03	0.0
71	12	0.08	0.0	-0.50	0.0	1.60e-03	0.0
71	14	0.01	0.0	-1.65	0.0	1.41e-03	0.0
71	17	0.43	0.0	-0.95	0.0	5.48e-03	0.0
71	19	0.01	0.0	-1.33	0.0	1.17e-03	0.0
71	20	0.33	0.0	-0.80	0.0	4.22e-03	0.0
71	21	3.99e-03	0.0	-0.37	0.0	4.33e-04	0.0
72	3	0.01	0.0	-2.21	0.0	1.82e-03	0.0
72	9	0.57	0.0	-1.21	0.0	7.32e-03	0.0
72	12	0.08	0.0	-0.49	0.0	1.58e-03	0.0
72	14	0.01	0.0	-1.64	0.0	1.35e-03	0.0
72	17	0.42	0.0	-0.89	0.0	5.42e-03	0.0
72	19	9.00e-03	0.0	-1.32	0.0	1.12e-03	0.0
72	20	0.32	0.0	-0.76	0.0	4.17e-03	0.0
72	21	3.15e-03	0.0	-0.37	0.0	4.20e-04	0.0
73	3	0.01	0.0	-2.19	0.0	1.71e-03	0.0
73	9	0.55	0.0	-1.13	0.0	7.23e-03	0.0
73	12	0.08	0.0	-0.47	0.0	1.55e-03	0.0
73	14	8.45e-03	0.0	-1.62	0.0	1.27e-03	0.0
73	17	0.41	0.0	-0.84	0.0	5.36e-03	0.0
73	19	6.94e-03	0.0	-1.31	0.0	1.05e-03	0.0
73	20	0.31	0.0	-0.72	0.0	4.12e-03	0.0
73	21	2.42e-03	0.0	-0.37	0.0	4.01e-04	0.0
74	3	8.55e-03	0.0	-2.17	0.0	1.58e-03	0.0
74	9	0.54	0.0	-1.06	0.0	7.15e-03	0.0
74	12	0.07	0.0	-0.46	0.0	1.51e-03	0.0
74	14	6.33e-03	0.0	-1.61	0.0	1.17e-03	0.0
74	17	0.40	0.0	-0.79	0.0	5.30e-03	0.0
74	19	5.20e-03	0.0	-1.30	0.0	9.75e-04	0.0
74	20	0.30	0.0	-0.68	0.0	4.07e-03	0.0
74	21	1.80e-03	0.0	-0.36	0.0	3.76e-04	0.0
75	3	6.21e-03	0.0	-2.16	0.0	1.44e-03	0.0
75	9	0.53	0.0	-0.99	0.0	7.07e-03	0.0
75	12	0.07	0.0	-0.44	0.0	1.47e-03	0.0
75	14	4.60e-03	0.0	-1.60	0.0	1.07e-03	0.0
75	17	0.39	0.0	-0.73	0.0	5.24e-03	0.0
75	19	3.78e-03	0.0	-1.29	0.0	8.87e-04	0.0
75	20	0.30	0.0	-0.64	0.0	4.02e-03	0.0
75	21	1.30e-03	0.0	-0.36	0.0	3.47e-04	0.0
76	3	4.37e-03	0.0	-2.15	0.0	1.28e-03	0.0
76	9	0.52	0.0	-0.92	0.0	6.99e-03	0.0
76	12	0.07	0.0	-0.43	0.0	1.43e-03	0.0
76	14	3.24e-03	0.0	-1.59	0.0	9.48e-04	0.0
76	17	0.39	0.0	-0.68	0.0	5.18e-03	0.0
76	19	2.66e-03	0.0	-1.28	0.0	7.89e-04	0.0
76	20	0.29	0.0	-0.60	0.0	3.96e-03	0.0
76	21	9.13e-04	0.0	-0.36	0.0	3.12e-04	0.0
77	3	2.97e-03	0.0	-2.13	0.0	1.11e-03	0.0
77	9	0.51	0.0	-0.85	0.0	6.92e-03	0.0
77	12	0.07	0.0	-0.41	0.0	1.39e-03	0.0
77	14	2.20e-03	0.0	-1.58	0.0	8.19e-04	0.0
77	17	0.38	0.0	-0.63	0.0	5.12e-03	0.0
77	19	1.81e-03	0.0	-1.27	0.0	6.83e-04	0.0
77	20	0.29	0.0	-0.56	0.0	3.91e-03	0.0
77	21	6.27e-04	0.0	-0.35	0.0	2.75e-04	0.0
78	3	1.97e-03	0.0	-2.12	0.0	9.21e-04	0.0
78	9	0.51	0.0	-0.78	0.0	6.85e-03	0.0
78	12	0.07	0.0	-0.40	0.0	1.34e-03	0.0
78	14	1.46e-03	0.0	-1.57	0.0	6.82e-04	0.0
78	17	0.38	0.0	-0.58	0.0	5.07e-03	0.0
78	19	1.20e-03	0.0	-1.27	0.0	5.70e-04	0.0
78	20	0.28	0.0	-0.52	0.0	3.86e-03	0.0
78	21	4.35e-04	0.0	-0.35	0.0	2.34e-04	0.0
79	3	1.30e-03	0.0	-2.11	0.0	7.26e-04	0.0
79	9	0.50	0.0	-0.71	0.0	6.78e-03	0.0
79	12	0.07	0.0	-0.38	0.0	1.29e-03	0.0
79	14	9.62e-04	0.0	-1.57	0.0	5.38e-04	0.0
79	17	0.37	0.0	-0.53	0.0	5.02e-03	0.0

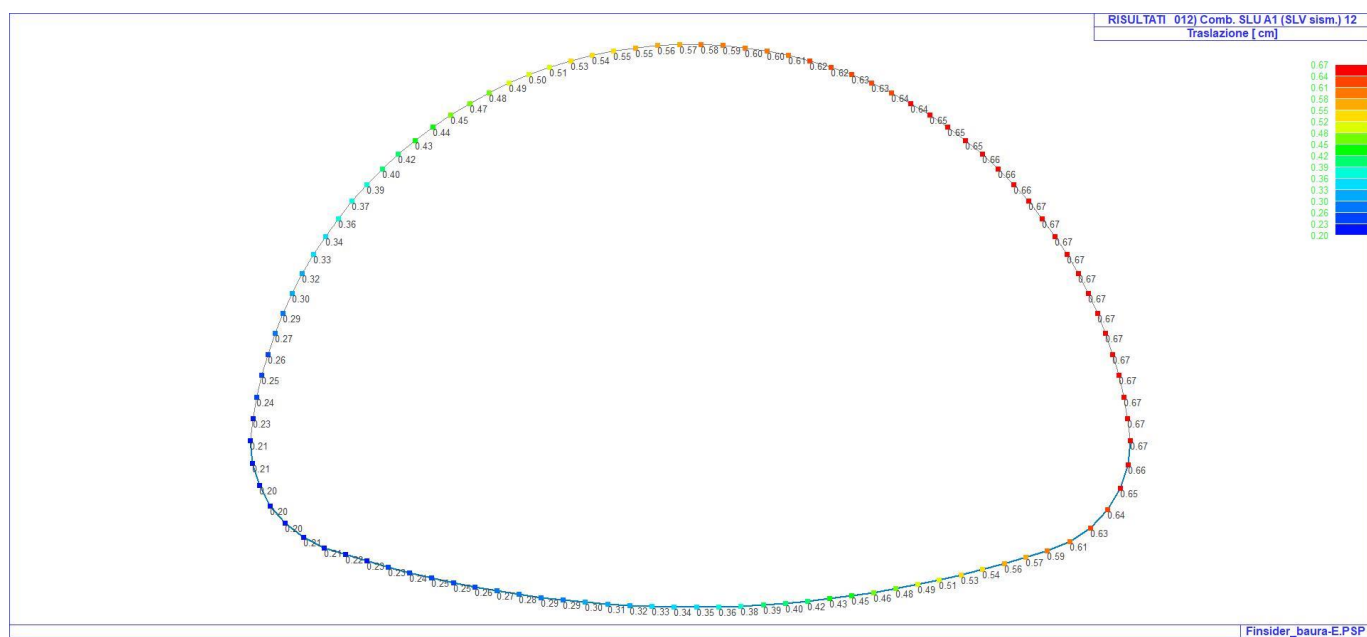
Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
79	19	8.02e-04	0.0	-1.26	0.0	4.51e-04	0.0
79	20	0.28	0.0	-0.48	0.0	3.81e-03	0.0
79	21	3.22e-04	0.0	-0.35	0.0	1.90e-04	0.0
80	3	8.95e-04	0.0	-2.11	0.0	5.25e-04	0.0
80	9	0.50	0.0	-0.64	0.0	6.72e-03	0.0
80	12	0.07	0.0	-0.37	0.0	1.24e-03	0.0
80	14	6.63e-04	0.0	-1.56	0.0	3.89e-04	0.0
80	17	0.37	0.0	-0.47	0.0	4.98e-03	0.0
80	19	5.66e-04	0.0	-1.26	0.0	3.28e-04	0.0
80	20	0.28	0.0	-0.44	0.0	3.77e-03	0.0
80	21	2.74e-04	0.0	-0.35	0.0	1.44e-04	0.0
81	3	6.83e-04	0.0	-2.10	0.0	3.19e-04	0.0
81	9	0.50	0.0	-0.57	0.0	6.66e-03	0.0
81	12	0.06	0.0	-0.36	0.0	1.19e-03	0.0
81	14	5.06e-04	0.0	-1.56	0.0	2.37e-04	0.0
81	17	0.37	0.0	-0.42	0.0	4.94e-03	0.0
81	19	4.48e-04	0.0	-1.26	0.0	2.02e-04	0.0
81	20	0.28	0.0	-0.40	0.0	3.73e-03	0.0
81	21	2.75e-04	0.0	-0.34	0.0	9.75e-05	0.0
82	3	5.83e-04	0.0	-2.10	0.0	1.11e-04	0.0
82	9	0.50	0.0	-0.50	0.0	6.62e-03	0.0
82	12	0.06	0.0	-0.35	0.0	1.14e-03	0.0
82	14	4.32e-04	0.0	-1.56	0.0	8.21e-05	0.0
82	17	0.37	0.0	-0.37	0.0	4.90e-03	0.0
82	19	4.00e-04	0.0	-1.25	0.0	7.40e-05	0.0
82	20	0.28	0.0	-0.37	0.0	3.69e-03	0.0
82	21	3.06e-04	0.0	-0.34	0.0	4.98e-05	0.0
83	3	5.15e-04	0.0	-2.10	0.0	-9.83e-05	0.0
83	9	0.50	0.0	-0.44	0.0	6.58e-03	0.0
83	12	0.06	0.0	-0.34	0.0	1.10e-03	0.0
83	14	3.82e-04	0.0	-1.56	0.0	-7.28e-05	0.0
83	17	0.37	0.0	-0.32	0.0	4.87e-03	0.0
83	19	3.73e-04	0.0	-1.25	0.0	-5.41e-05	0.0
83	20	0.28	0.0	-0.33	0.0	3.65e-03	0.0
83	21	3.48e-04	0.0	-0.34	0.0	1.90e-06	0.0
84	3	3.91e-04	0.0	-2.10	0.0	-3.06e-04	0.0
84	9	0.50	0.0	-0.37	0.0	6.55e-03	0.0
84	12	0.07	0.0	-0.32	0.0	1.05e-03	0.0
84	14	2.90e-04	0.0	-1.56	0.0	-2.27e-04	0.0
84	17	0.37	0.0	-0.27	0.0	4.85e-03	0.0
84	19	3.13e-04	0.0	-1.25	0.0	-1.81e-04	0.0
84	20	0.28	0.0	-0.29	0.0	3.63e-03	0.0
84	21	3.84e-04	0.0	-0.34	0.0	-4.55e-05	0.0
85	3	1.49e-04	0.0	-2.11	0.0	-5.10e-04	0.0
85	9	0.50	0.0	-0.30	0.0	6.53e-03	0.0
85	12	0.07	0.0	-0.31	0.0	1.01e-03	0.0
85	14	1.10e-04	0.0	-1.56	0.0	-3.78e-04	0.0
85	17	0.37	0.0	-0.23	0.0	4.84e-03	0.0
85	19	1.82e-04	0.0	-1.26	0.0	-3.06e-04	0.0
85	20	0.28	0.0	-0.26	0.0	3.60e-03	0.0
85	21	3.97e-04	0.0	-0.34	0.0	-9.19e-05	0.0
86	3	-2.98e-04	0.0	-2.11	0.0	-7.08e-04	0.0
86	9	0.51	0.0	-0.24	0.0	6.52e-03	0.0
86	12	0.07	0.0	-0.30	0.0	9.66e-04	0.0
86	14	-2.21e-04	0.0	-1.57	0.0	-5.24e-04	0.0
86	17	0.37	0.0	-0.18	0.0	4.83e-03	0.0
86	19	-7.34e-05	0.0	-1.26	0.0	-4.27e-04	0.0
86	20	0.28	0.0	-0.22	0.0	3.59e-03	0.0
86	21	3.68e-04	0.0	-0.35	0.0	-1.37e-04	0.0
87	3	-1.02e-03	0.0	-2.12	0.0	-8.98e-04	0.0
87	9	0.51	0.0	-0.17	0.0	6.52e-03	0.0
87	12	0.07	0.0	-0.29	0.0	9.29e-04	0.0
87	14	-7.56e-04	0.0	-1.57	0.0	-6.65e-04	0.0
87	17	0.38	0.0	-0.13	0.0	4.83e-03	0.0
87	19	-4.96e-04	0.0	-1.27	0.0	-5.44e-04	0.0
87	20	0.28	0.0	-0.18	0.0	3.58e-03	0.0
87	21	2.82e-04	0.0	-0.35	0.0	-1.79e-04	0.0
88	3	-2.08e-03	0.0	-2.13	0.0	-1.08e-03	0.0
88	9	0.52	0.0	-0.11	0.0	6.53e-03	0.0
88	12	0.07	0.0	-0.29	0.0	8.95e-04	0.0
88	14	-1.54e-03	0.0	-1.58	0.0	-7.99e-04	0.0
88	17	0.38	0.0	-0.08	0.0	4.84e-03	0.0
88	19	-1.13e-03	0.0	-1.27	0.0	-6.54e-04	0.0

Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
88	20	0.29	0.0	-0.15	0.0	3.57e-03	0.0
88	21	1.24e-04	0.0	-0.35	0.0	-2.19e-04	0.0
89	3	-3.55e-03	0.0	-2.14	0.0	-1.25e-03	0.0
89	10	0.53	0.0	0.08	0.0	6.64e-03	0.0
89	12	0.07	0.0	-0.28	0.0	8.67e-04	0.0
89	14	-2.63e-03	0.0	-1.59	0.0	-9.23e-04	0.0
89	17	0.39	0.0	-0.03	0.0	4.86e-03	0.0
89	19	-2.00e-03	0.0	-1.28	0.0	-7.56e-04	0.0
89	20	0.29	0.0	-0.11	0.0	3.58e-03	0.0
89	21	-1.18e-04	0.0	-0.35	0.0	-2.55e-04	0.0
90	3	-5.46e-03	0.0	-2.16	0.0	-1.40e-03	0.0
90	10	0.54	0.0	0.15	0.0	6.69e-03	0.0
90	12	0.07	0.0	-0.27	0.0	8.43e-04	0.0
90	14	-4.04e-03	0.0	-1.60	0.0	-1.04e-03	0.0
90	17	0.40	0.0	0.02	0.0	4.88e-03	0.0
90	19	-3.14e-03	0.0	-1.29	0.0	-8.49e-04	0.0
90	20	0.30	0.0	-0.07	0.0	3.59e-03	0.0
90	21	-4.52e-04	0.0	-0.35	0.0	-2.87e-04	0.0
91	3	-7.85e-03	0.0	-2.17	0.0	-1.54e-03	0.0
91	10	0.55	0.0	0.22	0.0	6.75e-03	0.0
91	12	0.07	0.0	-0.26	0.0	8.25e-04	0.0
91	14	-5.81e-03	0.0	-1.61	0.0	-1.14e-03	0.0
91	17	0.40	0.0	0.07	0.0	4.92e-03	0.0
91	19	-4.58e-03	0.0	-1.30	0.0	-9.33e-04	0.0
91	20	0.30	0.0	-0.04	0.0	3.61e-03	0.0
91	21	-8.85e-04	0.0	-0.36	0.0	-3.14e-04	0.0
92	3	-0.01	0.0	-2.19	0.0	-1.66e-03	0.0
92	10	0.56	0.0	0.29	0.0	6.81e-03	0.0
92	12	0.07	0.0	-0.25	0.0	8.13e-04	0.0
92	14	-7.96e-03	0.0	-1.62	0.0	-1.23e-03	0.0
92	17	0.41	0.0	0.12	0.0	4.96e-03	0.0
92	19	-6.32e-03	0.0	-1.31	0.0	-1.00e-03	0.0
92	20	0.31	0.0	-1.63e-03	0.0	3.64e-03	0.0
92	21	-1.42e-03	0.0	-0.36	0.0	-3.36e-04	0.0
93	3	-0.01	0.0	-2.21	0.0	-1.75e-03	0.0
93	10	0.57	0.0	0.35	0.0	6.89e-03	0.0
93	12	0.08	0.0	-0.24	0.0	8.08e-04	0.0
93	14	-0.01	0.0	-1.63	0.0	-1.30e-03	0.0
93	17	0.42	0.0	0.17	0.0	5.01e-03	0.0
93	19	-8.31e-03	0.0	-1.32	0.0	-1.06e-03	0.0
93	20	0.32	0.0	0.03	0.0	3.67e-03	0.0
93	21	-2.03e-03	0.0	-0.36	0.0	-3.53e-04	0.0
94	3	-0.02	0.0	-2.22	0.0	-1.83e-03	0.0
94	10	0.59	0.0	0.42	0.0	6.97e-03	0.0
94	12	0.08	0.0	-0.24	0.0	8.10e-04	0.0
94	14	-0.01	0.0	-1.65	0.0	-1.36e-03	0.0
94	17	0.43	0.0	0.22	0.0	5.07e-03	0.0
94	19	-0.01	0.0	-1.33	0.0	-1.11e-03	0.0
94	20	0.33	0.0	0.07	0.0	3.71e-03	0.0
94	21	-2.78e-03	0.0	-0.37	0.0	-3.63e-04	0.0
95	3	-0.02	0.0	-2.24	0.0	-1.88e-03	0.0
95	9	0.60	0.0	0.36	0.0	6.94e-03	0.0
95	10	0.60	0.0	0.49	0.0	7.07e-03	0.0
95	12	0.08	0.0	-0.23	0.0	8.19e-04	0.0
95	14	-0.02	0.0	-1.66	0.0	-1.40e-03	0.0
95	17	0.45	0.0	0.27	0.0	5.14e-03	0.0
95	19	-0.01	0.0	-1.34	0.0	-1.14e-03	0.0
95	20	0.33	0.0	0.11	0.0	3.77e-03	0.0
95	21	-3.59e-03	0.0	-0.37	0.0	-3.66e-04	0.0
96	3	-0.03	0.0	-2.26	0.0	-1.91e-03	0.0
96	9	0.62	0.0	0.43	0.0	7.05e-03	0.0
96	10	0.62	0.0	0.56	0.0	7.17e-03	0.0
96	12	0.08	0.0	-0.22	0.0	8.36e-04	0.0
96	14	-0.02	0.0	-1.67	0.0	-1.41e-03	0.0
96	17	0.46	0.0	0.32	0.0	5.22e-03	0.0
96	19	-0.02	0.0	-1.35	0.0	-1.15e-03	0.0
96	20	0.34	0.0	0.15	0.0	3.82e-03	0.0
96	21	-4.46e-03	0.0	-0.38	0.0	-3.61e-04	0.0
97	3	-0.03	0.0	-2.28	0.0	-1.91e-03	0.0
97	10	0.64	0.0	0.63	0.0	7.29e-03	0.0
97	12	0.08	0.0	-0.21	0.0	8.61e-04	0.0
97	14	-0.02	0.0	-1.69	0.0	-1.41e-03	0.0
97	17	0.48	0.0	0.37	0.0	5.31e-03	0.0

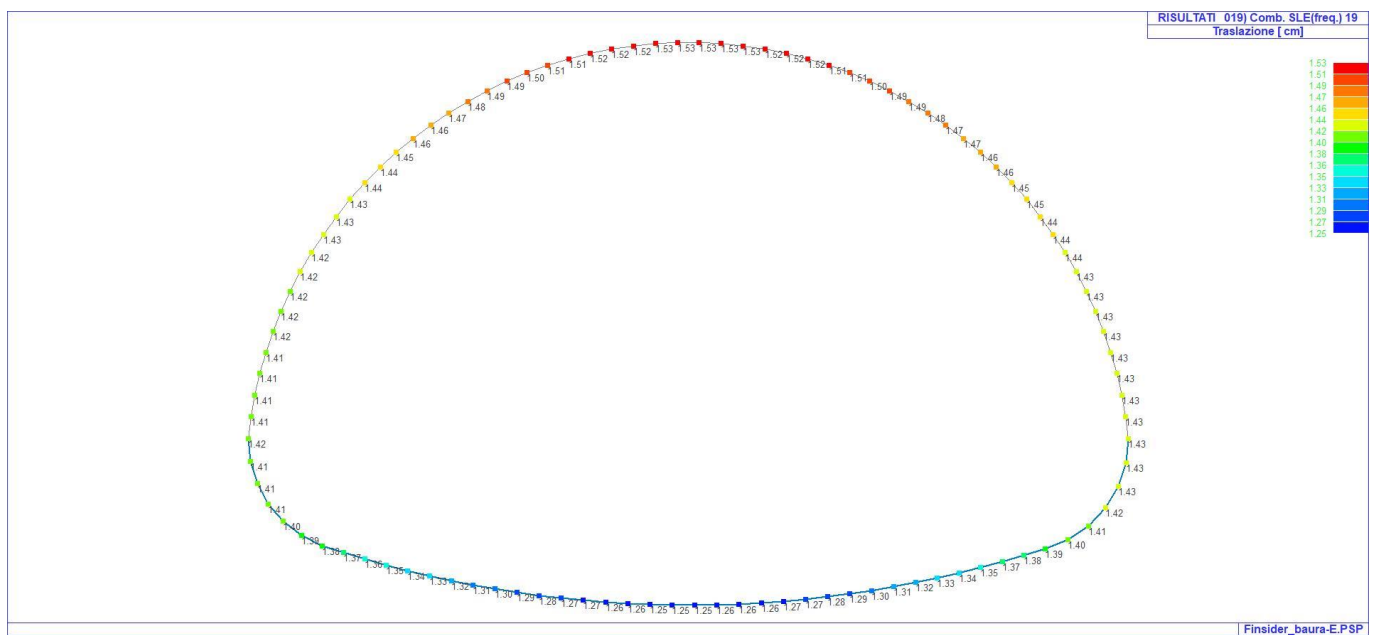
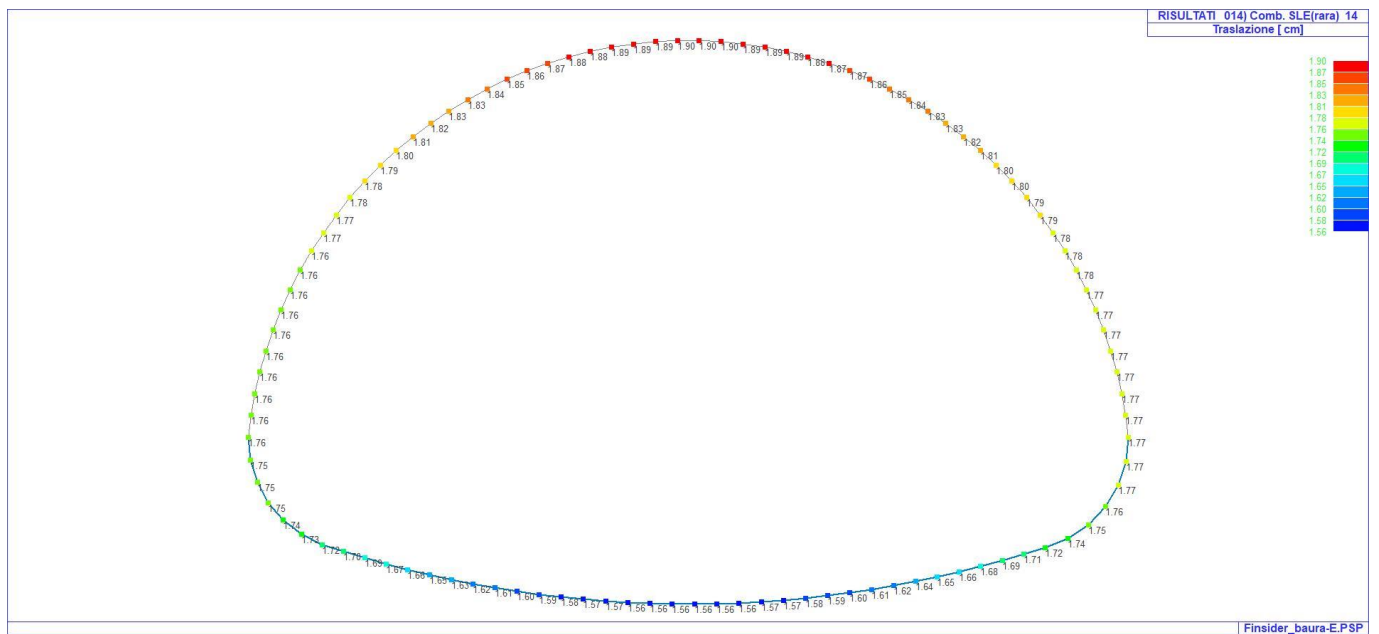
Nodo	Cmb	Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
97	19	-0.02	0.0	-1.36	0.0	-1.15e-03	0.0
97	20	0.35	0.0	0.18	0.0	3.89e-03	0.0
97	21	-5.37e-03	0.0	-0.38	0.0	-3.49e-04	0.0
98	3	-0.04	0.0	-2.30	0.0	-1.87e-03	0.0
98	10	0.66	0.0	0.70	0.0	7.41e-03	0.0
98	12	0.09	0.0	-0.20	0.0	8.96e-04	0.0
98	14	-0.03	0.0	-1.70	0.0	-1.39e-03	0.0
98	17	0.49	0.0	0.42	0.0	5.40e-03	0.0
98	19	-0.02	0.0	-1.37	0.0	-1.12e-03	0.0
98	20	0.37	0.0	0.22	0.0	3.97e-03	0.0
98	21	-6.31e-03	0.0	-0.38	0.0	-3.28e-04	0.0
99	3	-0.04	0.0	-2.32	0.0	-1.81e-03	0.0
99	10	0.69	0.0	0.78	0.0	7.54e-03	0.0
99	12	0.09	0.0	-0.19	0.0	9.39e-04	0.0
99	14	-0.03	0.0	-1.71	0.0	-1.34e-03	0.0
99	17	0.51	0.0	0.48	0.0	5.50e-03	0.0
99	19	-0.03	0.0	-1.38	0.0	-1.08e-03	0.0
99	20	0.38	0.0	0.26	0.0	4.05e-03	0.0
99	21	-7.22e-03	0.0	-0.39	0.0	-2.98e-04	0.0
100	3	-0.05	0.0	-2.33	0.0	-1.71e-03	0.0
100	10	0.72	0.0	0.85	0.0	7.67e-03	0.0
100	12	0.09	0.0	-0.18	0.0	9.93e-04	0.0
100	14	-0.04	0.0	-1.73	0.0	-1.27e-03	0.0
100	17	0.53	0.0	0.53	0.0	5.62e-03	0.0
100	19	-0.03	0.0	-1.39	0.0	-1.01e-03	0.0
100	20	0.40	0.0	0.30	0.0	4.15e-03	0.0
100	21	-8.46e-03	0.0	-0.39	0.0	-2.58e-04	0.0
101	3	-0.06	0.0	-2.35	0.0	-1.57e-03	0.0
101	10	0.77	0.0	0.91	0.0	7.81e-03	0.0
101	12	0.10	0.0	-0.18	0.0	1.05e-03	0.0
101	14	-0.05	0.0	-1.74	0.0	-1.16e-03	0.0
101	17	0.57	0.0	0.58	0.0	5.73e-03	0.0
101	19	-0.04	0.0	-1.40	0.0	-9.26e-04	0.0
101	20	0.43	0.0	0.33	0.0	4.24e-03	0.0
101	21	-9.92e-03	0.0	-0.39	0.0	-2.11e-04	0.0
102	3	-0.07	0.0	-2.36	0.0	-1.40e-03	0.0
102	10	0.84	0.0	0.97	0.0	7.93e-03	0.0
102	12	0.11	0.0	-0.17	0.0	1.12e-03	0.0
102	14	-0.06	0.0	-1.75	0.0	-1.04e-03	0.0
102	17	0.62	0.0	0.62	0.0	5.83e-03	0.0
102	19	-0.04	0.0	-1.41	0.0	-8.20e-04	0.0
102	20	0.46	0.0	0.36	0.0	4.33e-03	0.0
102	21	-0.01	0.0	-0.39	0.0	-1.60e-04	0.0
103	3	-0.09	0.0	-2.36	0.0	-1.21e-03	0.0
103	10	0.91	0.0	1.01	0.0	8.03e-03	0.0
103	12	0.12	0.0	-0.16	0.0	1.18e-03	0.0
103	14	-0.06	0.0	-1.75	0.0	-8.98e-04	0.0
103	17	0.67	0.0	0.64	0.0	5.92e-03	0.0
103	19	-0.05	0.0	-1.41	0.0	-7.00e-04	0.0
103	20	0.50	0.0	0.39	0.0	4.41e-03	0.0
103	21	-0.01	0.0	-0.39	0.0	-1.08e-04	0.0
104	3	-0.10	0.0	-2.37	0.0	-1.00e-03	0.0
104	10	0.99	0.0	1.03	0.0	8.10e-03	0.0
104	12	0.13	0.0	-0.16	0.0	1.23e-03	0.0
104	14	-0.07	0.0	-1.75	0.0	-7.41e-04	0.0
104	17	0.73	0.0	0.66	0.0	5.99e-03	0.0
104	19	-0.06	0.0	-1.41	0.0	-5.70e-04	0.0
104	20	0.55	0.0	0.40	0.0	4.48e-03	0.0
104	21	-0.01	0.0	-0.39	0.0	-5.77e-05	0.0
Nodo		Traslazione X	Traslazione Y	Traslazione Z	Rotazione X	Rotazione Y	Rotazione Z
		-0.12	0.0	-2.56	0.0	-1.91e-03	0.0
		2.44	0.0	1.04	0.0	8.17e-03	0.0



41\_RIS\_SPOSTAMENTI\_003\_Comb. SLU A1 3



41\_RIS\_SPOSTAMENTI\_012\_Comb. SLU A1 (SLV sism.) 12







# RISULTATI ELEMENTI TIPO TRAVE

## LEGENDA RISULTATI ELEMENTI TIPO TRAVE

Il controllo dei risultati delle analisi condotte, per quanto concerne gli elementi tipo trave, è possibile in relazione alle tabelle sotto riportate.

Gli elementi vengono suddivisi in relazione alle proprietà in elementi:

- tipo **pilastro**
- tipo **trave in elevazione**
- tipo **trave in fondazione**

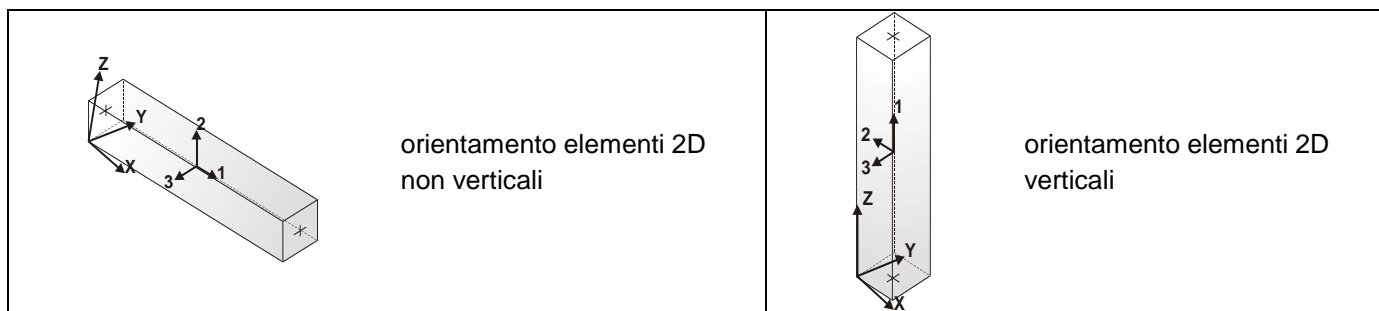
Per ogni elemento e per ogni combinazione (o caso di carico) vengono riportati i risultati più significativi.

Per gli elementi tipo *pilastro* sono riportati in tabella i seguenti valori:

<b>Pilas.</b>	numero dell'elemento pilastro
<b>Cmb</b>	combinazione in cui si verificano i valori riportati
<b>M3 mx/mn</b>	momento flettente in campata M3 max (prima riga) / min (seconda riga)
<b>M2 mx/mn</b>	momento flettente in campata M2 max (prima riga) / min (seconda riga)
<b>D2/D3</b>	freccia massima in direzione 2 (prima riga) / direzione 3 (seconda riga)
<b>Q2/Q3</b>	carico totale in direzione 2 (prima riga) / direzione 3 (seconda riga)
<b>Pos.</b>	ascissa del punto iniziale e finale dell'elemento
<b>N, V2, ecc..</b>	sei componenti di sollecitazione al piede ed in sommità dell'elemento

Per gli elementi tipo *trave in elevazione* sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri.

Per gli elementi tipo *trave in fondazione* (trave f.) sono riportati, oltre al numero dell'elemento, i medesimi risultati visti per i pilastri e la massima pressione sul terreno.



Trave	Cmb	M3 mx/mn kN m	M2 mx/mn kN m	D 2 / D 3 m	Q 2 / Q 3 kN	Pos. cm	N kN	V 2 kN	V 3 kN	T kN m	M 2 kN m	M 3 kN m
1	3	-91.29	0.0	6.67e-05	-10.37	0.0	-257.54	28.27	0.0	0.0	0.0	-93.61
		-93.61	0.0	0.0	0.0	10.0	-258.05	17.90	0.0	0.0	0.0	-91.29
1	4	-85.98	0.0	6.73e-05	-7.68	0.0	-230.96	16.47	0.0	0.0	0.0	-87.25
		-87.25	0.0	0.0	0.0	10.0	-231.34	8.79	0.0	0.0	0.0	-85.98
1	9	-6.59	0.0	-8.24e-04	-16.91	0.0	-67.84	135.06	0.0	0.0	0.0	-19.31
		-19.31	0.0	0.0	0.0	10.0	-69.22	118.15	0.0	0.0	0.0	-6.59
1	10	-1.28	0.0	-8.24e-04	-14.22	0.0	-41.26	123.27	0.0	0.0	0.0	-12.95
		-12.95	0.0	0.0	0.0	10.0	-42.50	109.05	0.0	0.0	0.0	-1.28
1	12	-15.75	0.0	-1.33e-04	-7.68	0.0	-69.64	42.33	0.0	0.0	0.0	-19.62
		-19.62	0.0	0.0	0.0	10.0	-70.02	34.65	0.0	0.0	0.0	-15.75
1	14	-67.62	0.0	4.94e-05	-7.68	0.0	-190.77	20.94	0.0	0.0	0.0	-69.34
		-69.34	0.0	0.0	0.0	10.0	-191.15	13.26	0.0	0.0	0.0	-67.62
1	17	-4.88	0.0	-6.11e-04	-12.52	0.0	-50.25	100.04	0.0	0.0	0.0	-14.31
		-14.31	0.0	0.0	0.0	10.0	-51.27	87.52	0.0	0.0	0.0	-4.88
1	19	-54.52	0.0	3.66e-05	-7.68	0.0	-162.07	24.13	0.0	0.0	0.0	-56.55
		-56.55	0.0	0.0	0.0	10.0	-162.45	16.45	0.0	0.0	0.0	-54.52
1	20	-7.46	0.0	-4.58e-04	-11.31	0.0	-56.68	83.46	0.0	0.0	0.0	-15.28
		-15.28	0.0	0.0	0.0	10.0	-57.54	72.14	0.0	0.0	0.0	-7.46
1	21	-15.19	0.0	-1.85e-06	-7.68	0.0	-75.95	33.69	0.0	0.0	0.0	-18.19
		-18.19	0.0	0.0	0.0	10.0	-76.33	26.01	0.0	0.0	0.0	-15.19
2	3	-88.72	0.0	4.56e-05	-10.07	0.0	-256.85	30.68	0.0	0.0	0.0	-91.29
		-91.29	0.0	0.0	0.0	10.0	-257.83	20.61	0.0	0.0	0.0	-88.72
2	4	-84.32	0.0	4.74e-05	-7.46	0.0	-230.62	20.26	0.0	0.0	0.0	-85.98
		-85.98	0.0	0.0	0.0	10.0	-231.34	12.80	0.0	0.0	0.0	-84.32
2	9	4.76	0.0	-8.25e-04	-16.97	0.0	-63.27	121.44	0.0	0.0	0.0	-6.59
		-6.59	0.0	0.0	0.0	10.0	-65.50	104.48	0.0	0.0	0.0	4.76
2	10	9.16	0.0	-8.24e-04	-14.35	0.0	-37.03	111.02	0.0	0.0	0.0	-1.28
		-1.28	0.0	0.0	0.0	10.0	-39.02	96.67	0.0	0.0	0.0	9.16
2	12	-12.33	0.0	-1.36e-04	-7.46	0.0	-68.26	37.85	0.0	0.0	0.0	-15.75
		-15.75	0.0	0.0	0.0	10.0	-68.98	30.39	0.0	0.0	0.0	-12.33
2	14	-65.72	0.0	3.38e-05	-7.46	0.0	-190.26	22.73	0.0	0.0	0.0	-67.62
		-67.62	0.0	0.0	0.0	10.0	-190.98	15.27	0.0	0.0	0.0	-65.72
2	17	3.52	0.0	-6.11e-04	-12.57	0.0	-46.86	89.96	0.0	0.0	0.0	-4.88
		-4.88	0.0	0.0	0.0	10.0	-48.52	77.39	0.0	0.0	0.0	3.52
2	19	-52.43	0.0	2.40e-05	-7.46	0.0	-161.43	24.49	0.0	0.0	0.0	-54.52
		-54.52	0.0	0.0	0.0	10.0	-162.15	17.03	0.0	0.0	0.0	-52.43
2	20	-0.50	0.0	-4.60e-04	-11.29	0.0	-53.88	74.91	0.0	0.0	0.0	-7.46
		-7.46	0.0	0.0	0.0	10.0	-55.31	63.62	0.0	0.0	0.0	-0.50
2	21	-12.57	0.0	-5.22e-06	-7.46	0.0	-74.95	29.77	0.0	0.0	0.0	-15.19
		-15.19	0.0	0.0	0.0	10.0	-75.67	22.31	0.0	0.0	0.0	-12.57
3	3	-85.86	0.0	2.50e-05	-9.76	0.0	-256.48	33.38	0.0	0.0	0.0	-88.72
		-88.72	0.0	0.0	0.0	10.0	-257.90	23.62	0.0	0.0	0.0	-85.86
3	4	-82.25	0.0	2.78e-05	-7.23	0.0	-230.42	24.27	0.0	0.0	0.0	-84.32
		-84.32	0.0	0.0	0.0	10.0	-231.47	17.03	0.0	0.0	0.0	-82.25
3	9	14.72	0.0	-8.24e-04	-16.98	0.0	-60.24	107.60	0.0	0.0	0.0	4.76
		4.76	0.0	0.0	0.0	10.0	-63.35	90.62	0.0	0.0	0.0	14.72
3	10	18.33	0.0	-8.21e-04	-14.45	0.0	-34.17	98.49	0.0	0.0	0.0	9.16
		9.16	0.0	0.0	0.0	10.0	-36.91	84.04	0.0	0.0	0.0	18.33
3	12	-9.32	0.0	-1.39e-04	-7.23	0.0	-67.44	33.54	0.0	0.0	0.0	-12.33
		-12.33	0.0	0.0	0.0	10.0	-68.49	26.30	0.0	0.0	0.0	-9.32
3	14	-63.60	0.0	1.85e-05	-7.23	0.0	-189.99	24.73	0.0	0.0	0.0	-65.72
		-65.72	0.0	0.0	0.0	10.0	-191.04	17.49	0.0	0.0	0.0	-63.60
3	17	10.90	0.0	-6.10e-04	-12.58	0.0	-44.62	79.70	0.0	0.0	0.0	3.52
		3.52	0.0	0.0	0.0	10.0	-46.92	67.12	0.0	0.0	0.0	10.90
3	19	-50.28	0.0	1.19e-05	-7.23	0.0	-161.11	25.05	0.0	0.0	0.0	-52.43
		-52.43	0.0	0.0	0.0	10.0	-162.16	17.82	0.0	0.0	0.0	-50.28
3	20	5.60	0.0	-4.60e-04	-11.24	0.0	-52.08	66.29	0.0	0.0	0.0	-0.50
		-0.50	0.0	0.0	0.0	10.0	-54.07	55.04	0.0	0.0	0.0	5.60
3	21	-10.32	0.0	-8.00e-06	-7.23	0.0	-74.47	26.04	0.0	0.0	0.0	-12.57
		-12.57	0.0	0.0	0.0	10.0	-75.52	18.81	0.0	0.0	0.0	-10.32
4	2	-8.41	0.0	-1.03e-05	-6.99	0.0	-74.49	22.53	0.0	0.0	0.0	-10.32
		-10.32	0.0	0.0	0.0	10.0	-75.85	15.54	0.0	0.0	0.0	-8.41
4	3	-82.68	0.0	5.64e-06	-9.44	0.0	-256.41	36.39	0.0	0.0	0.0	-85.86
		-85.86	0.0	0.0	0.0	10.0	-258.24	26.95	0.0	0.0	0.0	-82.68
4	9	23.28	0.0	-8.20e-04	-16.95	0.0	-58.77	93.65	0.0	0.0	0.0	14.72
		14.72	0.0	0.0	0.0	10.0	-62.76	76.70	0.0	0.0	0.0	23.28
4	10	26.22	0.0	-8.16e-04	-14.50	0.0	-32.70	85.77	0.0	0.0	0.0	18.33
		18.33	0.0	0.0	0.0	10.0	-36.21	71.26	0.0	0.0	0.0	26.22
4	12	-6.72	0.0	-1.41e-04	-6.99	0.0	-67.17	29.43	0.0	0.0	0.0	-9.32
		-9.32	0.0	0.0	0.0	10.0	-68.53	22.44	0.0	0.0	0.0	-6.72

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
4	13	-8.41	0.0	-1.03e-05	-6.99	0.0	-74.49	22.53	0.0	0.0	0.0	-10.32
		-10.32	0.0	0.0	0.0	10.0	-75.85	15.54	0.0	0.0	0.0	-8.41
4	14	-61.24	0.0	4.17e-06	-6.99	0.0	-189.93	26.95	0.0	0.0	0.0	-63.60
		-63.60	0.0	0.0	0.0	10.0	-191.29	19.97	0.0	0.0	0.0	-61.24
4	17	17.24	0.0	-6.07e-04	-12.55	0.0	-43.53	69.37	0.0	0.0	0.0	10.90
		10.90	0.0	0.0	0.0	10.0	-46.49	56.82	0.0	0.0	0.0	17.24
4	18	-8.41	0.0	-1.03e-05	-6.99	0.0	-74.49	22.53	0.0	0.0	0.0	-10.32
		-10.32	0.0	0.0	0.0	10.0	-75.85	15.54	0.0	0.0	0.0	-8.41
4	19	-48.04	0.0	1.53e-06	-6.99	0.0	-161.07	25.85	0.0	0.0	0.0	-50.28
		-50.28	0.0	0.0	0.0	10.0	-162.43	18.86	0.0	0.0	0.0	-48.04
4	20	10.83	0.0	-4.58e-04	-11.16	0.0	-51.27	57.66	0.0	0.0	0.0	5.60
		5.60	0.0	0.0	0.0	10.0	-53.83	46.50	0.0	0.0	0.0	10.83
4	21	-8.41	0.0	-1.03e-05	-6.99	0.0	-74.49	22.53	0.0	0.0	0.0	-10.32
		-10.32	0.0	0.0	0.0	10.0	-75.85	15.54	0.0	0.0	0.0	-8.41
5	2	-6.81	0.0	-1.21e-05	-6.74	0.0	-74.99	19.29	0.0	0.0	0.0	-8.41
		-8.41	0.0	0.0	0.0	10.0	-76.63	12.55	0.0	0.0	0.0	-6.81
5	3	-79.14	0.0	-1.40e-05	-9.10	0.0	-256.59	39.74	0.0	0.0	0.0	-82.68
		-82.68	0.0	0.0	0.0	10.0	-258.80	30.64	0.0	0.0	0.0	-79.14
5	9	30.44	0.0	-8.14e-04	-16.87	0.0	-58.88	79.72	0.0	0.0	0.0	23.28
		23.28	0.0	0.0	0.0	10.0	-63.75	62.86	0.0	0.0	0.0	30.44
5	10	32.82	0.0	-8.10e-04	-14.51	0.0	-32.63	72.97	0.0	0.0	0.0	26.22
		26.22	0.0	0.0	0.0	10.0	-36.93	58.47	0.0	0.0	0.0	32.82
5	12	-4.49	0.0	-1.42e-04	-6.74	0.0	-67.41	25.57	0.0	0.0	0.0	-6.72
		-6.72	0.0	0.0	0.0	10.0	-69.06	18.83	0.0	0.0	0.0	-4.49
5	13	-6.81	0.0	-1.21e-05	-6.74	0.0	-74.99	19.29	0.0	0.0	0.0	-8.41
		-8.41	0.0	0.0	0.0	10.0	-76.63	12.55	0.0	0.0	0.0	-6.81
5	14	-58.63	0.0	-1.04e-05	-6.74	0.0	-190.06	29.43	0.0	0.0	0.0	-61.24
		-61.24	0.0	0.0	0.0	10.0	-191.70	22.70	0.0	0.0	0.0	-58.63
5	17	22.55	0.0	-6.03e-04	-12.49	0.0	-43.61	59.05	0.0	0.0	0.0	17.24
		17.24	0.0	0.0	0.0	10.0	-47.22	46.56	0.0	0.0	0.0	22.55
5	18	-6.81	0.0	-1.21e-05	-6.74	0.0	-74.99	19.29	0.0	0.0	0.0	-8.41
		-8.41	0.0	0.0	0.0	10.0	-76.63	12.55	0.0	0.0	0.0	-6.81
5	19	-45.67	0.0	-1.08e-05	-6.74	0.0	-161.29	26.90	0.0	0.0	0.0	-48.04
		-48.04	0.0	0.0	0.0	10.0	-162.93	20.16	0.0	0.0	0.0	-45.67
5	20	15.21	0.0	-4.55e-04	-11.05	0.0	-51.45	49.11	0.0	0.0	0.0	10.83
		10.83	0.0	0.0	0.0	10.0	-54.57	38.06	0.0	0.0	0.0	15.21
5	21	-6.81	0.0	-1.21e-05	-6.74	0.0	-74.99	19.29	0.0	0.0	0.0	-8.41
		-8.41	0.0	0.0	0.0	10.0	-76.63	12.55	0.0	0.0	0.0	-6.81
6	3	-75.22	0.0	-3.24e-05	-8.75	0.0	-256.96	43.45	0.0	0.0	0.0	-79.14
		-79.14	0.0	0.0	0.0	10.0	-259.53	34.70	0.0	0.0	0.0	-75.22
6	4	-73.30	0.0	-2.76e-05	-6.48	0.0	-230.39	37.73	0.0	0.0	0.0	-76.76
		-76.76	0.0	0.0	0.0	10.0	-232.30	31.25	0.0	0.0	0.0	-73.30
6	9	36.22	0.0	-8.07e-04	-16.74	0.0	-60.55	65.94	0.0	0.0	0.0	30.44
		30.44	0.0	0.0	0.0	10.0	-66.31	49.21	0.0	0.0	0.0	36.22
6	10	38.15	0.0	-8.02e-04	-14.47	0.0	-33.98	60.23	0.0	0.0	0.0	32.82
		32.82	0.0	0.0	0.0	10.0	-39.07	45.76	0.0	0.0	0.0	38.15
6	12	-2.61	0.0	-1.43e-04	-6.48	0.0	-68.13	21.99	0.0	0.0	0.0	-4.49
		-4.49	0.0	0.0	0.0	10.0	-70.04	15.51	0.0	0.0	0.0	-2.61
6	14	-55.72	0.0	-2.40e-05	-6.48	0.0	-190.34	32.18	0.0	0.0	0.0	-58.63
		-58.63	0.0	0.0	0.0	10.0	-192.25	25.70	0.0	0.0	0.0	-55.72
6	17	26.83	0.0	-5.98e-04	-12.40	0.0	-44.85	48.85	0.0	0.0	0.0	22.55
		22.55	0.0	0.0	0.0	10.0	-49.12	36.45	0.0	0.0	0.0	26.83
6	19	-43.16	0.0	-2.14e-05	-6.48	0.0	-161.73	28.22	0.0	0.0	0.0	-45.67
		-45.67	0.0	0.0	0.0	10.0	-163.64	21.74	0.0	0.0	0.0	-43.16
6	20	18.75	0.0	-4.52e-04	-10.92	0.0	-52.62	40.72	0.0	0.0	0.0	15.21
		15.21	0.0	0.0	0.0	10.0	-56.29	29.80	0.0	0.0	0.0	18.75
6	21	-5.50	0.0	-1.36e-05	-6.48	0.0	-75.91	16.34	0.0	0.0	0.0	-6.81
		-6.81	0.0	0.0	0.0	10.0	-77.81	9.86	0.0	0.0	0.0	-5.50
7	2	-4.44	0.0	-1.48e-05	-6.21	0.0	-77.23	13.71	0.0	0.0	0.0	-5.50
		-5.50	0.0	0.0	0.0	10.0	-79.38	7.50	0.0	0.0	0.0	-4.44
7	3	-70.87	0.0	-4.99e-05	-8.39	0.0	-257.49	47.54	0.0	0.0	0.0	-75.22
		-75.22	0.0	0.0	0.0	10.0	-260.39	39.15	0.0	0.0	0.0	-70.87
7	9	40.66	0.0	-7.98e-04	-16.56	0.0	-63.78	52.44	0.0	0.0	0.0	36.22
		36.22	0.0	0.0	0.0	10.0	-70.42	35.88	0.0	0.0	0.0	40.66
7	10	42.21	0.0	-7.93e-04	-14.38	0.0	-36.75	47.64	0.0	0.0	0.0	38.15
		38.15	0.0	0.0	0.0	10.0	-42.64	33.26	0.0	0.0	0.0	42.21
7	12	-1.04	0.0	-1.44e-04	-6.21	0.0	-69.30	18.72	0.0	0.0	0.0	-2.61
		-2.61	0.0	0.0	0.0	10.0	-71.45	12.51	0.0	0.0	0.0	-1.04
7	13	-4.44	0.0	-1.48e-05	-6.21	0.0	-77.23	13.71	0.0	0.0	0.0	-5.50
		-5.50	0.0	0.0	0.0	10.0	-79.38	7.50	0.0	0.0	0.0	-4.44
7	14	-52.49	0.0	-3.69e-05	-6.21	0.0	-190.73	35.21	0.0	0.0	0.0	-55.72
		-55.72	0.0	0.0	0.0	10.0	-192.88	29.00	0.0	0.0	0.0	-52.49
7	17	30.12	0.0	-5.91e-04	-12.26	0.0	-47.25	38.84	0.0	0.0	0.0	26.83

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
7	18	26.83	0.0	0.0	0.0	10.0	-52.16	26.58	0.0	0.0	0.0	30.12
		-4.44	0.0	-1.48e-05	-6.21	0.0	-77.23	13.71	0.0	0.0	0.0	-5.50
		-5.50	0.0	0.0	0.0	10.0	-79.38	7.50	0.0	0.0	0.0	-4.44
7	19	-40.48	0.0	-3.14e-05	-6.21	0.0	-162.36	29.84	0.0	0.0	0.0	-43.16
		-43.16	0.0	0.0	0.0	10.0	-164.51	23.62	0.0	0.0	0.0	-40.48
7	20	21.48	0.0	-4.47e-04	-10.75	0.0	-54.74	32.56	0.0	0.0	0.0	18.75
		18.75	0.0	0.0	0.0	10.0	-58.97	21.81	0.0	0.0	0.0	21.48
7	21	-4.44	0.0	-1.48e-05	-6.21	0.0	-77.23	13.71	0.0	0.0	0.0	-5.50
		-5.50	0.0	0.0	0.0	10.0	-79.38	7.50	0.0	0.0	0.0	-4.44
8	2	-3.59	0.0	-1.57e-05	-5.94	0.0	-78.91	11.43	0.0	0.0	0.0	-4.44
		-4.44	0.0	0.0	0.0	10.0	-81.28	5.48	0.0	0.0	0.0	-3.59
8	3	-66.05	0.0	-6.63e-05	-8.02	0.0	-258.13	52.03	0.0	0.0	0.0	-70.87
		-70.87	0.0	0.0	0.0	10.0	-261.34	44.01	0.0	0.0	0.0	-66.05
8	9	43.79	0.0	-7.88e-04	-16.33	0.0	-68.55	39.33	0.0	0.0	0.0	40.66
		40.66	0.0	0.0	0.0	10.0	-76.07	23.00	0.0	0.0	0.0	43.79
8	10	45.05	0.0	-7.83e-04	-14.25	0.0	-40.93	35.33	0.0	0.0	0.0	42.21
		42.21	0.0	0.0	0.0	10.0	-47.62	21.08	0.0	0.0	0.0	45.05
8	12	0.25	0.0	-1.44e-04	-5.94	0.0	-70.87	15.79	0.0	0.0	0.0	-1.04
		-1.04	0.0	0.0	0.0	10.0	-73.24	9.84	0.0	0.0	0.0	0.25
8	13	-3.59	0.0	-1.57e-05	-5.94	0.0	-78.91	11.43	0.0	0.0	0.0	-4.44
		-4.44	0.0	0.0	0.0	10.0	-81.28	5.48	0.0	0.0	0.0	-3.59
8	14	-48.92	0.0	-4.91e-05	-5.94	0.0	-191.21	38.54	0.0	0.0	0.0	-52.49
		-52.49	0.0	0.0	0.0	10.0	-193.58	32.60	0.0	0.0	0.0	-48.92
8	17	32.44	0.0	-5.84e-04	-12.10	0.0	-50.78	29.13	0.0	0.0	0.0	30.12
		30.12	0.0	0.0	0.0	10.0	-56.35	17.04	0.0	0.0	0.0	32.44
8	18	-3.59	0.0	-1.57e-05	-5.94	0.0	-78.91	11.43	0.0	0.0	0.0	-4.44
		-4.44	0.0	0.0	0.0	10.0	-81.28	5.48	0.0	0.0	0.0	-3.59
8	19	-37.59	0.0	-4.08e-05	-5.94	0.0	-163.13	31.76	0.0	0.0	0.0	-40.48
		-40.48	0.0	0.0	0.0	10.0	-165.51	25.82	0.0	0.0	0.0	-37.59
8	20	23.43	0.0	-4.42e-04	-10.56	0.0	-57.81	24.71	0.0	0.0	0.0	21.48
		21.48	0.0	0.0	0.0	10.0	-62.58	14.15	0.0	0.0	0.0	23.43
8	21	-3.59	0.0	-1.57e-05	-5.94	0.0	-78.91	11.43	0.0	0.0	0.0	-4.44
		-4.44	0.0	0.0	0.0	10.0	-81.28	5.48	0.0	0.0	0.0	-3.59
9	2	-2.92	0.0	-1.65e-05	-5.67	0.0	-80.91	9.51	0.0	0.0	0.0	-3.59
		-3.59	0.0	0.0	0.0	10.0	-83.49	3.84	0.0	0.0	0.0	-2.92
9	3	-60.71	0.0	-8.17e-05	-7.65	0.0	-258.83	56.92	0.0	0.0	0.0	-66.05
		-66.05	0.0	0.0	0.0	10.0	-262.32	49.27	0.0	0.0	0.0	-60.71
9	9	45.68	0.0	-7.78e-04	-16.05	0.0	-74.83	26.75	0.0	0.0	0.0	43.79
		43.79	0.0	0.0	0.0	10.0	-83.22	10.70	0.0	0.0	0.0	45.68
9	10	46.70	0.0	-7.72e-04	-14.07	0.0	-46.51	23.42	0.0	0.0	0.0	45.05
		45.05	0.0	0.0	0.0	10.0	-53.99	9.35	0.0	0.0	0.0	46.70
9	12	1.29	0.0	-1.44e-04	-5.67	0.0	-72.81	13.22	0.0	0.0	0.0	0.25
		0.25	0.0	0.0	0.0	10.0	-75.39	7.55	0.0	0.0	0.0	1.29
9	13	-2.92	0.0	-1.65e-05	-5.67	0.0	-80.91	9.51	0.0	0.0	0.0	-3.59
		-3.59	0.0	0.0	0.0	10.0	-83.49	3.84	0.0	0.0	0.0	-2.92
9	14	-44.97	0.0	-6.05e-05	-5.67	0.0	-191.73	42.16	0.0	0.0	0.0	-48.92
		-48.92	0.0	0.0	0.0	10.0	-194.31	36.49	0.0	0.0	0.0	-44.97
9	17	33.83	0.0	-5.76e-04	-11.89	0.0	-55.43	19.81	0.0	0.0	0.0	32.44
		32.44	0.0	0.0	0.0	10.0	-61.64	7.92	0.0	0.0	0.0	33.83
9	18	-2.92	0.0	-1.65e-05	-5.67	0.0	-80.91	9.51	0.0	0.0	0.0	-3.59
		-3.59	0.0	0.0	0.0	10.0	-83.49	3.84	0.0	0.0	0.0	-2.92
9	19	-34.46	0.0	-4.95e-05	-5.67	0.0	-164.02	34.00	0.0	0.0	0.0	-37.59
		-37.59	0.0	0.0	0.0	10.0	-166.60	28.33	0.0	0.0	0.0	-34.46
9	20	24.65	0.0	-4.36e-04	-10.34	0.0	-61.80	17.24	0.0	0.0	0.0	23.43
		23.43	0.0	0.0	0.0	10.0	-67.10	6.90	0.0	0.0	0.0	24.65
9	21	-2.92	0.0	-1.65e-05	-5.67	0.0	-80.91	9.51	0.0	0.0	0.0	-3.59
		-3.59	0.0	0.0	0.0	10.0	-83.49	3.84	0.0	0.0	0.0	-2.92
10	2	-2.39	0.0	-1.71e-05	-5.40	0.0	-83.20	7.98	0.0	0.0	0.0	-2.92
		-2.92	0.0	0.0	0.0	10.0	-85.97	2.58	0.0	0.0	0.0	-2.39
10	3	-54.83	0.0	-9.59e-05	-7.28	0.0	-259.55	62.22	0.0	0.0	0.0	-60.71
		-60.71	0.0	0.0	0.0	10.0	-263.28	54.94	0.0	0.0	0.0	-54.83
10	9	46.38	0.0	-7.67e-04	-15.73	0.0	-82.58	14.81	0.0	0.0	0.0	45.68
		45.68	0.0	0.0	0.0	10.0	-91.82	-0.91	0.0	0.0	0.0	46.38
10	10	47.22	0.0	-7.61e-04	-13.84	0.0	-53.46	12.02	0.0	0.0	0.0	46.70
		46.70	0.0	0.0	0.0	10.0	-61.73	-1.82	0.0	0.0	0.0	47.21
10	12	2.12	0.0	-1.43e-04	-5.40	0.0	-75.09	11.03	0.0	0.0	0.0	1.29
		1.29	0.0	0.0	0.0	10.0	-77.86	5.63	0.0	0.0	0.0	2.12
10	13	-2.39	0.0	-1.71e-05	-5.40	0.0	-83.20	7.98	0.0	0.0	0.0	-2.92
		-2.92	0.0	0.0	0.0	10.0	-85.97	2.58	0.0	0.0	0.0	-2.39
10	14	-40.61	0.0	-7.10e-05	-5.40	0.0	-192.26	46.09	0.0	0.0	0.0	-44.97
		-44.97	0.0	0.0	0.0	10.0	-195.03	40.70	0.0	0.0	0.0	-40.61
10	17	34.35	0.0	-5.68e-04	-11.65	0.0	-61.17	10.97	0.0	0.0	0.0	33.83
		33.83	0.0	0.0	0.0	10.0	-68.02	-0.68	0.0	0.0	0.0	34.35

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
10	18	-2.39	0.0	-1.71e-05	-5.40	0.0	-83.20	7.98	0.0	0.0	0.0	-2.92
		-2.92	0.0	0.0	0.0	10.0	-85.97	2.58	0.0	0.0	0.0	-2.39
10	19	-31.06	0.0	-5.75e-05	-5.40	0.0	-164.99	36.56	0.0	0.0	0.0	-34.46
		-34.46	0.0	0.0	0.0	10.0	-167.76	31.17	0.0	0.0	0.0	-31.06
10	20	25.17	0.0	-4.30e-04	-10.09	0.0	-66.68	10.22	0.0	0.0	0.0	24.65
		24.65	0.0	0.0	0.0	10.0	-72.51	0.14	0.0	0.0	0.0	25.17
10	21	-2.39	0.0	-1.71e-05	-5.40	0.0	-83.20	7.98	0.0	0.0	0.0	-2.92
		-2.92	0.0	0.0	0.0	10.0	-85.97	2.58	0.0	0.0	0.0	-2.39
11	3	-48.35	0.0	-1.09e-04	-6.91	0.0	-260.23	67.94	0.0	0.0	0.0	-54.83
		-54.83	0.0	0.0	0.0	10.0	-264.20	61.02	0.0	0.0	0.0	-48.35
11	4	-47.67	0.0	-1.03e-04	-5.12	0.0	-230.23	65.54	0.0	0.0	0.0	-53.99
		-53.99	0.0	0.0	0.0	10.0	-233.17	60.42	0.0	0.0	0.0	-47.67
11	9	46.42	0.0	-7.56e-04	-15.35	0.0	-91.76	3.65	0.0	0.0	0.0	46.38
		45.97	0.0	0.0	0.0	10.0	-101.84	-11.70	0.0	0.0	0.0	45.97
11	10	47.22	0.0	-7.50e-04	-13.56	0.0	-61.75	1.25	0.0	0.0	0.0	47.21
		46.66	0.0	0.0	0.0	10.0	-70.80	-12.31	0.0	0.0	0.0	46.66
11	12	2.79	0.0	-1.43e-04	-5.12	0.0	-77.66	9.24	0.0	0.0	0.0	2.12
		2.12	0.0	0.0	0.0	10.0	-80.60	4.12	0.0	0.0	0.0	2.79
11	14	-35.82	0.0	-8.05e-05	-5.12	0.0	-192.77	50.32	0.0	0.0	0.0	-40.61
		-40.61	0.0	0.0	0.0	10.0	-195.71	45.20	0.0	0.0	0.0	-35.82
11	17	34.38	0.0	-5.60e-04	-11.37	0.0	-67.97	2.70	0.0	0.0	0.0	34.35
		34.05	0.0	0.0	0.0	10.0	-75.44	-8.67	0.0	0.0	0.0	34.05
11	19	-27.35	0.0	-6.48e-05	-5.12	0.0	-166.01	39.45	0.0	0.0	0.0	-31.06
		-31.06	0.0	0.0	0.0	10.0	-168.95	34.33	0.0	0.0	0.0	-27.35
11	20	25.24	0.0	-4.24e-04	-9.81	0.0	-72.41	3.74	0.0	0.0	0.0	25.17
		25.05	0.0	0.0	0.0	10.0	-78.75	-6.07	0.0	0.0	0.0	25.05
11	21	-1.96	0.0	-1.76e-05	-5.12	0.0	-85.73	6.85	0.0	0.0	0.0	-2.39
		-2.39	0.0	0.0	0.0	10.0	-88.67	1.72	0.0	0.0	0.0	-1.96
12	2	-1.59	0.0	-1.80e-05	-4.85	0.0	-88.48	6.12	0.0	0.0	0.0	-1.96
		-1.96	0.0	0.0	0.0	10.0	-91.57	1.27	0.0	0.0	0.0	-1.59
12	3	-41.24	0.0	-1.20e-04	-6.55	0.0	-260.85	74.06	0.0	0.0	0.0	-48.35
		-48.35	0.0	0.0	0.0	10.0	-265.02	67.51	0.0	0.0	0.0	-41.24
12	9	45.97	0.0	-7.45e-04	-14.92	0.0	-102.30	-6.63	0.0	0.0	0.0	45.97
		44.56	0.0	0.0	0.0	10.0	-113.20	-21.56	0.0	0.0	0.0	44.56
12	10	46.66	0.0	-7.38e-04	-13.23	0.0	-71.33	-8.78	0.0	0.0	0.0	46.66
		45.11	0.0	0.0	0.0	10.0	-81.15	-22.00	0.0	0.0	0.0	45.11
12	12	3.34	0.0	-1.42e-04	-4.85	0.0	-80.49	7.88	0.0	0.0	0.0	2.79
		2.79	0.0	0.0	0.0	10.0	-83.58	3.03	0.0	0.0	0.0	3.34
12	13	-1.59	0.0	-1.80e-05	-4.85	0.0	-88.48	6.12	0.0	0.0	0.0	-1.96
		-1.96	0.0	0.0	0.0	10.0	-91.57	1.27	0.0	0.0	0.0	-1.59
12	14	-30.55	0.0	-8.89e-05	-4.85	0.0	-193.22	54.86	0.0	0.0	0.0	-35.82
		-35.82	0.0	0.0	0.0	10.0	-196.31	50.01	0.0	0.0	0.0	-30.55
12	17	34.05	0.0	-5.52e-04	-11.05	0.0	-75.77	-4.91	0.0	0.0	0.0	34.05
		33.00	0.0	0.0	0.0	10.0	-83.86	-15.97	0.0	0.0	0.0	33.00
12	18	-1.59	0.0	-1.80e-05	-4.85	0.0	-88.48	6.12	0.0	0.0	0.0	-1.96
		-1.96	0.0	0.0	0.0	10.0	-91.57	1.27	0.0	0.0	0.0	-1.59
12	19	-23.31	0.0	-7.12e-05	-4.85	0.0	-167.03	42.68	0.0	0.0	0.0	-27.35
		-27.35	0.0	0.0	0.0	10.0	-170.13	37.83	0.0	0.0	0.0	-23.31
12	20	25.05	0.0	-4.18e-04	-9.50	0.0	-78.95	-2.15	0.0	0.0	0.0	25.05
		24.36	0.0	0.0	0.0	10.0	-85.78	-11.66	0.0	0.0	0.0	24.36
12	21	-1.59	0.0	-1.80e-05	-4.85	0.0	-88.48	6.12	0.0	0.0	0.0	-1.96
		-1.96	0.0	0.0	0.0	10.0	-91.57	1.27	0.0	0.0	0.0	-1.59
13	2	-1.23	0.0	-1.84e-05	-4.58	0.0	-91.39	5.82	0.0	0.0	0.0	-1.59
		-1.59	0.0	0.0	0.0	10.0	-94.63	1.24	0.0	0.0	0.0	-1.23
13	3	-33.46	0.0	-1.30e-04	-6.18	0.0	-261.35	80.58	0.0	0.0	0.0	-41.24
		-41.24	0.0	0.0	0.0	10.0	-265.71	74.40	0.0	0.0	0.0	-33.46
13	9	44.56	0.0	-7.34e-04	-14.45	0.0	-114.13	-15.91	0.0	0.0	0.0	44.56
		42.23	0.0	0.0	0.0	10.0	-125.85	-30.36	0.0	0.0	0.0	42.23
13	10	45.11	0.0	-7.28e-04	-12.85	0.0	-82.15	-17.95	0.0	0.0	0.0	45.11
		42.66	0.0	0.0	0.0	10.0	-92.73	-30.80	0.0	0.0	0.0	42.66
13	12	3.81	0.0	-1.41e-04	-4.58	0.0	-83.54	6.93	0.0	0.0	0.0	3.34
		3.34	0.0	0.0	0.0	10.0	-86.77	2.36	0.0	0.0	0.0	3.81
13	13	-1.23	0.0	-1.84e-05	-4.58	0.0	-91.39	5.82	0.0	0.0	0.0	-1.59
		-1.59	0.0	0.0	0.0	10.0	-94.63	1.24	0.0	0.0	0.0	-1.23
13	14	-24.78	0.0	-9.61e-05	-4.58	0.0	-193.59	59.69	0.0	0.0	0.0	-30.55
		-30.55	0.0	0.0	0.0	10.0	-196.82	55.11	0.0	0.0	0.0	-24.78
13	17	33.00	0.0	-5.44e-04	-10.70	0.0	-84.54	-11.79	0.0	0.0	0.0	33.00
		31.28	0.0	0.0	0.0	10.0	-93.22	-22.49	0.0	0.0	0.0	31.28
13	18	-1.23	0.0	-1.84e-05	-4.58	0.0	-91.39	5.82	0.0	0.0	0.0	-1.59
		-1.59	0.0	0.0	0.0	10.0	-94.63	1.24	0.0	0.0	0.0	-1.23
13	19	-18.90	0.0	-7.67e-05	-4.58	0.0	-168.04	46.22	0.0	0.0	0.0	-23.31
		-23.31	0.0	0.0	0.0	10.0	-171.27	41.64	0.0	0.0	0.0	-18.90
13	20	24.36	0.0	-4.12e-04	-9.17	0.0	-86.26	-7.39	0.0	0.0	0.0	24.36

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		23.15	0.0	0.0	0.0	10.0	-93.57	-16.56	0.0	0.0	0.0	23.15
13	21	-1.23	0.0	-1.84e-05	-4.58	0.0	-91.39	5.82	0.0	0.0	0.0	-1.59
		-1.59	0.0	0.0	0.0	10.0	-94.63	1.24	0.0	0.0	0.0	-1.23
14	1	-1.16	0.0	-2.52e-05	-5.82	0.0	-127.50	8.01	0.0	0.0	0.0	-1.67
		-1.67	0.0	0.0	0.0	10.0	-132.03	2.19	0.0	0.0	0.0	-1.16
14	3	-24.96	0.0	-1.38e-04	-5.82	0.0	-261.69	87.50	0.0	0.0	0.0	-33.46
		-33.46	0.0	0.0	0.0	10.0	-266.21	81.68	0.0	0.0	0.0	-24.96
14	9	42.23	0.0	-7.24e-04	-13.93	0.0	-127.20	-24.08	0.0	0.0	0.0	42.23
		39.11	0.0	0.0	0.0	10.0	-139.70	-38.01	0.0	0.0	0.0	39.11
14	10	42.66	0.0	-7.18e-04	-12.42	0.0	-94.14	-26.16	0.0	0.0	0.0	42.66
		39.41	0.0	0.0	0.0	10.0	-105.47	-38.58	0.0	0.0	0.0	39.41
14	12	4.24	0.0	-1.40e-04	-4.31	0.0	-86.77	6.43	0.0	0.0	0.0	3.81
		3.81	0.0	0.0	0.0	10.0	-90.12	2.12	0.0	0.0	0.0	4.24
14	13	-0.86	0.0	-1.86e-05	-4.31	0.0	-94.45	5.93	0.0	0.0	0.0	-1.23
		-1.23	0.0	0.0	0.0	10.0	-97.80	1.62	0.0	0.0	0.0	-0.86
14	14	-18.49	0.0	-1.02e-04	-4.31	0.0	-193.84	64.81	0.0	0.0	0.0	-24.78
		-24.78	0.0	0.0	0.0	10.0	-197.20	60.50	0.0	0.0	0.0	-18.49
14	17	31.28	0.0	-5.36e-04	-10.32	0.0	-94.22	-17.84	0.0	0.0	0.0	31.28
		28.97	0.0	0.0	0.0	10.0	-103.48	-28.16	0.0	0.0	0.0	28.97
14	18	-0.86	0.0	-1.86e-05	-4.31	0.0	-94.45	5.93	0.0	0.0	0.0	-1.23
		-1.23	0.0	0.0	0.0	10.0	-97.80	1.62	0.0	0.0	0.0	-0.86
14	19	-14.08	0.0	-8.11e-05	-4.31	0.0	-168.99	50.09	0.0	0.0	0.0	-18.90
		-18.90	0.0	0.0	0.0	10.0	-172.35	45.78	0.0	0.0	0.0	-14.08
14	20	23.15	0.0	-4.07e-04	-8.82	0.0	-94.28	-11.90	0.0	0.0	0.0	23.15
		21.52	0.0	0.0	0.0	10.0	-102.06	-20.71	0.0	0.0	0.0	21.52
14	21	-0.86	0.0	-1.86e-05	-4.31	0.0	-94.45	5.93	0.0	0.0	0.0	-1.23
		-1.23	0.0	0.0	0.0	10.0	-97.80	1.62	0.0	0.0	0.0	-0.86
15	2	-0.41	0.0	-1.89e-05	-4.05	0.0	-97.60	6.47	0.0	0.0	0.0	-0.86
		-0.86	0.0	0.0	0.0	10.0	-101.06	2.43	0.0	0.0	0.0	-0.41
15	3	-15.71	0.0	-1.44e-04	-5.46	0.0	-261.83	94.79	0.0	0.0	0.0	-24.96
		-24.96	0.0	0.0	0.0	10.0	-266.51	89.32	0.0	0.0	0.0	-15.71
15	10	39.41	0.0	-7.08e-04	-11.95	0.0	-107.25	-33.30	0.0	0.0	0.0	39.41
		35.47	0.0	0.0	0.0	10.0	-119.29	-45.25	0.0	0.0	0.0	35.47
15	12	4.67	0.0	-1.39e-04	-4.05	0.0	-90.15	6.37	0.0	0.0	0.0	4.24
		4.24	0.0	0.0	0.0	10.0	-93.61	2.32	0.0	0.0	0.0	4.67
15	13	-0.41	0.0	-1.89e-05	-4.05	0.0	-97.60	6.47	0.0	0.0	0.0	-0.86
		-0.86	0.0	0.0	0.0	10.0	-101.06	2.43	0.0	0.0	0.0	-0.41
15	14	-11.64	0.0	-1.06e-04	-4.05	0.0	-193.95	70.21	0.0	0.0	0.0	-18.49
		-18.49	0.0	0.0	0.0	10.0	-197.41	66.17	0.0	0.0	0.0	-11.64
15	17	28.97	0.0	-5.30e-04	-9.90	0.0	-104.75	-22.99	0.0	0.0	0.0	28.97
		26.17	0.0	0.0	0.0	10.0	-114.56	-32.89	0.0	0.0	0.0	26.17
15	18	-0.41	0.0	-1.89e-05	-4.05	0.0	-97.60	6.47	0.0	0.0	0.0	-0.86
		-0.86	0.0	0.0	0.0	10.0	-101.06	2.43	0.0	0.0	0.0	-0.41
15	19	-8.83	0.0	-8.45e-05	-4.05	0.0	-169.86	54.28	0.0	0.0	0.0	-14.08
		-14.08	0.0	0.0	0.0	10.0	-173.33	50.23	0.0	0.0	0.0	-8.83
15	20	21.52	0.0	-4.02e-04	-8.44	0.0	-102.96	-15.62	0.0	0.0	0.0	21.52
		19.52	0.0	0.0	0.0	10.0	-111.19	-24.06	0.0	0.0	0.0	19.52
15	21	-0.41	0.0	-1.89e-05	-4.05	0.0	-97.60	6.47	0.0	0.0	0.0	-0.86
		-0.86	0.0	0.0	0.0	10.0	-101.06	2.43	0.0	0.0	0.0	-0.41
16	1	0.20	0.0	-2.56e-05	-5.03	0.0	-136.11	10.04	0.0	0.0	0.0	-0.55
		-0.55	0.0	0.0	0.0	10.0	-131.92	5.02	0.0	0.0	0.0	0.20
16	2	0.15	0.0	-1.90e-05	-3.72	0.0	-100.82	7.44	0.0	0.0	0.0	-0.41
		-0.41	0.0	0.0	0.0	10.0	-97.72	3.72	0.0	0.0	0.0	0.15
16	3	-6.08	0.0	-1.47e-04	-13.05	0.0	-261.75	102.44	0.0	0.0	0.0	-15.71
		-15.71	0.0	0.0	0.0	10.0	-250.87	89.39	0.0	0.0	0.0	-6.08
16	10	35.47	0.0	-7.00e-04	-3.72	0.0	-121.39	-39.27	0.0	0.0	0.0	35.47
		31.34	0.0	0.0	0.0	10.0	-118.28	-43.00	0.0	0.0	0.0	31.34
16	12	5.16	0.0	-1.38e-04	-3.72	0.0	-93.64	6.75	0.0	0.0	0.0	4.67
		4.67	0.0	0.0	0.0	10.0	-90.53	3.02	0.0	0.0	0.0	5.16
16	13	0.15	0.0	-1.90e-05	-3.72	0.0	-100.82	7.44	0.0	0.0	0.0	-0.41
		-0.41	0.0	0.0	0.0	10.0	-97.72	3.72	0.0	0.0	0.0	0.15
16	14	-4.50	0.0	-1.09e-04	-9.66	0.0	-193.89	75.88	0.0	0.0	0.0	-11.64
		-11.64	0.0	0.0	0.0	10.0	-185.83	66.22	0.0	0.0	0.0	-4.50
16	17	26.17	0.0	-5.23e-04	-3.72	0.0	-116.05	-27.16	0.0	0.0	0.0	26.17
		23.25	0.0	0.0	0.0	10.0	-112.95	-30.89	0.0	0.0	0.0	23.25
16	18	0.15	0.0	-1.90e-05	-3.72	0.0	-100.82	7.44	0.0	0.0	0.0	-0.41
		-0.41	0.0	0.0	0.0	10.0	-97.72	3.72	0.0	0.0	0.0	0.15
16	19	-3.34	0.0	-8.66e-05	-8.18	0.0	-170.62	58.77	0.0	0.0	0.0	-8.83
		-8.83	0.0	0.0	0.0	10.0	-163.80	50.59	0.0	0.0	0.0	-3.34
16	20	19.52	0.0	-3.97e-04	-3.72	0.0	-112.25	-18.51	0.0	0.0	0.0	19.52
		17.48	0.0	0.0	0.0	10.0	-109.14	-22.23	0.0	0.0	0.0	17.48
16	21	0.15	0.0	-1.90e-05	-3.72	0.0	-100.82	7.44	0.0	0.0	0.0	-0.41
		-0.41	0.0	0.0	0.0	10.0	-97.72	3.72	0.0	0.0	0.0	0.15

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
17	2	0.82	0.0	-1.90e-05	-3.87	0.0	-97.41	8.56	0.0	0.0	0.0	0.15
		0.15	0.0	0.0	0.0	10.0	-94.49	4.69	0.0	0.0	0.0	0.82
17	3	3.46	0.0	-1.49e-04	-13.57	0.0	-246.12	101.74	0.0	0.0	0.0	-6.08
		-6.08	0.0	0.0	0.0	10.0	-235.90	88.16	0.0	0.0	0.0	3.46
17	4	3.18	0.0	-1.42e-04	-12.22	0.0	-212.03	98.74	0.0	0.0	0.0	-6.13
		-6.13	0.0	0.0	0.0	10.0	-202.83	86.52	0.0	0.0	0.0	3.18
17	9	31.39	0.0	-6.99e-04	-5.23	0.0	-154.36	-34.08	0.0	0.0	0.0	31.39
		27.70	0.0	0.0	0.0	10.0	-150.43	-39.30	0.0	0.0	0.0	27.70
17	10	31.34	0.0	-6.93e-04	-3.87	0.0	-120.27	-37.07	0.0	0.0	0.0	31.34
		27.42	0.0	0.0	0.0	10.0	-117.35	-40.94	0.0	0.0	0.0	27.42
17	12	5.70	0.0	-1.37e-04	-3.87	0.0	-90.54	7.31	0.0	0.0	0.0	5.16
		5.16	0.0	0.0	0.0	10.0	-87.63	3.44	0.0	0.0	0.0	5.70
17	13	0.82	0.0	-1.90e-05	-3.87	0.0	-97.41	8.56	0.0	0.0	0.0	0.15
		0.15	0.0	0.0	0.0	10.0	-94.49	4.69	0.0	0.0	0.0	0.82
17	14	2.57	0.0	-1.10e-04	-10.05	0.0	-182.31	75.36	0.0	0.0	0.0	-4.50
		-4.50	0.0	0.0	0.0	10.0	-174.74	65.31	0.0	0.0	0.0	2.57
17	17	23.25	0.0	-5.18e-04	-3.87	0.0	-114.34	-25.24	0.0	0.0	0.0	23.25
		20.52	0.0	0.0	0.0	10.0	-111.43	-29.11	0.0	0.0	0.0	20.52
17	18	0.82	0.0	-1.90e-05	-3.87	0.0	-97.41	8.56	0.0	0.0	0.0	0.15
		0.15	0.0	0.0	0.0	10.0	-94.49	4.69	0.0	0.0	0.0	0.82
17	19	2.13	0.0	-8.74e-05	-8.51	0.0	-161.09	58.66	0.0	0.0	0.0	-3.34
		-3.34	0.0	0.0	0.0	10.0	-154.68	50.15	0.0	0.0	0.0	2.13
17	20	17.48	0.0	-3.93e-04	-3.87	0.0	-110.11	-16.79	0.0	0.0	0.0	17.48
		15.59	0.0	0.0	0.0	10.0	-107.19	-20.66	0.0	0.0	0.0	15.59
17	21	0.82	0.0	-1.90e-05	-3.87	0.0	-97.41	8.56	0.0	0.0	0.0	0.15
		0.15	0.0	0.0	0.0	10.0	-94.49	4.69	0.0	0.0	0.0	0.82
18	2	1.56	0.0	-1.88e-05	-4.01	0.0	-94.15	9.37	0.0	0.0	0.0	0.82
		0.82	0.0	0.0	0.0	10.0	-91.42	5.36	0.0	0.0	0.0	1.56
18	3	12.78	0.0	-1.48e-04	-14.06	0.0	-231.24	99.76	0.0	0.0	0.0	3.46
		3.46	0.0	0.0	0.0	10.0	-221.70	85.70	0.0	0.0	0.0	12.78
18	9	27.70	0.0	-6.93e-04	-5.42	0.0	-152.19	-31.79	0.0	0.0	0.0	27.70
		24.24	0.0	0.0	0.0	10.0	-148.52	-37.21	0.0	0.0	0.0	24.24
18	10	27.42	0.0	-6.87e-04	-4.01	0.0	-119.24	-35.07	0.0	0.0	0.0	27.42
		23.69	0.0	0.0	0.0	10.0	-116.52	-39.08	0.0	0.0	0.0	23.69
18	12	6.26	0.0	-1.36e-04	-4.01	0.0	-87.63	7.59	0.0	0.0	0.0	5.70
		5.70	0.0	0.0	0.0	10.0	-84.91	3.58	0.0	0.0	0.0	6.26
18	13	1.56	0.0	-1.88e-05	-4.01	0.0	-94.15	9.37	0.0	0.0	0.0	0.82
		0.82	0.0	0.0	0.0	10.0	-91.42	5.36	0.0	0.0	0.0	1.56
18	14	9.47	0.0	-1.10e-04	-10.42	0.0	-171.29	73.90	0.0	0.0	0.0	2.57
		2.57	0.0	0.0	0.0	10.0	-164.22	63.48	0.0	0.0	0.0	9.47
18	17	20.52	0.0	-5.13e-04	-4.01	0.0	-112.73	-23.55	0.0	0.0	0.0	20.52
		17.95	0.0	0.0	0.0	10.0	-110.01	-27.56	0.0	0.0	0.0	17.95
18	18	1.56	0.0	-1.88e-05	-4.01	0.0	-94.15	9.37	0.0	0.0	0.0	0.82
		0.82	0.0	0.0	0.0	10.0	-91.42	5.36	0.0	0.0	0.0	1.56
18	19	7.49	0.0	-8.68e-05	-8.81	0.0	-152.00	57.77	0.0	0.0	0.0	2.13
		2.13	0.0	0.0	0.0	10.0	-146.02	48.95	0.0	0.0	0.0	7.49
18	20	15.59	0.0	-3.90e-04	-4.01	0.0	-108.09	-15.32	0.0	0.0	0.0	15.59
		13.85	0.0	0.0	0.0	10.0	-105.37	-19.33	0.0	0.0	0.0	13.85
18	21	1.56	0.0	-1.88e-05	-4.01	0.0	-94.15	9.37	0.0	0.0	0.0	0.82
		0.82	0.0	0.0	0.0	10.0	-91.42	5.36	0.0	0.0	0.0	1.56
19	2	2.34	0.0	-1.84e-05	-4.14	0.0	-91.05	9.89	0.0	0.0	0.0	1.56
		1.56	0.0	0.0	0.0	10.0	-88.53	5.75	0.0	0.0	0.0	2.34
19	3	21.76	0.0	-1.45e-04	-14.52	0.0	-217.18	96.60	0.0	0.0	0.0	12.78
		12.78	0.0	0.0	0.0	10.0	-208.35	82.08	0.0	0.0	0.0	21.76
19	9	24.24	0.0	-6.88e-04	-5.59	0.0	-150.18	-29.79	0.0	0.0	0.0	24.24
		20.96	0.0	0.0	0.0	10.0	-146.78	-35.38	0.0	0.0	0.0	20.96
19	10	23.69	0.0	-6.81e-04	-4.14	0.0	-118.32	-33.25	0.0	0.0	0.0	23.69
		20.14	0.0	0.0	0.0	10.0	-115.80	-37.39	0.0	0.0	0.0	20.14
19	12	6.82	0.0	-1.34e-04	-4.14	0.0	-84.93	7.61	0.0	0.0	0.0	6.26
		6.26	0.0	0.0	0.0	10.0	-82.41	3.46	0.0	0.0	0.0	6.82
19	13	2.34	0.0	-1.84e-05	-4.14	0.0	-91.05	9.89	0.0	0.0	0.0	1.56
		1.56	0.0	0.0	0.0	10.0	-88.53	5.75	0.0	0.0	0.0	2.34
19	14	16.12	0.0	-1.07e-04	-10.75	0.0	-160.87	71.56	0.0	0.0	0.0	9.47
		9.47	0.0	0.0	0.0	10.0	-154.34	60.80	0.0	0.0	0.0	16.12
19	17	17.95	0.0	-5.09e-04	-4.14	0.0	-111.25	-22.07	0.0	0.0	0.0	17.95
		15.53	0.0	0.0	0.0	10.0	-108.73	-26.21	0.0	0.0	0.0	15.53
19	18	2.34	0.0	-1.84e-05	-4.14	0.0	-91.05	9.89	0.0	0.0	0.0	1.56
		1.56	0.0	0.0	0.0	10.0	-88.53	5.75	0.0	0.0	0.0	2.34
19	19	12.67	0.0	-8.50e-05	-9.10	0.0	-143.42	56.14	0.0	0.0	0.0	7.49
		7.49	0.0	0.0	0.0	10.0	-137.88	47.04	0.0	0.0	0.0	12.67
19	20	13.85	0.0	-3.87e-04	-4.14	0.0	-106.20	-14.08	0.0	0.0	0.0	13.85
		12.23	0.0	0.0	0.0	10.0	-103.68	-18.22	0.0	0.0	0.0	12.23
19	21	2.34	0.0	-1.84e-05	-4.14	0.0	-91.05	9.89	0.0	0.0	0.0	1.56

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.56	0.0	0.0	0.0	10.0	-88.53	5.75	0.0	0.0	0.0	2.34
20	2	3.15	0.0	-1.79e-05	-4.26	0.0	-88.13	10.13	0.0	0.0	0.0	2.34
		2.34	0.0	0.0	0.0	10.0	-85.82	5.87	0.0	0.0	0.0	3.15
20	3	30.28	0.0	-1.40e-04	-14.94	0.0	-204.02	92.32	0.0	0.0	0.0	21.76
		21.76	0.0	0.0	0.0	10.0	-195.93	77.39	0.0	0.0	0.0	30.28
20	10	20.14	0.0	-6.77e-04	-4.26	0.0	-117.51	-31.60	0.0	0.0	0.0	20.14
		16.75	0.0	0.0	0.0	10.0	-115.20	-35.86	0.0	0.0	0.0	16.75
20	12	7.35	0.0	-1.33e-04	-4.26	0.0	-82.45	7.38	0.0	0.0	0.0	6.82
		6.82	0.0	0.0	0.0	10.0	-80.14	3.12	0.0	0.0	0.0	7.35
20	13	3.15	0.0	-1.79e-05	-4.26	0.0	-88.13	10.13	0.0	0.0	0.0	2.34
		2.34	0.0	0.0	0.0	10.0	-85.82	5.87	0.0	0.0	0.0	3.15
20	14	22.43	0.0	-1.03e-04	-11.06	0.0	-151.13	68.39	0.0	0.0	0.0	16.12
		16.12	0.0	0.0	0.0	10.0	-145.13	57.32	0.0	0.0	0.0	22.43
20	17	15.53	0.0	-5.06e-04	-4.26	0.0	-109.89	-20.78	0.0	0.0	0.0	15.53
		13.23	0.0	0.0	0.0	10.0	-107.59	-25.04	0.0	0.0	0.0	13.23
20	18	3.15	0.0	-1.79e-05	-4.26	0.0	-88.13	10.13	0.0	0.0	0.0	2.34
		2.34	0.0	0.0	0.0	10.0	-85.82	5.87	0.0	0.0	0.0	3.15
20	19	17.61	0.0	-8.20e-05	-9.36	0.0	-135.38	53.82	0.0	0.0	0.0	12.67
		12.67	0.0	0.0	0.0	10.0	-130.31	44.46	0.0	0.0	0.0	17.61
20	20	12.23	0.0	-3.84e-04	-4.26	0.0	-104.45	-13.05	0.0	0.0	0.0	12.23
		10.71	0.0	0.0	0.0	10.0	-102.15	-17.31	0.0	0.0	0.0	10.71
20	21	3.15	0.0	-1.79e-05	-4.26	0.0	-88.13	10.13	0.0	0.0	0.0	2.34
		2.34	0.0	0.0	0.0	10.0	-85.82	5.87	0.0	0.0	0.0	3.15
21	2	3.94	0.0	-1.72e-05	-4.37	0.0	-85.43	10.12	0.0	0.0	0.0	3.15
		3.15	0.0	0.0	0.0	10.0	-83.33	5.75	0.0	0.0	0.0	3.94
21	3	38.25	0.0	-1.32e-04	-15.32	0.0	-191.85	87.01	0.0	0.0	0.0	30.28
		30.28	0.0	0.0	0.0	10.0	-184.51	71.69	0.0	0.0	0.0	38.25
21	10	16.75	0.0	-6.73e-04	-4.37	0.0	-116.84	-30.10	0.0	0.0	0.0	16.75
		13.51	0.0	0.0	0.0	10.0	-114.74	-34.47	0.0	0.0	0.0	13.51
21	12	7.82	0.0	-1.31e-04	-4.37	0.0	-80.21	6.94	0.0	0.0	0.0	7.35
		7.35	0.0	0.0	0.0	10.0	-78.11	2.57	0.0	0.0	0.0	7.82
21	13	3.94	0.0	-1.72e-05	-4.37	0.0	-85.43	10.12	0.0	0.0	0.0	3.15
		3.15	0.0	0.0	0.0	10.0	-83.33	5.75	0.0	0.0	0.0	3.94
21	14	28.34	0.0	-9.81e-05	-11.35	0.0	-142.11	64.45	0.0	0.0	0.0	22.43
		22.43	0.0	0.0	0.0	10.0	-136.67	53.11	0.0	0.0	0.0	28.34
21	17	13.23	0.0	-5.03e-04	-4.37	0.0	-108.70	-19.67	0.0	0.0	0.0	13.23
		11.03	0.0	0.0	0.0	10.0	-106.60	-24.04	0.0	0.0	0.0	11.03
21	18	3.94	0.0	-1.72e-05	-4.37	0.0	-85.43	10.12	0.0	0.0	0.0	3.15
		3.15	0.0	0.0	0.0	10.0	-83.33	5.75	0.0	0.0	0.0	3.94
21	19	22.24	0.0	-7.78e-05	-9.60	0.0	-127.94	50.87	0.0	0.0	0.0	17.61
		17.61	0.0	0.0	0.0	10.0	-123.34	41.27	0.0	0.0	0.0	22.24
21	20	10.71	0.0	-3.81e-04	-4.37	0.0	-102.88	-12.22	0.0	0.0	0.0	10.71
		9.26	0.0	0.0	0.0	10.0	-100.78	-16.60	0.0	0.0	0.0	9.26
21	21	3.94	0.0	-1.72e-05	-4.37	0.0	-85.43	10.12	0.0	0.0	0.0	3.15
		3.15	0.0	0.0	0.0	10.0	-83.33	5.75	0.0	0.0	0.0	3.94
22	2	4.71	0.0	-1.62e-05	-4.47	0.0	-82.94	9.88	0.0	0.0	0.0	3.94
		3.94	0.0	0.0	0.0	10.0	-81.07	5.41	0.0	0.0	0.0	4.71
22	3	45.58	0.0	-1.23e-04	-15.67	0.0	-180.72	80.76	0.0	0.0	0.0	38.25
		38.25	0.0	0.0	0.0	10.0	-174.15	65.10	0.0	0.0	0.0	45.58
22	10	13.51	0.0	-6.70e-04	-4.47	0.0	-116.31	-28.74	0.0	0.0	0.0	13.51
		10.40	0.0	0.0	0.0	10.0	-114.44	-33.21	0.0	0.0	0.0	10.40
22	12	8.23	0.0	-1.29e-04	-4.47	0.0	-78.22	6.30	0.0	0.0	0.0	7.82
		7.82	0.0	0.0	0.0	10.0	-76.35	1.83	0.0	0.0	0.0	8.23
22	13	4.71	0.0	-1.62e-05	-4.47	0.0	-82.94	9.88	0.0	0.0	0.0	3.94
		3.94	0.0	0.0	0.0	10.0	-81.07	5.41	0.0	0.0	0.0	4.71
22	14	33.76	0.0	-9.14e-05	-11.60	0.0	-133.87	59.82	0.0	0.0	0.0	28.34
		28.34	0.0	0.0	0.0	10.0	-129.00	48.22	0.0	0.0	0.0	33.76
22	17	11.03	0.0	-5.00e-04	-4.47	0.0	-107.66	-18.72	0.0	0.0	0.0	11.03
		8.92	0.0	0.0	0.0	10.0	-105.79	-23.19	0.0	0.0	0.0	8.92
22	18	4.71	0.0	-1.62e-05	-4.47	0.0	-82.94	9.88	0.0	0.0	0.0	3.94
		3.94	0.0	0.0	0.0	10.0	-81.07	5.41	0.0	0.0	0.0	4.71
22	19	26.50	0.0	-7.26e-05	-9.82	0.0	-121.14	47.34	0.0	0.0	0.0	22.24
		22.24	0.0	0.0	0.0	10.0	-117.02	37.52	0.0	0.0	0.0	26.50
22	20	9.26	0.0	-3.79e-04	-4.47	0.0	-101.48	-11.57	0.0	0.0	0.0	9.26
		7.87	0.0	0.0	0.0	10.0	-99.61	-16.04	0.0	0.0	0.0	7.87
22	21	4.71	0.0	-1.62e-05	-4.47	0.0	-82.94	9.88	0.0	0.0	0.0	3.94
		3.94	0.0	0.0	0.0	10.0	-81.07	5.41	0.0	0.0	0.0	4.71
23	2	5.43	0.0	-1.51e-05	-4.56	0.0	-80.70	9.43	0.0	0.0	0.0	4.71
		4.71	0.0	0.0	0.0	10.0	-79.05	4.87	0.0	0.0	0.0	5.43
23	3	52.18	0.0	-1.13e-04	-15.97	0.0	-170.70	73.66	0.0	0.0	0.0	45.58
		45.58	0.0	0.0	0.0	10.0	-164.92	57.69	0.0	0.0	0.0	52.18
23	10	10.40	0.0	-6.67e-04	-4.56	0.0	-115.95	-27.49	0.0	0.0	0.0	10.40
		7.41	0.0	0.0	0.0	10.0	-114.29	-32.04	0.0	0.0	0.0	7.41



Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
23	12	8.56	0.0	-1.27e-04	-4.56	0.0	-76.50	5.49	0.0	0.0	0.0	8.23
		8.23	0.0	0.0	0.0	10.0	-74.85	0.93	0.0	0.0	0.0	8.56
23	13	5.43	0.0	-1.51e-05	-4.56	0.0	-80.70	9.43	0.0	0.0	0.0	4.71
		4.71	0.0	0.0	0.0	10.0	-79.05	4.87	0.0	0.0	0.0	5.43
23	14	38.65	0.0	-8.34e-05	-11.83	0.0	-126.45	54.56	0.0	0.0	0.0	33.76
		33.76	0.0	0.0	0.0	10.0	-122.16	42.73	0.0	0.0	0.0	38.65
23	17	8.92	0.0	-4.98e-04	-4.56	0.0	-106.81	-17.92	0.0	0.0	0.0	8.92
		6.90	0.0	0.0	0.0	10.0	-105.16	-22.47	0.0	0.0	0.0	6.90
23	18	5.43	0.0	-1.51e-05	-4.56	0.0	-80.70	9.43	0.0	0.0	0.0	4.71
		4.71	0.0	0.0	0.0	10.0	-79.05	4.87	0.0	0.0	0.0	5.43
23	19	30.35	0.0	-6.63e-05	-10.01	0.0	-115.01	43.28	0.0	0.0	0.0	26.50
		26.50	0.0	0.0	0.0	10.0	-111.38	33.27	0.0	0.0	0.0	30.35
23	20	7.87	0.0	-3.77e-04	-4.56	0.0	-100.28	-11.08	0.0	0.0	0.0	7.87
		6.53	0.0	0.0	0.0	10.0	-98.63	-15.64	0.0	0.0	0.0	6.53
23	21	5.43	0.0	-1.51e-05	-4.56	0.0	-80.70	9.43	0.0	0.0	0.0	4.71
		4.71	0.0	0.0	0.0	10.0	-79.05	4.87	0.0	0.0	0.0	5.43
24	2	6.08	0.0	-1.38e-05	-4.63	0.0	-78.71	8.79	0.0	0.0	0.0	5.43
		5.43	0.0	0.0	0.0	10.0	-77.29	4.15	0.0	0.0	0.0	6.08
24	3	57.98	0.0	-1.00e-04	-16.24	0.0	-161.85	65.80	0.0	0.0	0.0	52.18
		52.18	0.0	0.0	0.0	10.0	-156.87	49.56	0.0	0.0	0.0	57.98
24	10	7.41	0.0	-6.66e-04	-4.63	0.0	-115.74	-26.33	0.0	0.0	0.0	7.41
		4.53	0.0	0.0	0.0	10.0	-114.32	-30.97	0.0	0.0	0.0	4.53
24	12	8.78	0.0	-1.25e-04	-4.63	0.0	-75.07	4.54	0.0	0.0	0.0	8.56
		8.56	0.0	0.0	0.0	10.0	-73.64	-0.09	0.0	0.0	0.0	8.78
24	13	6.08	0.0	-1.38e-05	-4.63	0.0	-78.71	8.79	0.0	0.0	0.0	5.43
		5.43	0.0	0.0	0.0	10.0	-77.29	4.15	0.0	0.0	0.0	6.08
24	14	42.94	0.0	-7.43e-05	-12.03	0.0	-119.89	48.74	0.0	0.0	0.0	38.65
		38.65	0.0	0.0	0.0	10.0	-116.20	36.71	0.0	0.0	0.0	42.94
24	17	6.90	0.0	-4.97e-04	-4.63	0.0	-106.14	-17.23	0.0	0.0	0.0	6.90
		4.93	0.0	0.0	0.0	10.0	-104.72	-21.86	0.0	0.0	0.0	4.93
24	18	6.08	0.0	-1.38e-05	-4.63	0.0	-78.71	8.79	0.0	0.0	0.0	5.43
		5.43	0.0	0.0	0.0	10.0	-77.29	4.15	0.0	0.0	0.0	6.08
24	19	33.73	0.0	-5.91e-05	-10.18	0.0	-109.60	38.75	0.0	0.0	0.0	30.35
		30.35	0.0	0.0	0.0	10.0	-106.47	28.57	0.0	0.0	0.0	33.73
24	20	6.53	0.0	-3.76e-04	-4.63	0.0	-99.28	-10.72	0.0	0.0	0.0	6.53
		5.22	0.0	0.0	0.0	10.0	-97.86	-15.36	0.0	0.0	0.0	5.22
24	21	6.08	0.0	-1.38e-05	-4.63	0.0	-78.71	8.79	0.0	0.0	0.0	5.43
		5.43	0.0	0.0	0.0	10.0	-77.29	4.15	0.0	0.0	0.0	6.08
25	2	6.65	0.0	-1.24e-05	-4.70	0.0	-76.99	7.98	0.0	0.0	0.0	6.08
		6.08	0.0	0.0	0.0	10.0	-75.80	3.29	0.0	0.0	0.0	6.65
25	3	62.90	0.0	-8.66e-05	-16.47	0.0	-154.21	57.29	0.0	0.0	0.0	57.98
		57.98	0.0	0.0	0.0	10.0	-150.04	40.82	0.0	0.0	0.0	62.90
25	10	4.53	0.0	-6.65e-04	-4.70	0.0	-115.72	-25.25	0.0	0.0	0.0	4.53
		1.76	0.0	0.0	0.0	10.0	-114.53	-29.95	0.0	0.0	0.0	1.76
25	12	8.91	0.0	-1.23e-04	-4.70	0.0	-73.91	3.47	0.0	0.0	0.0	8.78
		8.78	0.0	0.0	0.0	10.0	-72.72	-1.23	0.0	0.0	0.0	8.89
25	13	6.65	0.0	-1.24e-05	-4.70	0.0	-76.99	7.98	0.0	0.0	0.0	6.08
		6.08	0.0	0.0	0.0	10.0	-75.80	3.29	0.0	0.0	0.0	6.65
25	14	46.60	0.0	-6.41e-05	-12.20	0.0	-114.23	42.43	0.0	0.0	0.0	42.94
		42.94	0.0	0.0	0.0	10.0	-111.14	30.24	0.0	0.0	0.0	46.60
25	17	4.93	0.0	-4.95e-04	-4.70	0.0	-105.68	-16.64	0.0	0.0	0.0	4.93
		3.02	0.0	0.0	0.0	10.0	-104.48	-21.34	0.0	0.0	0.0	3.02
25	18	6.65	0.0	-1.24e-05	-4.70	0.0	-76.99	7.98	0.0	0.0	0.0	6.08
		6.08	0.0	0.0	0.0	10.0	-75.80	3.29	0.0	0.0	0.0	6.65
25	19	36.61	0.0	-5.12e-05	-10.32	0.0	-104.92	33.82	0.0	0.0	0.0	33.73
		33.73	0.0	0.0	0.0	10.0	-102.30	23.50	0.0	0.0	0.0	36.61
25	20	5.22	0.0	-3.75e-04	-4.70	0.0	-98.50	-10.48	0.0	0.0	0.0	5.22
		3.93	0.0	0.0	0.0	10.0	-97.31	-15.18	0.0	0.0	0.0	3.93
25	21	6.65	0.0	-1.24e-05	-4.70	0.0	-76.99	7.98	0.0	0.0	0.0	6.08
		6.08	0.0	0.0	0.0	10.0	-75.80	3.29	0.0	0.0	0.0	6.65
26	2	7.12	0.0	-1.08e-05	-4.75	0.0	-75.54	7.04	0.0	0.0	0.0	6.65
		6.65	0.0	0.0	0.0	10.0	-74.58	2.29	0.0	0.0	0.0	7.12
26	3	66.91	0.0	-7.17e-05	-16.65	0.0	-147.83	48.21	0.0	0.0	0.0	62.90
		62.90	0.0	0.0	0.0	10.0	-144.48	31.56	0.0	0.0	0.0	66.91
26	10	1.76	0.0	-6.64e-04	-4.75	0.0	-115.87	-24.23	0.0	0.0	0.0	1.76
		-0.92	0.0	0.0	0.0	10.0	-114.92	-28.98	0.0	0.0	0.0	-0.92
26	12	8.95	0.0	-1.21e-04	-4.75	0.0	-73.06	2.31	0.0	0.0	0.0	8.89
		8.88	0.0	0.0	0.0	10.0	-72.10	-2.44	0.0	0.0	0.0	8.88
26	13	7.12	0.0	-1.08e-05	-4.75	0.0	-75.54	7.04	0.0	0.0	0.0	6.65
		6.65	0.0	0.0	0.0	10.0	-74.58	2.29	0.0	0.0	0.0	7.12
26	14	49.56	0.0	-5.31e-05	-12.34	0.0	-109.50	35.71	0.0	0.0	0.0	46.60
		46.60	0.0	0.0	0.0	10.0	-107.02	23.38	0.0	0.0	0.0	49.56
26	17	3.02	0.0	-4.95e-04	-4.75	0.0	-105.42	-16.12	0.0	0.0	0.0	3.02

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
		1.17	0.0	0.0	0.0	10.0	-104.46	-20.88	0.0	0.0	0.0	1.17
26	18	7.12	0.0	-1.08e-05	-4.75	0.0	-75.54	7.04	0.0	0.0	0.0	6.65
		6.65	0.0	0.0	0.0	10.0	-74.58	2.29	0.0	0.0	0.0	7.12
26	19	38.95	0.0	-4.26e-05	-10.44	0.0	-101.01	28.55	0.0	0.0	0.0	36.61
		36.61	0.0	0.0	0.0	10.0	-98.91	18.11	0.0	0.0	0.0	38.95
26	20	3.93	0.0	-3.74e-04	-4.75	0.0	-97.95	-10.33	0.0	0.0	0.0	3.93
		2.65	0.0	0.0	0.0	10.0	-96.99	-15.08	0.0	0.0	0.0	2.65
26	21	7.12	0.0	-1.08e-05	-4.75	0.0	-75.54	7.04	0.0	0.0	0.0	6.65
		6.65	0.0	0.0	0.0	10.0	-74.58	2.29	0.0	0.0	0.0	7.12
27	2	7.48	0.0	-9.15e-06	-4.79	0.0	-74.38	5.99	0.0	0.0	0.0	7.12
		7.12	0.0	0.0	0.0	10.0	-73.66	1.19	0.0	0.0	0.0	7.48
27	3	69.95	0.0	-5.60e-05	-16.80	0.0	-142.73	38.69	0.0	0.0	0.0	66.91
		66.91	0.0	0.0	0.0	10.0	-140.21	21.89	0.0	0.0	0.0	69.95
27	10	-0.92	0.0	-6.64e-04	-4.79	0.0	-116.21	-23.25	0.0	0.0	0.0	-0.92
		-3.49	0.0	0.0	0.0	10.0	-115.49	-28.04	0.0	0.0	0.0	-3.49
27	12	8.90	0.0	-1.19e-04	-4.79	0.0	-72.50	1.08	0.0	0.0	0.0	8.88
		8.75	0.0	0.0	0.0	10.0	-71.78	-3.71	0.0	0.0	0.0	8.75
27	13	7.48	0.0	-9.15e-06	-4.79	0.0	-74.38	5.99	0.0	0.0	0.0	7.12
		7.12	0.0	0.0	0.0	10.0	-73.66	1.19	0.0	0.0	0.0	7.48
27	14	51.82	0.0	-4.15e-05	-12.44	0.0	-105.73	28.66	0.0	0.0	0.0	49.56
		49.56	0.0	0.0	0.0	10.0	-103.86	16.22	0.0	0.0	0.0	51.82
27	17	1.17	0.0	-4.95e-04	-4.79	0.0	-105.37	-15.67	0.0	0.0	0.0	1.17
		-0.65	0.0	0.0	0.0	10.0	-104.65	-20.46	0.0	0.0	0.0	-0.65
27	18	7.48	0.0	-9.15e-06	-4.79	0.0	-74.38	5.99	0.0	0.0	0.0	7.12
		7.12	0.0	0.0	0.0	10.0	-73.66	1.19	0.0	0.0	0.0	7.48
27	19	40.73	0.0	-3.34e-05	-10.53	0.0	-97.89	22.99	0.0	0.0	0.0	38.95
		38.95	0.0	0.0	0.0	10.0	-96.31	12.46	0.0	0.0	0.0	40.73
27	20	2.65	0.0	-3.73e-04	-4.79	0.0	-97.62	-10.25	0.0	0.0	0.0	2.65
		1.38	0.0	0.0	0.0	10.0	-96.90	-15.05	0.0	0.0	0.0	1.38
27	21	7.48	0.0	-9.15e-06	-4.79	0.0	-74.38	5.99	0.0	0.0	0.0	7.12
		7.12	0.0	0.0	0.0	10.0	-73.66	1.19	0.0	0.0	0.0	7.48
28	2	7.72	0.0	-7.38e-06	-4.82	0.0	-73.51	4.85	0.0	0.0	0.0	7.48
		7.48	0.0	0.0	0.0	10.0	-73.03	0.03	0.0	0.0	0.0	7.72
28	3	72.00	0.0	-3.95e-05	-16.90	0.0	-138.95	28.82	0.0	0.0	0.0	69.95
		69.95	0.0	0.0	0.0	10.0	-137.27	11.92	0.0	0.0	0.0	72.00
28	9	-0.88	0.0	-6.68e-04	-6.51	0.0	-142.47	-20.58	0.0	0.0	0.0	-0.88
		-3.27	0.0	0.0	0.0	10.0	-141.82	-27.09	0.0	0.0	0.0	-3.27
28	10	-3.49	0.0	-6.65e-04	-4.82	0.0	-116.74	-22.27	0.0	0.0	0.0	-3.49
		-5.97	0.0	0.0	0.0	10.0	-116.26	-27.10	0.0	0.0	0.0	-5.97
28	12	8.75	0.0	-1.17e-04	-4.82	0.0	-72.25	-0.18	0.0	0.0	0.0	8.75
		8.49	0.0	0.0	0.0	10.0	-71.77	-5.00	0.0	0.0	0.0	8.49
28	13	7.72	0.0	-7.38e-06	-4.82	0.0	-73.51	4.85	0.0	0.0	0.0	7.48
		7.48	0.0	0.0	0.0	10.0	-73.03	0.03	0.0	0.0	0.0	7.72
28	14	53.33	0.0	-2.93e-05	-12.52	0.0	-102.93	21.35	0.0	0.0	0.0	51.82
		51.82	0.0	0.0	0.0	10.0	-101.68	8.83	0.0	0.0	0.0	53.33
28	17	-0.65	0.0	-4.95e-04	-4.82	0.0	-105.53	-15.24	0.0	0.0	0.0	-0.65
		-2.42	0.0	0.0	0.0	10.0	-105.05	-20.06	0.0	0.0	0.0	-2.42
28	18	7.72	0.0	-7.38e-06	-4.82	0.0	-73.51	4.85	0.0	0.0	0.0	7.48
		7.48	0.0	0.0	0.0	10.0	-73.03	0.03	0.0	0.0	0.0	7.72
28	19	41.93	0.0	-2.38e-05	-10.60	0.0	-95.57	17.23	0.0	0.0	0.0	40.73
		40.73	0.0	0.0	0.0	10.0	-94.52	6.63	0.0	0.0	0.0	41.93
28	20	1.38	0.0	-3.73e-04	-4.82	0.0	-97.53	-10.22	0.0	0.0	0.0	1.38
		0.11	0.0	0.0	0.0	10.0	-97.05	-15.04	0.0	0.0	0.0	0.11
28	21	7.72	0.0	-7.38e-06	-4.82	0.0	-73.51	4.85	0.0	0.0	0.0	7.48
		7.48	0.0	0.0	0.0	10.0	-73.03	0.03	0.0	0.0	0.0	7.72
29	2	7.86	0.0	-5.55e-06	-4.84	0.0	-72.94	3.65	0.0	0.0	0.0	7.72
		7.72	0.0	0.0	0.0	10.0	-72.69	-1.19	0.0	0.0	0.0	7.84
29	3	73.03	0.0	-2.25e-05	-16.97	0.0	-136.51	18.72	0.0	0.0	0.0	72.00
		72.00	0.0	0.0	0.0	10.0	-135.66	1.75	0.0	0.0	0.0	73.03
29	9	-3.27	0.0	-6.69e-04	-6.54	0.0	-142.99	-20.02	0.0	0.0	0.0	-3.27
		-5.61	0.0	0.0	0.0	10.0	-142.67	-26.55	0.0	0.0	0.0	-5.61
29	10	-5.97	0.0	-6.67e-04	-4.84	0.0	-117.46	-21.29	0.0	0.0	0.0	-5.97
		-8.36	0.0	0.0	0.0	10.0	-117.22	-26.14	0.0	0.0	0.0	-8.36
29	12	8.49	0.0	-1.15e-04	-4.84	0.0	-72.31	-1.46	0.0	0.0	0.0	8.49
		8.10	0.0	0.0	0.0	10.0	-72.06	-6.30	0.0	0.0	0.0	8.10
29	13	7.86	0.0	-5.55e-06	-4.84	0.0	-72.94	3.65	0.0	0.0	0.0	7.72
		7.72	0.0	0.0	0.0	10.0	-72.69	-1.19	0.0	0.0	0.0	7.84
29	14	54.10	0.0	-1.67e-05	-12.57	0.0	-101.12	13.86	0.0	0.0	0.0	53.33
		53.33	0.0	0.0	0.0	10.0	-100.49	1.30	0.0	0.0	0.0	54.10
29	17	-2.42	0.0	-4.95e-04	-4.84	0.0	-105.92	-14.83	0.0	0.0	0.0	-2.42
		-4.16	0.0	0.0	0.0	10.0	-105.68	-19.67	0.0	0.0	0.0	-4.16
29	18	7.86	0.0	-5.55e-06	-4.84	0.0	-72.94	3.65	0.0	0.0	0.0	7.72
		7.72	0.0	0.0	0.0	10.0	-72.69	-1.19	0.0	0.0	0.0	7.84

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
29	19	42.53	0.0	-1.39e-05	-10.64	0.0	-94.07	11.31	0.0	0.0	0.0	41.93
		41.93	0.0	0.0	0.0	10.0	-93.54	0.67	0.0	0.0	0.0	42.53
29	20	0.11	0.0	-3.73e-04	-4.84	0.0	-97.67	-10.21	0.0	0.0	0.0	0.11
		-1.16	0.0	0.0	0.0	10.0	-97.43	-15.05	0.0	0.0	0.0	-1.16
29	21	7.86	0.0	-5.55e-06	-4.84	0.0	-72.94	3.65	0.0	0.0	0.0	7.72
		7.72	0.0	0.0	0.0	10.0	-72.69	-1.19	0.0	0.0	0.0	7.84
30	2	7.90	0.0	-3.70e-06	-4.85	0.0	-72.66	2.42	0.0	0.0	0.0	7.84
		7.84	0.0	0.0	0.0	10.0	-72.66	-2.43	0.0	0.0	0.0	7.84
30	3	73.24	0.0	-5.68e-06	-16.99	0.0	-135.41	8.48	0.0	0.0	0.0	73.03
		73.03	0.0	0.0	0.0	10.0	-135.41	-8.51	0.0	0.0	0.0	73.03
30	9	-5.61	0.0	-6.70e-04	-6.54	0.0	-143.81	-19.44	0.0	0.0	0.0	-5.61
		-7.89	0.0	0.0	0.0	10.0	-143.81	-25.98	0.0	0.0	0.0	-7.89
30	10	-8.36	0.0	-6.69e-04	-4.85	0.0	-118.38	-20.28	0.0	0.0	0.0	-8.36
		-10.64	0.0	0.0	0.0	10.0	-118.38	-25.13	0.0	0.0	0.0	-10.64
30	12	8.10	0.0	-1.13e-04	-4.85	0.0	-72.66	-2.71	0.0	0.0	0.0	8.10
		7.59	0.0	0.0	0.0	10.0	-72.66	-7.56	0.0	0.0	0.0	7.59
30	13	7.90	0.0	-3.70e-06	-4.85	0.0	-72.66	2.42	0.0	0.0	0.0	7.84
		7.84	0.0	0.0	0.0	10.0	-72.66	-2.43	0.0	0.0	0.0	7.84
30	14	54.25	0.0	-4.20e-06	-12.58	0.0	-100.30	6.28	0.0	0.0	0.0	54.10
		54.09	0.0	0.0	0.0	10.0	-100.30	-6.30	0.0	0.0	0.0	54.09
30	17	-4.16	0.0	-4.96e-04	-4.85	0.0	-106.52	-14.40	0.0	0.0	0.0	-4.16
		-5.85	0.0	0.0	0.0	10.0	-106.52	-19.25	0.0	0.0	0.0	-5.85
30	18	7.90	0.0	-3.70e-06	-4.85	0.0	-72.66	2.42	0.0	0.0	0.0	7.84
		7.84	0.0	0.0	0.0	10.0	-72.66	-2.43	0.0	0.0	0.0	7.84
30	19	42.67	0.0	-3.97e-06	-10.65	0.0	-93.39	5.32	0.0	0.0	0.0	42.53
		42.53	0.0	0.0	0.0	10.0	-93.39	-5.33	0.0	0.0	0.0	42.53
30	20	-1.16	0.0	-3.73e-04	-4.85	0.0	-98.06	-10.20	0.0	0.0	0.0	-1.16
		-2.42	0.0	0.0	0.0	10.0	-98.06	-15.04	0.0	0.0	0.0	-2.42
30	21	7.90	0.0	-3.70e-06	-4.85	0.0	-72.66	2.42	0.0	0.0	0.0	7.84
		7.84	0.0	0.0	0.0	10.0	-72.66	-2.43	0.0	0.0	0.0	7.84
31	2	7.86	0.0	-1.84e-06	-4.84	0.0	-72.70	1.18	0.0	0.0	0.0	7.84
		7.72	0.0	0.0	0.0	10.0	-72.94	-3.66	0.0	0.0	0.0	7.72
31	3	73.03	0.0	1.18e-05	-16.97	0.0	-135.67	-1.78	0.0	0.0	0.0	73.03
		72.00	0.0	0.0	0.0	10.0	-136.51	-18.74	0.0	0.0	0.0	72.00
31	9	-7.89	0.0	-6.72e-04	-6.54	0.0	-144.92	-18.81	0.0	0.0	0.0	-7.89
		-10.11	0.0	0.0	0.0	10.0	-145.24	-25.35	0.0	0.0	0.0	-10.11
31	10	-10.64	0.0	-6.71e-04	-4.84	0.0	-119.48	-19.23	0.0	0.0	0.0	-10.64
		-12.81	0.0	0.0	0.0	10.0	-119.72	-24.07	0.0	0.0	0.0	-12.81
31	12	7.59	0.0	-1.11e-04	-4.84	0.0	-73.32	-3.93	0.0	0.0	0.0	7.59
		6.95	0.0	0.0	0.0	10.0	-73.56	-8.77	0.0	0.0	0.0	6.95
31	13	7.86	0.0	-1.84e-06	-4.84	0.0	-72.70	1.18	0.0	0.0	0.0	7.84
		7.72	0.0	0.0	0.0	10.0	-72.94	-3.66	0.0	0.0	0.0	7.72
31	14	54.09	0.0	8.78e-06	-12.57	0.0	-100.49	-1.32	0.0	0.0	0.0	54.09
		53.33	0.0	0.0	0.0	10.0	-101.12	-13.88	0.0	0.0	0.0	53.33
31	17	-5.85	0.0	-4.98e-04	-4.84	0.0	-107.35	-13.94	0.0	0.0	0.0	-5.85
		-7.49	0.0	0.0	0.0	10.0	-107.59	-18.78	0.0	0.0	0.0	-7.49
31	18	7.86	0.0	-1.84e-06	-4.84	0.0	-72.70	1.18	0.0	0.0	0.0	7.84
		7.72	0.0	0.0	0.0	10.0	-72.94	-3.66	0.0	0.0	0.0	7.72
31	19	42.53	0.0	6.12e-06	-10.64	0.0	-93.54	-0.69	0.0	0.0	0.0	42.53
		41.93	0.0	0.0	0.0	10.0	-94.07	-11.33	0.0	0.0	0.0	41.93
31	20	-2.42	0.0	-3.74e-04	-4.84	0.0	-98.68	-10.16	0.0	0.0	0.0	-2.42
		-3.69	0.0	0.0	0.0	10.0	-98.93	-15.00	0.0	0.0	0.0	-3.69
31	21	7.86	0.0	-1.84e-06	-4.84	0.0	-72.70	1.18	0.0	0.0	0.0	7.84
		7.72	0.0	0.0	0.0	10.0	-72.94	-3.66	0.0	0.0	0.0	7.72
32	2	7.72	0.0	0.0	-4.82	0.0	-73.03	-0.04	0.0	0.0	0.0	7.72
		7.47	0.0	0.0	0.0	10.0	-73.51	-4.86	0.0	0.0	0.0	7.47
32	3	72.00	0.0	2.88e-05	-16.90	0.0	-137.27	-11.95	0.0	0.0	0.0	72.00
		69.95	0.0	0.0	0.0	10.0	-138.95	-28.85	0.0	0.0	0.0	69.95
32	9	-10.11	0.0	-6.74e-04	-6.51	0.0	-146.32	-18.11	0.0	0.0	0.0	-10.11
		-12.26	0.0	0.0	0.0	10.0	-146.97	-24.62	0.0	0.0	0.0	-12.26
32	10	-12.81	0.0	-6.74e-04	-4.82	0.0	-120.76	-18.10	0.0	0.0	0.0	-12.81
		-14.87	0.0	0.0	0.0	10.0	-121.24	-22.92	0.0	0.0	0.0	-14.87
32	12	6.95	0.0	-1.09e-04	-4.82	0.0	-74.28	-5.07	0.0	0.0	0.0	6.95
		6.20	0.0	0.0	0.0	10.0	-74.76	-9.89	0.0	0.0	0.0	6.20
32	13	7.72	0.0	0.0	-4.82	0.0	-73.03	-0.04	0.0	0.0	0.0	7.72
		7.47	0.0	0.0	0.0	10.0	-73.51	-4.86	0.0	0.0	0.0	7.47
32	14	53.33	0.0	2.13e-05	-12.52	0.0	-101.68	-8.85	0.0	0.0	0.0	53.33
		51.81	0.0	0.0	0.0	10.0	-102.93	-21.37	0.0	0.0	0.0	51.81
32	17	-7.49	0.0	-4.99e-04	-4.82	0.0	-108.39	-13.42	0.0	0.0	0.0	-7.49
		-9.08	0.0	0.0	0.0	10.0	-108.87	-18.24	0.0	0.0	0.0	-9.08
32	18	7.72	0.0	0.0	-4.82	0.0	-73.03	-0.04	0.0	0.0	0.0	7.72
		7.47	0.0	0.0	0.0	10.0	-73.51	-4.86	0.0	0.0	0.0	7.47
32	19	41.93	0.0	1.60e-05	-10.60	0.0	-94.52	-6.65	0.0	0.0	0.0	41.93

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
32	20	40.73	0.0	0.0	0.0	10.0	-95.57	-17.24	0.0	0.0	0.0	40.73
		-3.69	0.0	-3.74e-04	-4.82	0.0	-99.55	-10.07	0.0	0.0	0.0	-3.69
		-4.94	0.0	0.0	0.0	10.0	-100.03	-14.90	0.0	0.0	0.0	-4.94
32	21	7.72	0.0	0.0	-4.82	0.0	-73.03	-0.04	0.0	0.0	0.0	7.72
		7.47	0.0	0.0	0.0	10.0	-73.51	-4.86	0.0	0.0	0.0	7.47
33	2	7.47	0.0	1.76e-06	-4.79	0.0	-73.66	-1.21	0.0	0.0	0.0	7.47
		7.11	0.0	0.0	0.0	10.0	-74.38	-6.00	0.0	0.0	0.0	7.11
33	3	69.95	0.0	4.53e-05	-16.80	0.0	-140.22	-21.92	0.0	0.0	0.0	69.95
		66.90	0.0	0.0	0.0	10.0	-142.74	-38.72	0.0	0.0	0.0	66.90
33	9	-12.26	0.0	-6.77e-04	-6.47	0.0	-148.01	-17.30	0.0	0.0	0.0	-12.26
		-14.32	0.0	0.0	0.0	10.0	-148.98	-23.77	0.0	0.0	0.0	-14.32
33	10	-14.87	0.0	-6.77e-04	-4.79	0.0	-122.23	-16.87	0.0	0.0	0.0	-14.87
		-16.81	0.0	0.0	0.0	10.0	-122.95	-21.67	0.0	0.0	0.0	-16.81
33	12	6.20	0.0	-1.08e-04	-4.79	0.0	-75.53	-6.11	0.0	0.0	0.0	6.20
		5.34	0.0	0.0	0.0	10.0	-76.25	-10.91	0.0	0.0	0.0	5.34
33	13	7.47	0.0	1.76e-06	-4.79	0.0	-73.66	-1.21	0.0	0.0	0.0	7.47
		7.11	0.0	0.0	0.0	10.0	-74.38	-6.00	0.0	0.0	0.0	7.11
33	14	51.81	0.0	3.35e-05	-12.44	0.0	-103.86	-16.24	0.0	0.0	0.0	51.81
		49.56	0.0	0.0	0.0	10.0	-105.73	-28.68	0.0	0.0	0.0	49.56
33	17	-9.08	0.0	-5.01e-04	-4.79	0.0	-109.64	-12.81	0.0	0.0	0.0	-9.08
		-10.61	0.0	0.0	0.0	10.0	-110.36	-17.61	0.0	0.0	0.0	-10.61
33	18	7.47	0.0	1.76e-06	-4.79	0.0	-73.66	-1.21	0.0	0.0	0.0	7.47
		7.11	0.0	0.0	0.0	10.0	-74.38	-6.00	0.0	0.0	0.0	7.11
33	19	40.73	0.0	2.56e-05	-10.53	0.0	-96.31	-12.48	0.0	0.0	0.0	40.73
		38.95	0.0	0.0	0.0	10.0	-97.89	-23.01	0.0	0.0	0.0	38.95
33	20	-4.94	0.0	-3.76e-04	-4.79	0.0	-100.64	-9.91	0.0	0.0	0.0	-4.94
		-6.18	0.0	0.0	0.0	10.0	-101.36	-14.71	0.0	0.0	0.0	-6.18
33	21	7.47	0.0	1.76e-06	-4.79	0.0	-73.66	-1.21	0.0	0.0	0.0	7.47
		7.11	0.0	0.0	0.0	10.0	-74.38	-6.00	0.0	0.0	0.0	7.11
34	2	7.11	0.0	3.44e-06	-4.75	0.0	-74.58	-2.30	0.0	0.0	0.0	7.11
		6.64	0.0	0.0	0.0	10.0	-75.54	-7.06	0.0	0.0	0.0	6.64
34	3	66.90	0.0	6.10e-05	-16.65	0.0	-144.48	-31.59	0.0	0.0	0.0	66.90
		62.89	0.0	0.0	0.0	10.0	-147.83	-48.24	0.0	0.0	0.0	62.89
34	9	-14.32	0.0	-6.80e-04	-6.42	0.0	-149.98	-16.35	0.0	0.0	0.0	-14.32
		-16.28	0.0	0.0	0.0	10.0	-151.27	-22.76	0.0	0.0	0.0	-16.28
34	10	-16.81	0.0	-6.81e-04	-4.75	0.0	-123.88	-15.54	0.0	0.0	0.0	-16.81
		-18.61	0.0	0.0	0.0	10.0	-124.83	-20.29	0.0	0.0	0.0	-18.61
34	12	5.34	0.0	-1.07e-04	-4.75	0.0	-77.06	-7.04	0.0	0.0	0.0	5.34
		4.40	0.0	0.0	0.0	10.0	-78.02	-11.79	0.0	0.0	0.0	4.40
34	13	7.11	0.0	3.44e-06	-4.75	0.0	-74.58	-2.30	0.0	0.0	0.0	7.11
		6.64	0.0	0.0	0.0	10.0	-75.54	-7.06	0.0	0.0	0.0	6.64
34	14	49.56	0.0	4.52e-05	-12.34	0.0	-107.02	-23.40	0.0	0.0	0.0	49.56
		46.59	0.0	0.0	0.0	10.0	-109.51	-35.73	0.0	0.0	0.0	46.59
34	17	-10.61	0.0	-5.04e-04	-4.75	0.0	-111.10	-12.11	0.0	0.0	0.0	-10.61
		-12.06	0.0	0.0	0.0	10.0	-112.05	-16.86	0.0	0.0	0.0	-12.06
34	18	7.11	0.0	3.44e-06	-4.75	0.0	-74.58	-2.30	0.0	0.0	0.0	7.11
		6.64	0.0	0.0	0.0	10.0	-75.54	-7.06	0.0	0.0	0.0	6.64
34	19	38.95	0.0	3.48e-05	-10.44	0.0	-98.91	-18.12	0.0	0.0	0.0	38.95
		36.60	0.0	0.0	0.0	10.0	-101.01	-28.57	0.0	0.0	0.0	36.60
34	20	-6.18	0.0	-3.77e-04	-4.75	0.0	-101.97	-9.66	0.0	0.0	0.0	-6.18
		-7.39	0.0	0.0	0.0	10.0	-102.93	-14.41	0.0	0.0	0.0	-7.39
34	21	7.11	0.0	3.44e-06	-4.75	0.0	-74.58	-2.30	0.0	0.0	0.0	7.11
		6.64	0.0	0.0	0.0	10.0	-75.54	-7.06	0.0	0.0	0.0	6.64
35	2	6.64	0.0	5.01e-06	-4.70	0.0	-75.80	-3.30	0.0	0.0	0.0	6.64
		6.07	0.0	0.0	0.0	10.0	-76.99	-8.00	0.0	0.0	0.0	6.07
35	3	62.89	0.0	7.59e-05	-16.47	0.0	-150.05	-40.85	0.0	0.0	0.0	62.89
		57.96	0.0	0.0	0.0	10.0	-154.22	-57.31	0.0	0.0	0.0	57.96
35	9	-16.28	0.0	-6.84e-04	-6.34	0.0	-152.22	-15.23	0.0	0.0	0.0	-16.28
		-18.13	0.0	0.0	0.0	10.0	-153.82	-21.57	0.0	0.0	0.0	-18.13
35	10	-18.61	0.0	-6.86e-04	-4.70	0.0	-125.69	-14.07	0.0	0.0	0.0	-18.61
		-20.26	0.0	0.0	0.0	10.0	-126.88	-18.77	0.0	0.0	0.0	-20.26
35	12	4.40	0.0	-1.06e-04	-4.70	0.0	-78.87	-7.81	0.0	0.0	0.0	4.40
		3.38	0.0	0.0	0.0	10.0	-80.06	-12.51	0.0	0.0	0.0	3.38
35	13	6.64	0.0	5.01e-06	-4.70	0.0	-75.80	-3.30	0.0	0.0	0.0	6.64
		6.07	0.0	0.0	0.0	10.0	-76.99	-8.00	0.0	0.0	0.0	6.07
35	14	46.59	0.0	5.62e-05	-12.20	0.0	-111.14	-30.26	0.0	0.0	0.0	46.59
		42.93	0.0	0.0	0.0	10.0	-114.24	-42.45	0.0	0.0	0.0	42.93
35	17	-12.06	0.0	-5.07e-04	-4.70	0.0	-112.75	-11.28	0.0	0.0	0.0	-12.06
		-13.43	0.0	0.0	0.0	10.0	-113.94	-15.98	0.0	0.0	0.0	-13.43
35	18	6.64	0.0	5.01e-06	-4.70	0.0	-75.80	-3.30	0.0	0.0	0.0	6.64
		6.07	0.0	0.0	0.0	10.0	-76.99	-8.00	0.0	0.0	0.0	6.07
35	19	36.60	0.0	4.34e-05	-10.32	0.0	-102.31	-23.52	0.0	0.0	0.0	36.60
		33.72	0.0	0.0	0.0	10.0	-104.92	-33.84	0.0	0.0	0.0	33.72

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
35	20	-7.39	0.0	-3.79e-04	-4.70	0.0	-103.51	-9.28	0.0	0.0	0.0	-7.39
		-8.56	0.0	0.0	0.0	10.0	-104.70	-13.98	0.0	0.0	0.0	-8.56
35	21	6.64	0.0	5.01e-06	-4.70	0.0	-75.80	-3.30	0.0	0.0	0.0	6.64
		6.07	0.0	0.0	0.0	10.0	-76.99	-8.00	0.0	0.0	0.0	6.07
36	2	6.07	0.0	6.45e-06	-4.63	0.0	-77.29	-4.17	0.0	0.0	0.0	6.07
		5.42	0.0	0.0	0.0	10.0	-78.71	-8.80	0.0	0.0	0.0	5.42
36	3	57.96	0.0	8.95e-05	-16.24	0.0	-156.87	-49.59	0.0	0.0	0.0	57.96
		52.16	0.0	0.0	0.0	10.0	-161.86	-65.83	0.0	0.0	0.0	52.16
36	9	-18.13	0.0	-6.88e-04	-6.26	0.0	-154.70	-13.91	0.0	0.0	0.0	-18.13
		-19.84	0.0	0.0	0.0	10.0	-156.62	-20.17	0.0	0.0	0.0	-19.84
36	10	-20.26	0.0	-6.90e-04	-4.63	0.0	-127.65	-12.45	0.0	0.0	0.0	-20.26
		-21.74	0.0	0.0	0.0	10.0	-129.07	-17.09	0.0	0.0	0.0	-21.74
36	12	3.38	0.0	-1.05e-04	-4.63	0.0	-80.93	-8.41	0.0	0.0	0.0	3.38
		2.30	0.0	0.0	0.0	10.0	-82.36	-13.05	0.0	0.0	0.0	2.30
36	13	6.07	0.0	6.45e-06	-4.63	0.0	-77.29	-4.17	0.0	0.0	0.0	6.07
		5.42	0.0	0.0	0.0	10.0	-78.71	-8.80	0.0	0.0	0.0	5.42
36	14	42.93	0.0	6.63e-05	-12.03	0.0	-116.20	-36.73	0.0	0.0	0.0	42.93
		38.64	0.0	0.0	0.0	10.0	-119.90	-48.76	0.0	0.0	0.0	38.64
36	17	-13.43	0.0	-5.10e-04	-4.63	0.0	-114.60	-10.30	0.0	0.0	0.0	-13.43
		-14.70	0.0	0.0	0.0	10.0	-116.02	-14.94	0.0	0.0	0.0	-14.70
36	18	6.07	0.0	6.45e-06	-4.63	0.0	-77.29	-4.17	0.0	0.0	0.0	6.07
		5.42	0.0	0.0	0.0	10.0	-78.71	-8.80	0.0	0.0	0.0	5.42
36	19	33.72	0.0	5.14e-05	-10.18	0.0	-106.48	-28.59	0.0	0.0	0.0	33.72
		30.33	0.0	0.0	0.0	10.0	-109.60	-38.77	0.0	0.0	0.0	30.33
36	20	-8.56	0.0	-3.81e-04	-4.63	0.0	-105.27	-8.77	0.0	0.0	0.0	-8.56
		-9.67	0.0	0.0	0.0	10.0	-106.69	-13.40	0.0	0.0	0.0	-9.67
36	21	6.07	0.0	6.45e-06	-4.63	0.0	-77.29	-4.17	0.0	0.0	0.0	6.07
		5.42	0.0	0.0	0.0	10.0	-78.71	-8.80	0.0	0.0	0.0	5.42
37	2	5.42	0.0	7.73e-06	-4.56	0.0	-79.05	-4.88	0.0	0.0	0.0	5.42
		4.70	0.0	0.0	0.0	10.0	-80.71	-9.44	0.0	0.0	0.0	4.70
37	3	52.16	0.0	1.02e-04	-15.97	0.0	-164.93	-57.71	0.0	0.0	0.0	52.16
		45.56	0.0	0.0	0.0	10.0	-170.71	-73.69	0.0	0.0	0.0	45.56
37	9	-19.84	0.0	-6.93e-04	-6.15	0.0	-157.43	-12.37	0.0	0.0	0.0	-19.84
		-21.40	0.0	0.0	0.0	10.0	-159.66	-18.52	0.0	0.0	0.0	-21.40
37	10	-21.74	0.0	-6.96e-04	-4.56	0.0	-129.76	-10.66	0.0	0.0	0.0	-21.74
		-23.04	0.0	0.0	0.0	10.0	-131.42	-15.22	0.0	0.0	0.0	-23.04
37	12	2.30	0.0	-1.04e-04	-4.56	0.0	-83.25	-8.82	0.0	0.0	0.0	2.30
		1.18	0.0	0.0	0.0	10.0	-84.90	-13.38	0.0	0.0	0.0	1.18
37	13	5.42	0.0	7.73e-06	-4.56	0.0	-79.05	-4.88	0.0	0.0	0.0	5.42
		4.70	0.0	0.0	0.0	10.0	-80.71	-9.44	0.0	0.0	0.0	4.70
37	14	38.64	0.0	7.54e-05	-11.83	0.0	-122.17	-42.75	0.0	0.0	0.0	38.64
		33.75	0.0	0.0	0.0	10.0	-126.45	-54.58	0.0	0.0	0.0	33.75
37	17	-14.70	0.0	-5.13e-04	-4.56	0.0	-116.62	-9.16	0.0	0.0	0.0	-14.70
		-15.85	0.0	0.0	0.0	10.0	-118.27	-13.72	0.0	0.0	0.0	-15.85
37	18	5.42	0.0	7.73e-06	-4.56	0.0	-79.05	-4.88	0.0	0.0	0.0	5.42
		4.70	0.0	0.0	0.0	10.0	-80.71	-9.44	0.0	0.0	0.0	4.70
37	19	30.33	0.0	5.85e-05	-10.01	0.0	-111.39	-33.28	0.0	0.0	0.0	30.33
		26.49	0.0	0.0	0.0	10.0	-115.02	-43.30	0.0	0.0	0.0	26.49
37	20	-9.67	0.0	-3.83e-04	-4.56	0.0	-107.23	-8.09	0.0	0.0	0.0	-9.67
		-10.71	0.0	0.0	0.0	10.0	-108.88	-12.65	0.0	0.0	0.0	-10.71
37	21	5.42	0.0	7.73e-06	-4.56	0.0	-79.05	-4.88	0.0	0.0	0.0	5.42
		4.70	0.0	0.0	0.0	10.0	-80.71	-9.44	0.0	0.0	0.0	4.70
38	2	4.70	0.0	8.84e-06	-4.47	0.0	-81.07	-5.42	0.0	0.0	0.0	4.70
		3.93	0.0	0.0	0.0	10.0	-82.95	-9.89	0.0	0.0	0.0	3.93
38	3	45.56	0.0	1.13e-04	-15.67	0.0	-174.16	-65.12	0.0	0.0	0.0	45.56
		38.23	0.0	0.0	0.0	10.0	-180.73	-80.79	0.0	0.0	0.0	38.23
38	9	-21.40	0.0	-6.98e-04	-6.03	0.0	-160.38	-10.57	0.0	0.0	0.0	-21.40
		-22.76	0.0	0.0	0.0	10.0	-162.92	-16.61	0.0	0.0	0.0	-22.76
38	10	-23.04	0.0	-7.01e-04	-4.47	0.0	-132.01	-8.68	0.0	0.0	0.0	-23.04
		-24.14	0.0	0.0	0.0	10.0	-133.88	-13.15	0.0	0.0	0.0	-24.14
38	12	1.18	0.0	-1.04e-04	-4.47	0.0	-85.79	-9.01	0.0	0.0	0.0	1.18
		0.05	0.0	0.0	0.0	10.0	-87.67	-13.48	0.0	0.0	0.0	0.05
38	13	4.70	0.0	8.84e-06	-4.47	0.0	-81.07	-5.42	0.0	0.0	0.0	4.70
		3.93	0.0	0.0	0.0	10.0	-82.95	-9.89	0.0	0.0	0.0	3.93
38	14	33.75	0.0	8.34e-05	-11.60	0.0	-129.01	-48.24	0.0	0.0	0.0	33.75
		28.32	0.0	0.0	0.0	10.0	-133.88	-59.84	0.0	0.0	0.0	28.32
38	17	-15.85	0.0	-5.17e-04	-4.47	0.0	-118.80	-7.83	0.0	0.0	0.0	-15.85
		-16.86	0.0	0.0	0.0	10.0	-120.68	-12.30	0.0	0.0	0.0	-16.86
38	18	4.70	0.0	8.84e-06	-4.47	0.0	-81.07	-5.42	0.0	0.0	0.0	4.70
		3.93	0.0	0.0	0.0	10.0	-82.95	-9.89	0.0	0.0	0.0	3.93
38	19	26.49	0.0	6.48e-05	-9.82	0.0	-117.02	-37.54	0.0	0.0	0.0	26.49
		22.22	0.0	0.0	0.0	10.0	-121.14	-47.36	0.0	0.0	0.0	22.22
38	20	-10.71	0.0	-3.85e-04	-4.47	0.0	-109.37	-7.23	0.0	0.0	0.0	-10.71

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
38	21	-11.66	0.0	0.0	0.0	10.0	-111.25	-11.70	0.0	0.0	0.0	-11.66
		4.70	0.0	8.84e-06	-4.47	0.0	-81.07	-5.42	0.0	0.0	0.0	4.70
		3.93	0.0	0.0	0.0	10.0	-82.95	-9.89	0.0	0.0	0.0	3.93
39	2	3.93	0.0	9.76e-06	-4.37	0.0	-83.34	-5.76	0.0	0.0	0.0	3.93
		3.13	0.0	0.0	0.0	10.0	-85.43	-10.14	0.0	0.0	0.0	3.13
39	3	38.23	0.0	1.22e-04	-15.32	0.0	-184.52	-71.72	0.0	0.0	0.0	38.23
		30.26	0.0	0.0	0.0	10.0	-191.86	-87.04	0.0	0.0	0.0	30.26
39	9	-22.76	0.0	-7.03e-04	-5.90	0.0	-163.54	-8.50	0.0	0.0	0.0	-22.76
		-23.91	0.0	0.0	0.0	10.0	-166.37	-14.40	0.0	0.0	0.0	-23.91
39	10	-24.14	0.0	-7.07e-04	-4.37	0.0	-134.37	-6.48	0.0	0.0	0.0	-24.14
		-25.01	0.0	0.0	0.0	10.0	-136.47	-10.86	0.0	0.0	0.0	-25.01
39	12	0.05	0.0	-1.04e-04	-4.37	0.0	-88.56	-8.95	0.0	0.0	0.0	0.05
		-1.07	0.0	0.0	0.0	10.0	-90.65	-13.32	0.0	0.0	0.0	-1.07
39	13	3.93	0.0	9.76e-06	-4.37	0.0	-83.34	-5.76	0.0	0.0	0.0	3.93
		3.13	0.0	0.0	0.0	10.0	-85.43	-10.14	0.0	0.0	0.0	3.13
39	14	28.32	0.0	9.01e-05	-11.35	0.0	-136.68	-53.13	0.0	0.0	0.0	28.32
		22.41	0.0	0.0	0.0	10.0	-142.12	-64.47	0.0	0.0	0.0	22.41
39	17	-16.86	0.0	-5.21e-04	-4.37	0.0	-121.14	-6.30	0.0	0.0	0.0	-16.86
		-17.71	0.0	0.0	0.0	10.0	-123.24	-10.67	0.0	0.0	0.0	-17.71
39	18	3.93	0.0	9.76e-06	-4.37	0.0	-83.34	-5.76	0.0	0.0	0.0	3.93
		3.13	0.0	0.0	0.0	10.0	-85.43	-10.14	0.0	0.0	0.0	3.13
39	19	22.22	0.0	7.00e-05	-9.60	0.0	-123.35	-41.28	0.0	0.0	0.0	22.22
		17.59	0.0	0.0	0.0	10.0	-127.95	-50.89	0.0	0.0	0.0	17.59
39	20	-11.66	0.0	-3.88e-04	-4.37	0.0	-111.69	-6.16	0.0	0.0	0.0	-11.66
		-12.50	0.0	0.0	0.0	10.0	-113.78	-10.54	0.0	0.0	0.0	-12.50
39	21	3.93	0.0	9.76e-06	-4.37	0.0	-83.34	-5.76	0.0	0.0	0.0	3.93
		3.13	0.0	0.0	0.0	10.0	-85.43	-10.14	0.0	0.0	0.0	3.13
40	2	3.13	0.0	1.05e-05	-4.26	0.0	-85.83	-5.88	0.0	0.0	0.0	3.13
		2.33	0.0	0.0	0.0	10.0	-88.14	-10.15	0.0	0.0	0.0	2.33
40	3	30.26	0.0	1.29e-04	-14.94	0.0	-195.94	-77.41	0.0	0.0	0.0	30.26
		21.73	0.0	0.0	0.0	10.0	-204.04	-92.35	0.0	0.0	0.0	21.73
40	9	-23.91	0.0	-7.09e-04	-5.75	0.0	-166.88	-6.13	0.0	0.0	0.0	-23.91
		-24.82	0.0	0.0	0.0	10.0	-169.99	-11.88	0.0	0.0	0.0	-24.82
40	10	-25.01	0.0	-7.12e-04	-4.26	0.0	-136.84	-4.07	0.0	0.0	0.0	-25.01
		-25.63	0.0	0.0	0.0	10.0	-139.15	-8.33	0.0	0.0	0.0	-25.63
40	12	-1.07	0.0	-1.04e-04	-4.26	0.0	-91.51	-8.64	0.0	0.0	0.0	-1.07
		-2.15	0.0	0.0	0.0	10.0	-93.82	-12.90	0.0	0.0	0.0	-2.15
40	13	3.13	0.0	1.05e-05	-4.26	0.0	-85.83	-5.88	0.0	0.0	0.0	3.13
		2.33	0.0	0.0	0.0	10.0	-88.14	-10.15	0.0	0.0	0.0	2.33
40	14	22.41	0.0	9.54e-05	-11.06	0.0	-145.14	-57.34	0.0	0.0	0.0	22.41
		16.10	0.0	0.0	0.0	10.0	-151.14	-68.40	0.0	0.0	0.0	16.10
40	17	-17.71	0.0	-5.25e-04	-4.26	0.0	-123.61	-4.54	0.0	0.0	0.0	-17.71
		-18.38	0.0	0.0	0.0	10.0	-125.92	-8.80	0.0	0.0	0.0	-18.38
40	18	3.13	0.0	1.05e-05	-4.26	0.0	-85.83	-5.88	0.0	0.0	0.0	3.13
		2.33	0.0	0.0	0.0	10.0	-88.14	-10.15	0.0	0.0	0.0	2.33
40	19	17.59	0.0	7.42e-05	-9.36	0.0	-130.32	-44.48	0.0	0.0	0.0	17.59
		12.65	0.0	0.0	0.0	10.0	-135.39	-53.84	0.0	0.0	0.0	12.65
40	20	-12.50	0.0	-3.91e-04	-4.26	0.0	-114.17	-4.88	0.0	0.0	0.0	-12.50
		-13.21	0.0	0.0	0.0	10.0	-116.48	-9.14	0.0	0.0	0.0	-13.21
40	21	3.13	0.0	1.05e-05	-4.26	0.0	-85.83	-5.88	0.0	0.0	0.0	3.13
		2.33	0.0	0.0	0.0	10.0	-88.14	-10.15	0.0	0.0	0.0	2.33
41	2	2.33	0.0	1.10e-05	-4.14	0.0	-88.53	-5.76	0.0	0.0	0.0	2.33
		1.54	0.0	0.0	0.0	10.0	-91.05	-9.90	0.0	0.0	0.0	1.54
41	3	21.73	0.0	1.34e-04	-14.52	0.0	-208.37	-82.11	0.0	0.0	0.0	21.73
		12.75	0.0	0.0	0.0	10.0	-217.19	-96.62	0.0	0.0	0.0	12.75
41	9	-24.82	0.0	-7.14e-04	-5.59	0.0	-170.37	-3.43	0.0	0.0	0.0	-24.82
		-25.44	0.0	0.0	0.0	10.0	-173.77	-9.02	0.0	0.0	0.0	-25.44
41	10	-25.63	0.0	-7.18e-04	-4.14	0.0	-139.39	-1.42	0.0	0.0	0.0	-25.63
		-25.98	0.0	0.0	0.0	10.0	-141.91	-5.56	0.0	0.0	0.0	-25.98
41	12	-2.15	0.0	-1.05e-04	-4.14	0.0	-94.65	-8.05	0.0	0.0	0.0	-2.15
		-3.16	0.0	0.0	0.0	10.0	-97.17	-12.19	0.0	0.0	0.0	-3.16
41	13	2.33	0.0	1.10e-05	-4.14	0.0	-88.53	-5.76	0.0	0.0	0.0	2.33
		1.54	0.0	0.0	0.0	10.0	-91.05	-9.90	0.0	0.0	0.0	1.54
41	14	16.10	0.0	9.93e-05	-10.75	0.0	-154.35	-60.82	0.0	0.0	0.0	16.10
		9.44	0.0	0.0	0.0	10.0	-160.88	-71.57	0.0	0.0	0.0	9.44
41	17	-18.38	0.0	-5.29e-04	-4.14	0.0	-126.20	-2.54	0.0	0.0	0.0	-18.38
		-18.85	0.0	0.0	0.0	10.0	-128.72	-6.69	0.0	0.0	0.0	-18.85
41	18	2.33	0.0	1.10e-05	-4.14	0.0	-88.53	-5.76	0.0	0.0	0.0	2.33
		1.54	0.0	0.0	0.0	10.0	-91.05	-9.90	0.0	0.0	0.0	1.54
41	19	12.65	0.0	7.72e-05	-9.10	0.0	-137.89	-47.05	0.0	0.0	0.0	12.65
		7.47	0.0	0.0	0.0	10.0	-143.42	-56.16	0.0	0.0	0.0	7.47
41	20	-13.21	0.0	-3.94e-04	-4.14	0.0	-116.79	-3.35	0.0	0.0	0.0	-13.21
		-13.75	0.0	0.0	0.0	10.0	-119.30	-7.49	0.0	0.0	0.0	-13.75

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
41	21	2.33	0.0	1.10e-05	-4.14	0.0	-88.53	-5.76	0.0	0.0	0.0	2.33
		1.54	0.0	0.0	0.0	10.0	-91.05	-9.90	0.0	0.0	0.0	1.54
42	2	1.54	0.0	1.14e-05	-4.01	0.0	-91.43	-5.37	0.0	0.0	0.0	1.54
		0.80	0.0	0.0	0.0	10.0	-94.15	-9.38	0.0	0.0	0.0	0.80
42	3	12.75	0.0	1.37e-04	-14.06	0.0	-221.72	-85.72	0.0	0.0	0.0	12.75
		3.43	0.0	0.0	0.0	10.0	-231.25	-99.79	0.0	0.0	0.0	3.43
42	9	-25.44	0.0	-7.20e-04	-5.42	0.0	-174.01	-0.39	0.0	0.0	0.0	-25.44
		-25.75	0.0	0.0	0.0	10.0	-177.68	-5.81	0.0	0.0	0.0	-25.75
42	10	-25.96	0.0	-7.24e-04	-4.01	0.0	-142.01	1.49	0.0	0.0	0.0	-25.98
		-26.03	0.0	0.0	0.0	10.0	-144.73	-2.52	0.0	0.0	0.0	-26.03
42	12	-3.16	0.0	-1.06e-04	-4.01	0.0	-97.94	-7.15	0.0	0.0	0.0	-3.16
		-4.08	0.0	0.0	0.0	10.0	-100.66	-11.17	0.0	0.0	0.0	-4.08
42	13	1.54	0.0	1.14e-05	-4.01	0.0	-91.43	-5.37	0.0	0.0	0.0	1.54
		0.80	0.0	0.0	0.0	10.0	-94.15	-9.38	0.0	0.0	0.0	0.80
42	14	9.44	0.0	1.02e-04	-10.42	0.0	-164.24	-63.50	0.0	0.0	0.0	9.44
		2.54	0.0	0.0	0.0	10.0	-171.30	-73.92	0.0	0.0	0.0	2.54
42	17	-18.85	0.0	-5.34e-04	-4.01	0.0	-128.89	-0.29	0.0	0.0	0.0	-18.85
		-19.08	0.0	0.0	0.0	10.0	-131.62	-4.30	0.0	0.0	0.0	-19.08
42	18	1.54	0.0	1.14e-05	-4.01	0.0	-91.43	-5.37	0.0	0.0	0.0	1.54
		0.80	0.0	0.0	0.0	10.0	-94.15	-9.38	0.0	0.0	0.0	0.80
42	19	7.47	0.0	7.90e-05	-8.81	0.0	-146.04	-48.97	0.0	0.0	0.0	7.47
		2.11	0.0	0.0	0.0	10.0	-152.01	-57.78	0.0	0.0	0.0	2.11
42	20	-13.75	0.0	-3.97e-04	-4.01	0.0	-119.53	-1.56	0.0	0.0	0.0	-13.75
		-14.11	0.0	0.0	0.0	10.0	-122.25	-5.57	0.0	0.0	0.0	-14.11
42	21	1.54	0.0	1.14e-05	-4.01	0.0	-91.43	-5.37	0.0	0.0	0.0	1.54
		0.80	0.0	0.0	0.0	10.0	-94.15	-9.38	0.0	0.0	0.0	0.80
43	2	0.80	0.0	1.16e-05	-3.87	0.0	-94.50	-4.70	0.0	0.0	0.0	0.80
		0.13	0.0	0.0	0.0	10.0	-97.42	-8.57	0.0	0.0	0.0	0.13
43	3	3.43	0.0	1.38e-04	-13.57	0.0	-235.92	-88.19	0.0	0.0	0.0	3.43
		-6.11	0.0	0.0	0.0	10.0	-246.14	-101.76	0.0	0.0	0.0	-6.11
43	9	-25.67	0.0	-7.26e-04	-5.23	0.0	-177.75	3.02	0.0	0.0	0.0	-25.75
		-25.75	0.0	0.0	0.0	10.0	-181.69	-2.21	0.0	0.0	0.0	-25.71
43	10	-25.76	0.0	-7.31e-04	-3.87	0.0	-144.67	4.66	0.0	0.0	0.0	-26.03
		-26.03	0.0	0.0	0.0	10.0	-147.59	0.79	0.0	0.0	0.0	-25.76
43	12	-4.08	0.0	-1.07e-04	-3.87	0.0	-101.37	-5.95	0.0	0.0	0.0	-4.08
		-4.88	0.0	0.0	0.0	10.0	-104.28	-9.82	0.0	0.0	0.0	-4.88
43	13	0.80	0.0	1.16e-05	-3.87	0.0	-94.50	-4.70	0.0	0.0	0.0	0.80
		0.13	0.0	0.0	0.0	10.0	-97.42	-8.57	0.0	0.0	0.0	0.13
43	14	2.54	0.0	1.02e-04	-10.05	0.0	-174.75	-65.32	0.0	0.0	0.0	2.54
		-4.53	0.0	0.0	0.0	10.0	-182.32	-75.38	0.0	0.0	0.0	-4.53
43	17	-19.01	0.0	-5.38e-04	-3.87	0.0	-131.67	2.24	0.0	0.0	0.0	-19.08
		-19.08	0.0	0.0	0.0	10.0	-134.58	-1.64	0.0	0.0	0.0	-19.05
43	18	0.80	0.0	1.16e-05	-3.87	0.0	-94.50	-4.70	0.0	0.0	0.0	0.80
		0.13	0.0	0.0	0.0	10.0	-97.42	-8.57	0.0	0.0	0.0	0.13
43	19	2.11	0.0	7.95e-05	-8.51	0.0	-154.69	-50.17	0.0	0.0	0.0	2.11
		-3.36	0.0	0.0	0.0	10.0	-161.10	-58.68	0.0	0.0	0.0	-3.36
43	20	-14.10	0.0	-4.01e-04	-3.87	0.0	-122.38	0.50	0.0	0.0	0.0	-14.11
		-14.25	0.0	0.0	0.0	10.0	-125.29	-3.37	0.0	0.0	0.0	-14.25
43	21	0.80	0.0	1.16e-05	-3.87	0.0	-94.50	-4.70	0.0	0.0	0.0	0.80
		0.13	0.0	0.0	0.0	10.0	-97.42	-8.57	0.0	0.0	0.0	0.13
44	2	0.13	0.0	1.16e-05	-3.72	0.0	-97.72	-3.73	0.0	0.0	0.0	0.13
		-0.43	0.0	0.0	0.0	10.0	-100.83	-7.45	0.0	0.0	0.0	-0.43
44	3	-6.11	0.0	1.37e-04	-13.05	0.0	-250.89	-89.42	0.0	0.0	0.0	-6.11
		-15.75	0.0	0.0	0.0	10.0	-261.77	-102.46	0.0	0.0	0.0	-15.75
44	4	-6.16	0.0	1.33e-04	-11.74	0.0	-216.68	-88.11	0.0	0.0	0.0	-6.16
		-15.60	0.0	0.0	0.0	10.0	-226.48	-99.86	0.0	0.0	0.0	-15.60
44	9	-25.28	0.0	-7.33e-04	-5.03	0.0	-181.57	6.81	0.0	0.0	0.0	-25.71
		-25.71	0.0	0.0	0.0	10.0	-185.76	1.79	0.0	0.0	0.0	-25.28
44	10	-25.13	0.0	-7.37e-04	-3.72	0.0	-147.37	8.12	0.0	0.0	0.0	-25.76
		-25.76	0.0	0.0	0.0	10.0	-150.47	4.39	0.0	0.0	0.0	-25.13
44	11	0.57	0.0	1.78e-05	-5.03	0.0	-129.13	-7.37	0.0	0.0	0.0	0.57
		-0.42	0.0	0.0	0.0	10.0	-133.32	-12.39	0.0	0.0	0.0	-0.42
44	12	-4.88	0.0	-1.08e-04	-3.72	0.0	-104.90	-4.42	0.0	0.0	0.0	-4.88
		-5.51	0.0	0.0	0.0	10.0	-108.01	-8.14	0.0	0.0	0.0	-5.51
44	13	0.13	0.0	1.16e-05	-3.72	0.0	-97.72	-3.73	0.0	0.0	0.0	0.13
		-0.43	0.0	0.0	0.0	10.0	-100.83	-7.45	0.0	0.0	0.0	-0.43
44	14	-4.53	0.0	1.01e-04	-9.66	0.0	-185.84	-66.23	0.0	0.0	0.0	-4.53
		-11.67	0.0	0.0	0.0	10.0	-193.90	-75.90	0.0	0.0	0.0	-11.67
44	17	-18.73	0.0	-5.43e-04	-3.72	0.0	-134.50	5.05	0.0	0.0	0.0	-19.05
		-19.05	0.0	0.0	0.0	10.0	-137.60	1.32	0.0	0.0	0.0	-18.73
44	18	0.13	0.0	1.16e-05	-3.72	0.0	-97.72	-3.73	0.0	0.0	0.0	0.13
		-0.43	0.0	0.0	0.0	10.0	-100.83	-7.45	0.0	0.0	0.0	-0.43
44	19	-3.36	0.0	7.88e-05	-8.18	0.0	-163.81	-50.61	0.0	0.0	0.0	-3.36

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
44	20	-8.86	0.0	0.0	0.0	10.0	-170.63	-58.79	0.0	0.0	0.0	-8.86
		-14.14	0.0	-4.04e-04	-3.72	0.0	-125.30	2.85	0.0	0.0	0.0	-14.25
		-14.25	0.0	0.0	0.0	10.0	-128.41	-0.87	0.0	0.0	0.0	-14.15
44	21	0.13	0.0	1.16e-05	-3.72	0.0	-97.72	-3.73	0.0	0.0	0.0	0.13
		-0.43	0.0	0.0	0.0	10.0	-100.83	-7.45	0.0	0.0	0.0	-0.43
45	2	-0.43	0.0	1.14e-05	-4.05	0.0	-101.07	-2.44	0.0	0.0	0.0	-0.43
		-0.87	0.0	0.0	0.0	10.0	-97.61	-6.48	0.0	0.0	0.0	-0.87
45	3	-15.75	0.0	1.33e-04	-5.46	0.0	-266.53	-89.35	0.0	0.0	0.0	-15.75
		-25.00	0.0	0.0	0.0	10.0	-261.85	-94.81	0.0	0.0	0.0	-25.00
45	9	-24.45	0.0	-7.38e-04	-5.46	0.0	-185.45	11.00	0.0	0.0	0.0	-25.28
		-25.28	0.0	0.0	0.0	10.0	-180.77	5.54	0.0	0.0	0.0	-24.45
45	11	-0.42	0.0	1.77e-05	-5.46	0.0	-133.77	-5.76	0.0	0.0	0.0	-0.42
		-1.28	0.0	0.0	0.0	10.0	-129.09	-11.23	0.0	0.0	0.0	-1.28
45	12	-5.51	0.0	-1.09e-04	-4.05	0.0	-108.52	-2.54	0.0	0.0	0.0	-5.51
		-5.97	0.0	0.0	0.0	10.0	-105.06	-6.59	0.0	0.0	0.0	-5.97
45	13	-0.43	0.0	1.14e-05	-4.05	0.0	-101.07	-2.44	0.0	0.0	0.0	-0.43
		-0.87	0.0	0.0	0.0	10.0	-97.61	-6.48	0.0	0.0	0.0	-0.87
45	14	-11.67	0.0	9.84e-05	-4.05	0.0	-197.43	-66.18	0.0	0.0	0.0	-11.67
		-18.52	0.0	0.0	0.0	10.0	-193.96	-70.23	0.0	0.0	0.0	-18.52
45	17	-18.11	0.0	-5.47e-04	-4.05	0.0	-137.37	8.15	0.0	0.0	0.0	-18.73
		-18.73	0.0	0.0	0.0	10.0	-133.90	4.10	0.0	0.0	0.0	-18.11
45	18	-0.43	0.0	1.14e-05	-4.05	0.0	-101.07	-2.44	0.0	0.0	0.0	-0.43
		-0.87	0.0	0.0	0.0	10.0	-97.61	-6.48	0.0	0.0	0.0	-0.87
45	19	-8.86	0.0	7.67e-05	-4.05	0.0	-173.34	-50.25	0.0	0.0	0.0	-8.86
		-14.11	0.0	0.0	0.0	10.0	-169.88	-54.29	0.0	0.0	0.0	-14.11
45	20	-13.80	0.0	-4.07e-04	-4.05	0.0	-128.29	5.50	0.0	0.0	0.0	-14.15
		-14.15	0.0	0.0	0.0	10.0	-124.83	1.46	0.0	0.0	0.0	-13.80
45	21	-0.43	0.0	1.14e-05	-4.05	0.0	-101.07	-2.44	0.0	0.0	0.0	-0.43
		-0.87	0.0	0.0	0.0	10.0	-97.61	-6.48	0.0	0.0	0.0	-0.87
46	2	-0.87	0.0	1.12e-05	-4.31	0.0	-97.81	-1.63	0.0	0.0	0.0	-0.87
		-1.25	0.0	0.0	0.0	10.0	-94.46	-5.94	0.0	0.0	0.0	-1.25
46	3	-25.00	0.0	1.27e-04	-5.82	0.0	-266.23	-81.70	0.0	0.0	0.0	-25.00
		-33.50	0.0	0.0	0.0	10.0	-261.71	-87.52	0.0	0.0	0.0	-33.50
46	9	-23.28	0.0	-7.44e-04	-5.82	0.0	-180.27	14.50	0.0	0.0	0.0	-24.45
		-24.45	0.0	0.0	0.0	10.0	-175.74	8.68	0.0	0.0	0.0	-23.28
46	12	-5.97	0.0	-1.10e-04	-4.31	0.0	-105.49	-1.13	0.0	0.0	0.0	-5.97
		-6.30	0.0	0.0	0.0	10.0	-102.13	-5.45	0.0	0.0	0.0	-6.30
46	13	-0.87	0.0	1.12e-05	-4.31	0.0	-97.81	-1.63	0.0	0.0	0.0	-0.87
		-1.25	0.0	0.0	0.0	10.0	-94.46	-5.94	0.0	0.0	0.0	-1.25
46	14	-18.52	0.0	9.40e-05	-4.31	0.0	-197.21	-60.52	0.0	0.0	0.0	-18.52
		-24.81	0.0	0.0	0.0	10.0	-193.86	-64.83	0.0	0.0	0.0	-24.81
46	17	-17.25	0.0	-5.51e-04	-4.31	0.0	-133.53	10.74	0.0	0.0	0.0	-18.11
		-18.11	0.0	0.0	0.0	10.0	-130.18	6.43	0.0	0.0	0.0	-17.25
46	18	-0.87	0.0	1.12e-05	-4.31	0.0	-97.81	-1.63	0.0	0.0	0.0	-0.87
		-1.25	0.0	0.0	0.0	10.0	-94.46	-5.94	0.0	0.0	0.0	-1.25
46	19	-14.11	0.0	7.33e-05	-4.31	0.0	-172.36	-45.79	0.0	0.0	0.0	-14.11
		-18.92	0.0	0.0	0.0	10.0	-169.01	-50.11	0.0	0.0	0.0	-18.92
46	20	-13.25	0.0	-4.11e-04	-4.31	0.0	-124.60	7.65	0.0	0.0	0.0	-13.80
		-13.80	0.0	0.0	0.0	10.0	-121.25	3.34	0.0	0.0	0.0	-13.25
46	21	-0.87	0.0	1.12e-05	-4.31	0.0	-97.81	-1.63	0.0	0.0	0.0	-0.87
		-1.25	0.0	0.0	0.0	10.0	-94.46	-5.94	0.0	0.0	0.0	-1.25
47	2	-1.25	0.0	1.09e-05	-4.58	0.0	-94.64	-1.25	0.0	0.0	0.0	-1.25
		-1.61	0.0	0.0	0.0	10.0	-91.40	-5.83	0.0	0.0	0.0	-1.61
47	3	-33.50	0.0	1.19e-04	-6.18	0.0	-265.73	-74.42	0.0	0.0	0.0	-33.50
		-41.28	0.0	0.0	0.0	10.0	-261.37	-80.60	0.0	0.0	0.0	-41.28
47	10	-21.28	0.0	-7.53e-04	-4.58	0.0	-141.97	17.83	0.0	0.0	0.0	-22.85
		-22.85	0.0	0.0	0.0	10.0	-138.74	13.25	0.0	0.0	0.0	-21.28
47	12	-6.30	0.0	-1.12e-04	-4.58	0.0	-102.49	-0.13	0.0	0.0	0.0	-6.30
		-6.54	0.0	0.0	0.0	10.0	-99.26	-4.71	0.0	0.0	0.0	-6.54
47	13	-1.25	0.0	1.09e-05	-4.58	0.0	-94.64	-1.25	0.0	0.0	0.0	-1.25
		-1.61	0.0	0.0	0.0	10.0	-91.40	-5.83	0.0	0.0	0.0	-1.61
47	14	-24.81	0.0	8.81e-05	-4.58	0.0	-196.83	-55.13	0.0	0.0	0.0	-24.81
		-30.58	0.0	0.0	0.0	10.0	-193.60	-59.71	0.0	0.0	0.0	-30.58
47	17	-16.18	0.0	-5.55e-04	-4.58	0.0	-129.70	12.88	0.0	0.0	0.0	-17.25
		-17.25	0.0	0.0	0.0	10.0	-126.47	8.31	0.0	0.0	0.0	-16.18
47	18	-1.25	0.0	1.09e-05	-4.58	0.0	-94.64	-1.25	0.0	0.0	0.0	-1.25
		-1.61	0.0	0.0	0.0	10.0	-91.40	-5.83	0.0	0.0	0.0	-1.61
47	19	-18.92	0.0	6.88e-05	-4.58	0.0	-171.29	-41.66	0.0	0.0	0.0	-18.92
		-23.34	0.0	0.0	0.0	10.0	-168.05	-46.24	0.0	0.0	0.0	-23.34
47	20	-12.54	0.0	-4.14e-04	-4.58	0.0	-120.93	9.35	0.0	0.0	0.0	-13.25
		-13.25	0.0	0.0	0.0	10.0	-117.70	4.77	0.0	0.0	0.0	-12.54
47	21	-1.25	0.0	1.09e-05	-4.58	0.0	-94.64	-1.25	0.0	0.0	0.0	-1.25
		-1.61	0.0	0.0	0.0	10.0	-91.40	-5.83	0.0	0.0	0.0	-1.61



Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
48	2	-1.61	0.0	1.06e-05	-4.85	0.0	-91.58	-1.28	0.0	0.0	0.0	-1.61
		-1.98	0.0	0.0	0.0	10.0	-88.49	-6.13	0.0	0.0	0.0	-1.98
48	3	-41.28	0.0	1.09e-04	-6.55	0.0	-265.04	-67.53	0.0	0.0	0.0	-41.28
		-48.40	0.0	0.0	0.0	10.0	-260.87	-74.08	0.0	0.0	0.0	-48.40
48	10	-19.50	0.0	-7.58e-04	-4.85	0.0	-137.91	20.12	0.0	0.0	0.0	-21.28
		-21.28	0.0	0.0	0.0	10.0	-134.82	15.27	0.0	0.0	0.0	-19.50
48	12	-6.54	0.0	-1.13e-04	-4.85	0.0	-99.57	0.47	0.0	0.0	0.0	-6.54
		-6.73	0.0	0.0	0.0	10.0	-96.48	-4.38	0.0	0.0	0.0	-6.73
48	13	-1.61	0.0	1.06e-05	-4.85	0.0	-91.58	-1.28	0.0	0.0	0.0	-1.61
		-1.98	0.0	0.0	0.0	10.0	-88.49	-6.13	0.0	0.0	0.0	-1.98
48	14	-30.58	0.0	8.09e-05	-4.85	0.0	-196.33	-50.02	0.0	0.0	0.0	-30.58
		-35.85	0.0	0.0	0.0	10.0	-193.24	-54.87	0.0	0.0	0.0	-35.85
48	17	-14.96	0.0	-5.59e-04	-4.85	0.0	-125.90	14.57	0.0	0.0	0.0	-16.18
		-16.18	0.0	0.0	0.0	10.0	-122.81	9.72	0.0	0.0	0.0	-14.96
48	18	-1.61	0.0	1.06e-05	-4.85	0.0	-91.58	-1.28	0.0	0.0	0.0	-1.61
		-1.98	0.0	0.0	0.0	10.0	-88.49	-6.13	0.0	0.0	0.0	-1.98
48	19	-23.34	0.0	6.33e-05	-4.85	0.0	-170.14	-37.84	0.0	0.0	0.0	-23.34
		-27.38	0.0	0.0	0.0	10.0	-167.05	-42.69	0.0	0.0	0.0	-27.38
48	20	-11.72	0.0	-4.17e-04	-4.85	0.0	-117.32	10.61	0.0	0.0	0.0	-12.54
		-12.54	0.0	0.0	0.0	10.0	-114.23	5.76	0.0	0.0	0.0	-11.72
48	21	-1.61	0.0	1.06e-05	-4.85	0.0	-91.58	-1.28	0.0	0.0	0.0	-1.61
		-1.98	0.0	0.0	0.0	10.0	-88.49	-6.13	0.0	0.0	0.0	-1.98
49	1	-2.67	0.0	1.37e-05	-6.91	0.0	-119.72	-2.34	0.0	0.0	0.0	-2.67
		-3.25	0.0	0.0	0.0	10.0	-115.76	-9.25	0.0	0.0	0.0	-3.25
49	2	-1.98	0.0	1.01e-05	-5.12	0.0	-88.68	-1.73	0.0	0.0	0.0	-1.98
		-2.41	0.0	0.0	0.0	10.0	-85.74	-6.85	0.0	0.0	0.0	-2.41
49	3	-48.40	0.0	9.79e-05	-6.91	0.0	-264.22	-61.04	0.0	0.0	0.0	-48.40
		-54.88	0.0	0.0	0.0	10.0	-260.26	-67.95	0.0	0.0	0.0	-54.88
49	10	-17.56	0.0	-7.63e-04	-5.12	0.0	-133.90	21.95	0.0	0.0	0.0	-19.50
		-19.50	0.0	0.0	0.0	10.0	-130.96	16.82	0.0	0.0	0.0	-17.56
49	12	-6.73	0.0	-1.15e-04	-5.12	0.0	-96.76	0.67	0.0	0.0	0.0	-6.73
		-6.92	0.0	0.0	0.0	10.0	-93.82	-4.46	0.0	0.0	0.0	-6.92
49	13	-1.98	0.0	1.01e-05	-5.12	0.0	-88.68	-1.73	0.0	0.0	0.0	-1.98
		-2.41	0.0	0.0	0.0	10.0	-85.74	-6.85	0.0	0.0	0.0	-2.41
49	14	-35.85	0.0	7.25e-05	-5.12	0.0	-195.72	-45.21	0.0	0.0	0.0	-35.85
		-40.65	0.0	0.0	0.0	10.0	-192.78	-50.34	0.0	0.0	0.0	-40.65
49	17	-13.63	0.0	-5.63e-04	-5.12	0.0	-122.18	15.81	0.0	0.0	0.0	-14.96
		-14.96	0.0	0.0	0.0	10.0	-119.24	10.68	0.0	0.0	0.0	-13.63
49	18	-1.98	0.0	1.01e-05	-5.12	0.0	-88.68	-1.73	0.0	0.0	0.0	-1.98
		-2.41	0.0	0.0	0.0	10.0	-85.74	-6.85	0.0	0.0	0.0	-2.41
49	19	-27.38	0.0	5.69e-05	-5.12	0.0	-168.96	-34.34	0.0	0.0	0.0	-27.38
		-31.09	0.0	0.0	0.0	10.0	-166.02	-39.46	0.0	0.0	0.0	-31.09
49	20	-10.82	0.0	-4.19e-04	-5.12	0.0	-113.80	11.42	0.0	0.0	0.0	-11.72
		-11.72	0.0	0.0	0.0	10.0	-110.86	6.30	0.0	0.0	0.0	-10.82
49	21	-1.98	0.0	1.01e-05	-5.12	0.0	-88.68	-1.73	0.0	0.0	0.0	-1.98
		-2.41	0.0	0.0	0.0	10.0	-85.74	-6.85	0.0	0.0	0.0	-2.41
50	2	-2.41	0.0	9.63e-06	-5.40	0.0	-85.98	-2.59	0.0	0.0	0.0	-2.41
		-2.94	0.0	0.0	0.0	10.0	-83.21	-7.99	0.0	0.0	0.0	-2.94
50	3	-54.88	0.0	8.51e-05	-7.28	0.0	-263.31	-54.95	0.0	0.0	0.0	-54.88
		-60.76	0.0	0.0	0.0	10.0	-259.57	-62.24	0.0	0.0	0.0	-60.76
50	10	-15.48	0.0	-7.67e-04	-5.40	0.0	-129.96	23.30	0.0	0.0	0.0	-17.56
		-17.56	0.0	0.0	0.0	10.0	-127.19	17.90	0.0	0.0	0.0	-15.48
50	12	-6.92	0.0	-1.17e-04	-5.40	0.0	-94.09	0.46	0.0	0.0	0.0	-6.92
		-7.15	0.0	0.0	0.0	10.0	-91.32	-4.94	0.0	0.0	0.0	-7.15
50	13	-2.41	0.0	9.63e-06	-5.40	0.0	-85.98	-2.59	0.0	0.0	0.0	-2.41
		-2.94	0.0	0.0	0.0	10.0	-83.21	-7.99	0.0	0.0	0.0	-2.94
50	14	-40.65	0.0	6.30e-05	-5.40	0.0	-195.04	-40.71	0.0	0.0	0.0	-40.65
		-45.01	0.0	0.0	0.0	10.0	-192.27	-46.10	0.0	0.0	0.0	-45.01
50	17	-12.23	0.0	-5.66e-04	-5.40	0.0	-118.56	16.59	0.0	0.0	0.0	-13.63
		-13.63	0.0	0.0	0.0	10.0	-115.79	11.19	0.0	0.0	0.0	-12.23
50	18	-2.41	0.0	9.63e-06	-5.40	0.0	-85.98	-2.59	0.0	0.0	0.0	-2.41
		-2.94	0.0	0.0	0.0	10.0	-83.21	-7.99	0.0	0.0	0.0	-2.94
50	19	-31.09	0.0	4.97e-05	-5.40	0.0	-167.78	-31.18	0.0	0.0	0.0	-31.09
		-34.49	0.0	0.0	0.0	10.0	-165.01	-36.57	0.0	0.0	0.0	-34.49
50	20	-9.91	0.0	-4.22e-04	-5.40	0.0	-110.41	11.79	0.0	0.0	0.0	-10.82
		-10.82	0.0	0.0	0.0	10.0	-107.65	6.40	0.0	0.0	0.0	-9.91
50	21	-2.41	0.0	9.63e-06	-5.40	0.0	-85.98	-2.59	0.0	0.0	0.0	-2.41
		-2.94	0.0	0.0	0.0	10.0	-83.21	-7.99	0.0	0.0	0.0	-2.94
51	2	-2.94	0.0	9.01e-06	-5.67	0.0	-83.50	-3.85	0.0	0.0	0.0	-2.94
		-3.61	0.0	0.0	0.0	10.0	-80.92	-9.52	0.0	0.0	0.0	-3.61
51	3	-60.76	0.0	7.09e-05	-7.65	0.0	-262.34	-49.28	0.0	0.0	0.0	-60.76
		-66.10	0.0	0.0	0.0	10.0	-258.86	-56.93	0.0	0.0	0.0	-66.10
51	10	-13.34	0.0	-7.71e-04	-5.67	0.0	-126.15	24.20	0.0	0.0	0.0	-15.48

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
51	12	-15.48	0.0	0.0	0.0	10.0	-123.57	18.53	0.0	0.0	0.0	-13.34
		-7.15	0.0	-1.18e-04	-5.67	0.0	-91.60	-0.14	0.0	0.0	0.0	-7.15
		-7.44	0.0	0.0	0.0	10.0	-89.02	-5.81	0.0	0.0	0.0	-7.44
51	13	-2.94	0.0	9.01e-06	-5.67	0.0	-83.50	-3.85	0.0	0.0	0.0	-2.94
		-3.61	0.0	0.0	0.0	10.0	-80.92	-9.52	0.0	0.0	0.0	-3.61
51	14	-45.01	0.0	5.25e-05	-5.67	0.0	-194.33	-36.50	0.0	0.0	0.0	-45.01
		-48.96	0.0	0.0	0.0	10.0	-191.74	-42.17	0.0	0.0	0.0	-48.96
51	17	-10.82	0.0	-5.68e-04	-5.67	0.0	-115.09	16.93	0.0	0.0	0.0	-12.23
		-12.23	0.0	0.0	0.0	10.0	-112.51	11.26	0.0	0.0	0.0	-10.82
51	18	-2.94	0.0	9.01e-06	-5.67	0.0	-83.50	-3.85	0.0	0.0	0.0	-2.94
		-3.61	0.0	0.0	0.0	10.0	-80.92	-9.52	0.0	0.0	0.0	-3.61
51	19	-34.49	0.0	4.16e-05	-5.67	0.0	-166.62	-28.34	0.0	0.0	0.0	-34.49
		-37.62	0.0	0.0	0.0	10.0	-164.04	-34.01	0.0	0.0	0.0	-37.62
51	20	-9.01	0.0	-4.24e-04	-5.67	0.0	-107.20	11.73	0.0	0.0	0.0	-9.91
		-9.91	0.0	0.0	0.0	10.0	-104.61	6.06	0.0	0.0	0.0	-9.01
51	21	-2.94	0.0	9.01e-06	-5.67	0.0	-83.50	-3.85	0.0	0.0	0.0	-2.94
		-3.61	0.0	0.0	0.0	10.0	-80.92	-9.52	0.0	0.0	0.0	-3.61
52	2	-3.61	0.0	8.24e-06	-5.94	0.0	-81.30	-5.49	0.0	0.0	0.0	-3.61
		-4.46	0.0	0.0	0.0	10.0	-78.92	-11.43	0.0	0.0	0.0	-4.46
52	3	-66.10	0.0	5.55e-05	-8.02	0.0	-261.36	-44.02	0.0	0.0	0.0	-66.10
		-70.92	0.0	0.0	0.0	10.0	-258.15	-52.04	0.0	0.0	0.0	-70.92
52	10	-11.16	0.0	-7.74e-04	-5.94	0.0	-122.50	24.63	0.0	0.0	0.0	-13.34
		-13.34	0.0	0.0	0.0	10.0	-120.12	18.69	0.0	0.0	0.0	-11.16
52	12	-7.44	0.0	-1.20e-04	-5.94	0.0	-89.33	-1.13	0.0	0.0	0.0	-7.44
		-7.86	0.0	0.0	0.0	10.0	-86.96	-7.07	0.0	0.0	0.0	-7.86
52	13	-3.61	0.0	8.24e-06	-5.94	0.0	-81.30	-5.49	0.0	0.0	0.0	-3.61
		-4.46	0.0	0.0	0.0	10.0	-78.92	-11.43	0.0	0.0	0.0	-4.46
52	14	-48.96	0.0	4.11e-05	-5.94	0.0	-193.60	-32.61	0.0	0.0	0.0	-48.96
		-52.53	0.0	0.0	0.0	10.0	-191.23	-38.55	0.0	0.0	0.0	-52.53
52	17	-9.42	0.0	-5.71e-04	-5.94	0.0	-111.81	16.82	0.0	0.0	0.0	-10.82
		-10.82	0.0	0.0	0.0	10.0	-109.44	10.88	0.0	0.0	0.0	-9.42
52	18	-3.61	0.0	8.24e-06	-5.94	0.0	-81.30	-5.49	0.0	0.0	0.0	-3.61
		-4.46	0.0	0.0	0.0	10.0	-78.92	-11.43	0.0	0.0	0.0	-4.46
52	19	-37.62	0.0	3.29e-05	-5.94	0.0	-165.52	-25.83	0.0	0.0	0.0	-37.62
		-40.51	0.0	0.0	0.0	10.0	-163.15	-31.77	0.0	0.0	0.0	-40.51
52	20	-8.18	0.0	-4.26e-04	-5.94	0.0	-104.18	11.25	0.0	0.0	0.0	-9.01
		-9.01	0.0	0.0	0.0	10.0	-101.81	5.30	0.0	0.0	0.0	-8.18
52	21	-3.61	0.0	8.24e-06	-5.94	0.0	-81.30	-5.49	0.0	0.0	0.0	-3.61
		-4.46	0.0	0.0	0.0	10.0	-78.92	-11.43	0.0	0.0	0.0	-4.46
53	2	-4.46	0.0	7.29e-06	-6.21	0.0	-79.39	-7.50	0.0	0.0	0.0	-4.46
		-5.52	0.0	0.0	0.0	10.0	-77.24	-13.71	0.0	0.0	0.0	-5.52
53	3	-70.92	0.0	3.90e-05	-8.39	0.0	-260.42	-39.16	0.0	0.0	0.0	-70.92
		-75.27	0.0	0.0	0.0	10.0	-257.52	-47.55	0.0	0.0	0.0	-75.27
53	10	-9.00	0.0	-7.76e-04	-6.21	0.0	-119.04	24.63	0.0	0.0	0.0	-11.16
		-11.16	0.0	0.0	0.0	10.0	-116.89	18.42	0.0	0.0	0.0	-9.00
53	12	-7.86	0.0	-1.22e-04	-6.21	0.0	-87.32	-2.49	0.0	0.0	0.0	-7.86
		-8.42	0.0	0.0	0.0	10.0	-85.17	-8.71	0.0	0.0	0.0	-8.42
53	13	-4.46	0.0	7.29e-06	-6.21	0.0	-79.39	-7.50	0.0	0.0	0.0	-4.46
		-5.52	0.0	0.0	0.0	10.0	-77.24	-13.71	0.0	0.0	0.0	-5.52
53	14	-52.53	0.0	2.89e-05	-6.21	0.0	-192.90	-29.01	0.0	0.0	0.0	-52.53
		-55.76	0.0	0.0	0.0	10.0	-190.75	-35.22	0.0	0.0	0.0	-55.76
53	17	-8.10	0.0	-5.73e-04	-6.21	0.0	-108.76	16.30	0.0	0.0	0.0	-9.42
		-9.42	0.0	0.0	0.0	10.0	-106.61	10.09	0.0	0.0	0.0	-8.10
53	18	-4.46	0.0	7.29e-06	-6.21	0.0	-79.39	-7.50	0.0	0.0	0.0	-4.46
		-5.52	0.0	0.0	0.0	10.0	-77.24	-13.71	0.0	0.0	0.0	-5.52
53	19	-40.51	0.0	2.35e-05	-6.21	0.0	-164.53	-23.63	0.0	0.0	0.0	-40.51
		-43.20	0.0	0.0	0.0	10.0	-162.38	-29.85	0.0	0.0	0.0	-43.20
53	20	-7.45	0.0	-4.28e-04	-6.21	0.0	-101.42	10.35	0.0	0.0	0.0	-8.18
		-8.18	0.0	0.0	0.0	10.0	-99.27	4.14	0.0	0.0	0.0	-7.45
53	21	-4.46	0.0	7.29e-06	-6.21	0.0	-79.39	-7.50	0.0	0.0	0.0	-4.46
		-5.52	0.0	0.0	0.0	10.0	-77.24	-13.71	0.0	0.0	0.0	-5.52
54	1	-7.46	0.0	8.24e-06	-8.75	0.0	-105.07	-13.31	0.0	0.0	0.0	-7.46
		-9.23	0.0	0.0	0.0	10.0	-102.49	-22.06	0.0	0.0	0.0	-9.23
54	2	-5.52	0.0	6.10e-06	-6.48	0.0	-77.83	-9.86	0.0	0.0	0.0	-5.52
		-6.84	0.0	0.0	0.0	10.0	-75.92	-16.34	0.0	0.0	0.0	-6.84
54	3	-75.27	0.0	2.15e-05	-8.75	0.0	-259.56	-34.71	0.0	0.0	0.0	-75.27
		-79.20	0.0	0.0	0.0	10.0	-256.99	-43.45	0.0	0.0	0.0	-79.20
54	10	-6.89	0.0	-7.78e-04	-6.48	0.0	-115.84	24.20	0.0	0.0	0.0	-9.00
		-9.00	0.0	0.0	0.0	10.0	-113.93	17.72	0.0	0.0	0.0	-6.89
54	12	-8.42	0.0	-1.23e-04	-6.48	0.0	-85.60	-4.21	0.0	0.0	0.0	-8.42
		-9.16	0.0	0.0	0.0	10.0	-83.69	-10.69	0.0	0.0	0.0	-9.16
54	13	-5.52	0.0	6.10e-06	-6.48	0.0	-77.83	-9.86	0.0	0.0	0.0	-5.52
		-6.84	0.0	0.0	0.0	10.0	-75.92	-16.34	0.0	0.0	0.0	-6.84

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
54	14	-55.76	0.0	1.60e-05	-6.48	0.0	-192.27	-25.71	0.0	0.0	0.0	-55.76
		-58.67	0.0	0.0	0.0	10.0	-190.36	-32.19	0.0	0.0	0.0	-58.67
54	17	-6.88	0.0	-5.75e-04	-6.48	0.0	-105.98	15.37	0.0	0.0	0.0	-8.10
		-8.10	0.0	0.0	0.0	10.0	-104.08	8.89	0.0	0.0	0.0	-6.88
54	18	-5.52	0.0	6.10e-06	-6.48	0.0	-77.83	-9.86	0.0	0.0	0.0	-5.52
		-6.84	0.0	0.0	0.0	10.0	-75.92	-16.34	0.0	0.0	0.0	-6.84
54	19	-43.20	0.0	1.35e-05	-6.48	0.0	-163.66	-21.75	0.0	0.0	0.0	-43.20
		-45.71	0.0	0.0	0.0	10.0	-161.75	-28.23	0.0	0.0	0.0	-45.71
54	20	-6.87	0.0	-4.30e-04	-6.48	0.0	-98.94	9.06	0.0	0.0	0.0	-7.45
		-7.45	0.0	0.0	0.0	10.0	-97.04	2.58	0.0	0.0	0.0	-6.87
54	21	-5.52	0.0	6.10e-06	-6.48	0.0	-77.83	-9.86	0.0	0.0	0.0	-5.52
		-6.84	0.0	0.0	0.0	10.0	-75.92	-16.34	0.0	0.0	0.0	-6.84
55	2	-6.84	0.0	4.62e-06	-6.74	0.0	-76.64	-12.55	0.0	0.0	0.0	-6.84
		-8.44	0.0	0.0	0.0	10.0	-75.00	-19.29	0.0	0.0	0.0	-8.44
55	3	-79.20	0.0	4.15e-06	-9.10	0.0	-258.83	-30.65	0.0	0.0	0.0	-79.20
		-82.73	0.0	0.0	0.0	10.0	-256.61	-39.75	0.0	0.0	0.0	-82.73
55	10	-4.88	0.0	-7.80e-04	-6.74	0.0	-112.91	23.35	0.0	0.0	0.0	-6.89
		-6.89	0.0	0.0	0.0	10.0	-111.27	16.61	0.0	0.0	0.0	-4.88
55	12	-9.16	0.0	-1.25e-04	-6.74	0.0	-84.21	-6.27	0.0	0.0	0.0	-9.16
		-10.13	0.0	0.0	0.0	10.0	-82.57	-13.01	0.0	0.0	0.0	-10.13
55	13	-6.84	0.0	4.62e-06	-6.74	0.0	-76.64	-12.55	0.0	0.0	0.0	-6.84
		-8.44	0.0	0.0	0.0	10.0	-75.00	-19.29	0.0	0.0	0.0	-8.44
55	14	-58.67	0.0	3.07e-06	-6.74	0.0	-191.72	-22.70	0.0	0.0	0.0	-58.67
		-61.28	0.0	0.0	0.0	10.0	-190.08	-29.44	0.0	0.0	0.0	-61.28
55	17	-5.80	0.0	-5.76e-04	-6.74	0.0	-103.51	14.04	0.0	0.0	0.0	-6.88
		-6.88	0.0	0.0	0.0	10.0	-101.87	7.30	0.0	0.0	0.0	-5.80
55	18	-6.84	0.0	4.62e-06	-6.74	0.0	-76.64	-12.55	0.0	0.0	0.0	-6.84
		-8.44	0.0	0.0	0.0	10.0	-75.00	-19.29	0.0	0.0	0.0	-8.44
55	19	-45.71	0.0	3.18e-06	-6.74	0.0	-162.95	-20.17	0.0	0.0	0.0	-45.71
		-48.07	0.0	0.0	0.0	10.0	-161.31	-26.90	0.0	0.0	0.0	-48.07
55	20	-6.46	0.0	-4.31e-04	-6.74	0.0	-96.79	7.39	0.0	0.0	0.0	-6.87
		-6.87	0.0	0.0	0.0	10.0	-95.15	0.66	0.0	0.0	0.0	-6.46
55	21	-6.84	0.0	4.62e-06	-6.74	0.0	-76.64	-12.55	0.0	0.0	0.0	-6.84
		-8.44	0.0	0.0	0.0	10.0	-75.00	-19.29	0.0	0.0	0.0	-8.44
56	2	-8.44	0.0	2.78e-06	-6.99	0.0	-75.86	-15.55	0.0	0.0	0.0	-8.44
		-10.35	0.0	0.0	0.0	10.0	-74.51	-22.53	0.0	0.0	0.0	-10.35
56	3	-82.73	0.0	-1.60e-05	-9.44	0.0	-258.27	-26.96	0.0	0.0	0.0	-82.73
		-85.91	0.0	0.0	0.0	10.0	-256.44	-36.40	0.0	0.0	0.0	-85.91
56	10	-3.01	0.0	-7.81e-04	-6.99	0.0	-110.31	22.12	0.0	0.0	0.0	-4.88
		-4.88	0.0	0.0	0.0	10.0	-108.95	15.13	0.0	0.0	0.0	-3.01
56	12	-10.13	0.0	-1.28e-04	-6.99	0.0	-83.18	-8.65	0.0	0.0	0.0	-10.13
		-11.35	0.0	0.0	0.0	10.0	-81.83	-15.64	0.0	0.0	0.0	-11.35
56	13	-8.44	0.0	2.78e-06	-6.99	0.0	-75.86	-15.55	0.0	0.0	0.0	-8.44
		-10.35	0.0	0.0	0.0	10.0	-74.51	-22.53	0.0	0.0	0.0	-10.35
56	14	-61.28	0.0	-1.19e-05	-6.99	0.0	-191.31	-19.97	0.0	0.0	0.0	-61.28
		-63.64	0.0	0.0	0.0	10.0	-189.95	-26.96	0.0	0.0	0.0	-63.64
56	17	-4.91	0.0	-5.78e-04	-6.99	0.0	-101.38	12.35	0.0	0.0	0.0	-5.80
		-5.80	0.0	0.0	0.0	10.0	-100.02	5.36	0.0	0.0	0.0	-4.91
56	18	-8.44	0.0	2.78e-06	-6.99	0.0	-75.86	-15.55	0.0	0.0	0.0	-8.44
		-10.35	0.0	0.0	0.0	10.0	-74.51	-22.53	0.0	0.0	0.0	-10.35
56	19	-48.07	0.0	-8.20e-06	-6.99	0.0	-162.45	-18.86	0.0	0.0	0.0	-48.07
		-50.32	0.0	0.0	0.0	10.0	-161.09	-25.85	0.0	0.0	0.0	-50.32
56	20	-6.25	0.0	-4.33e-04	-6.99	0.0	-95.00	5.38	0.0	0.0	0.0	-6.46
		-6.46	0.0	0.0	0.0	10.0	-93.64	-1.61	0.0	0.0	0.0	-6.27
56	21	-8.44	0.0	2.78e-06	-6.99	0.0	-75.86	-15.55	0.0	0.0	0.0	-8.44
		-10.35	0.0	0.0	0.0	10.0	-74.51	-22.53	0.0	0.0	0.0	-10.35
57	1	-13.97	0.0	0.0	-9.76	0.0	-101.97	-25.39	0.0	0.0	0.0	-13.97
		-17.01	0.0	0.0	0.0	10.0	-100.55	-35.15	0.0	0.0	0.0	-17.01
57	2	-10.35	0.0	0.0	-7.23	0.0	-75.53	-18.81	0.0	0.0	0.0	-10.35
		-12.60	0.0	0.0	0.0	10.0	-74.48	-26.04	0.0	0.0	0.0	-12.60
57	3	-85.91	0.0	-3.59e-05	-9.76	0.0	-257.93	-23.62	0.0	0.0	0.0	-85.91
		-88.77	0.0	0.0	0.0	10.0	-256.51	-33.38	0.0	0.0	0.0	-88.77
57	4	-82.29	0.0	-3.61e-05	-7.23	0.0	-231.49	-17.04	0.0	0.0	0.0	-82.29
		-84.36	0.0	0.0	0.0	10.0	-230.44	-24.27	0.0	0.0	0.0	-84.36
57	10	-1.31	0.0	-7.82e-04	-7.23	0.0	-108.07	20.52	0.0	0.0	0.0	-3.01
		-3.01	0.0	0.0	0.0	10.0	-107.02	13.28	0.0	0.0	0.0	-1.31
57	12	-11.35	0.0	-1.30e-04	-7.23	0.0	-82.56	-11.31	0.0	0.0	0.0	-11.35
		-12.85	0.0	0.0	0.0	10.0	-81.51	-18.54	0.0	0.0	0.0	-12.85
57	13	-10.35	0.0	0.0	-7.23	0.0	-75.53	-18.81	0.0	0.0	0.0	-10.35
		-12.60	0.0	0.0	0.0	10.0	-74.48	-26.04	0.0	0.0	0.0	-12.60
57	14	-63.64	0.0	-2.66e-05	-7.23	0.0	-191.06	-17.50	0.0	0.0	0.0	-63.64
		-65.76	0.0	0.0	0.0	10.0	-190.01	-24.73	0.0	0.0	0.0	-65.76
57	17	-4.24	0.0	-5.79e-04	-7.23	0.0	-99.63	10.32	0.0	0.0	0.0	-4.91

Trave	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3	Pos.	N	V 2	V 3	T	M 2	M 3
57	18	-4.91	0.0	0.0	0.0	10.0	-98.58	3.09	0.0	0.0	0.0	-4.24
		-10.35	0.0	0.0	-7.23	0.0	-75.53	-18.81	0.0	0.0	0.0	-10.35
		-12.60	0.0	0.0	0.0	10.0	-74.48	-26.04	0.0	0.0	0.0	-12.60
57	19	-50.32	0.0	-1.98e-05	-7.23	0.0	-162.18	-17.83	0.0	0.0	0.0	-50.32
		-52.47	0.0	0.0	0.0	10.0	-161.13	-25.06	0.0	0.0	0.0	-52.47
57	20	-6.21	0.0	-4.34e-04	-7.23	0.0	-93.61	3.04	0.0	0.0	0.0	-6.27
		-6.33	0.0	0.0	0.0	10.0	-92.56	-4.19	0.0	0.0	0.0	-6.33
57	21	-10.35	0.0	0.0	-7.23	0.0	-75.53	-18.81	0.0	0.0	0.0	-10.35
		-12.60	0.0	0.0	0.0	10.0	-74.48	-26.04	0.0	0.0	0.0	-12.60
58	1	-17.01	0.0	-3.06e-06	-10.07	0.0	-102.17	-30.12	0.0	0.0	0.0	-17.01
		-20.54	0.0	0.0	0.0	10.0	-101.20	-40.19	0.0	0.0	0.0	-20.54
58	2	-12.60	0.0	-2.27e-06	-7.46	0.0	-75.68	-22.31	0.0	0.0	0.0	-12.60
		-15.21	0.0	0.0	0.0	10.0	-74.96	-29.77	0.0	0.0	0.0	-15.21
58	3	-88.77	0.0	-5.65e-05	-10.07	0.0	-257.85	-20.62	0.0	0.0	0.0	-88.77
		-91.35	0.0	0.0	0.0	10.0	-256.87	-30.69	0.0	0.0	0.0	-91.35
58	4	-84.36	0.0	-5.57e-05	-7.46	0.0	-231.36	-12.81	0.0	0.0	0.0	-84.36
		-86.02	0.0	0.0	0.0	10.0	-230.64	-20.27	0.0	0.0	0.0	-86.02
58	10	0.19	0.0	-7.82e-04	-7.46	0.0	-106.23	18.58	0.0	0.0	0.0	-1.31
		-1.31	0.0	0.0	0.0	10.0	-105.50	11.12	0.0	0.0	0.0	0.19
58	12	-12.85	0.0	-1.33e-04	-7.46	0.0	-82.37	-14.24	0.0	0.0	0.0	-12.85
		-14.65	0.0	0.0	0.0	10.0	-81.65	-21.70	0.0	0.0	0.0	-14.65
58	13	-12.60	0.0	-2.27e-06	-7.46	0.0	-75.68	-22.31	0.0	0.0	0.0	-12.60
		-15.21	0.0	0.0	0.0	10.0	-74.96	-29.77	0.0	0.0	0.0	-15.21
58	14	-65.76	0.0	-4.18e-05	-7.46	0.0	-191.00	-15.27	0.0	0.0	0.0	-65.76
		-67.67	0.0	0.0	0.0	10.0	-190.28	-22.73	0.0	0.0	0.0	-67.67
58	17	-3.81	0.0	-5.80e-04	-7.46	0.0	-98.31	7.98	0.0	0.0	0.0	-4.24
		-4.24	0.0	0.0	0.0	10.0	-97.58	0.51	0.0	0.0	0.0	-3.81
58	18	-12.60	0.0	-2.27e-06	-7.46	0.0	-75.68	-22.31	0.0	0.0	0.0	-12.60
		-15.21	0.0	0.0	0.0	10.0	-74.96	-29.77	0.0	0.0	0.0	-15.21
58	19	-52.47	0.0	-3.19e-05	-7.46	0.0	-162.17	-17.03	0.0	0.0	0.0	-52.47
		-54.55	0.0	0.0	0.0	10.0	-161.45	-24.49	0.0	0.0	0.0	-54.55
58	20	-6.33	0.0	-4.35e-04	-7.46	0.0	-92.65	0.40	0.0	0.0	0.0	-6.33
		-6.66	0.0	0.0	0.0	10.0	-91.93	-7.06	0.0	0.0	0.0	-6.66
58	21	-12.60	0.0	-2.27e-06	-7.46	0.0	-75.68	-22.31	0.0	0.0	0.0	-12.60
		-15.21	0.0	0.0	0.0	10.0	-74.96	-29.77	0.0	0.0	0.0	-15.21
59	1	-20.54	0.0	-7.62e-06	-10.37	0.0	-103.07	-35.12	0.0	0.0	0.0	-20.54
		-24.59	0.0	0.0	0.0	10.0	-102.56	-45.49	0.0	0.0	0.0	-24.59
59	2	-15.21	0.0	-5.65e-06	-7.68	0.0	-76.35	-26.02	0.0	0.0	0.0	-15.21
		-18.21	0.0	0.0	0.0	10.0	-75.97	-33.70	0.0	0.0	0.0	-18.21
59	3	-91.35	0.0	-7.76e-05	-10.37	0.0	-258.08	-17.90	0.0	0.0	0.0	-91.35
		-93.67	0.0	0.0	0.0	10.0	-257.57	-28.27	0.0	0.0	0.0	-93.67
59	4	-86.02	0.0	-7.56e-05	-7.68	0.0	-231.36	-8.79	0.0	0.0	0.0	-86.02
		-87.29	0.0	0.0	0.0	10.0	-230.98	-16.47	0.0	0.0	0.0	-87.29
59	10	1.44	0.0	-7.82e-04	-7.68	0.0	-104.82	16.34	0.0	0.0	0.0	0.19
		0.19	0.0	0.0	0.0	10.0	-104.44	8.66	0.0	0.0	0.0	1.44
59	12	-14.65	0.0	-1.36e-04	-7.68	0.0	-82.66	-17.38	0.0	0.0	0.0	-14.65
		-16.78	0.0	0.0	0.0	10.0	-82.28	-25.06	0.0	0.0	0.0	-16.78
59	13	-15.21	0.0	-5.65e-06	-7.68	0.0	-76.35	-26.02	0.0	0.0	0.0	-15.21
		-18.21	0.0	0.0	0.0	10.0	-75.97	-33.70	0.0	0.0	0.0	-18.21
59	14	-67.67	0.0	-5.75e-05	-7.68	0.0	-191.17	-13.26	0.0	0.0	0.0	-67.67
		-69.38	0.0	0.0	0.0	10.0	-190.79	-20.94	0.0	0.0	0.0	-69.38
59	17	-3.62	0.0	-5.80e-04	-7.68	0.0	-97.44	5.36	0.0	0.0	0.0	-3.81
		-3.81	0.0	0.0	0.0	10.0	-97.06	-2.32	0.0	0.0	0.0	-3.65
59	18	-15.21	0.0	-5.65e-06	-7.68	0.0	-76.35	-26.02	0.0	0.0	0.0	-15.21
		-18.21	0.0	0.0	0.0	10.0	-75.97	-33.70	0.0	0.0	0.0	-18.21
59	19	-54.55	0.0	-4.45e-05	-7.68	0.0	-162.47	-16.45	0.0	0.0	0.0	-54.55
		-56.59	0.0	0.0	0.0	10.0	-162.09	-24.13	0.0	0.0	0.0	-56.59
59	20	-6.66	0.0	-4.37e-04	-7.68	0.0	-92.17	-2.48	0.0	0.0	0.0	-6.66
		-7.29	0.0	0.0	0.0	10.0	-91.79	-10.16	0.0	0.0	0.0	-7.29
59	21	-15.21	0.0	-5.65e-06	-7.68	0.0	-76.35	-26.02	0.0	0.0	0.0	-15.21
		-18.21	0.0	0.0	0.0	10.0	-75.97	-33.70	0.0	0.0	0.0	-18.21
Trave		M3 mx/mn	M2 mx/mn	D 2 / D 3	Q 2 / Q 3		N	V 2	V 3	T		
		-93.67	0.0	-8.25e-04	-16.99		-266.53	-102.46	0.0	0.0		
		73.24	0.0	1.38e-04	0.0		-32.63	135.06	0.0	0.0		

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		kN m	kN m	m	kN/ m2	cm	kN	kN	kN	kN m	kN m	kN m
60	2	20.38	0.0	-1.25e-05	-1.37	0.0	-81.17	-23.61	0.0	0.0	0.0	20.38
		18.22	0.0	0.0		11.3	-79.51	-14.72	0.0	0.0	0.0	18.22

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
60	3	93.68	0.0	1.14e-04	-8.03	0.0	-245.81	21.04	0.0	0.0	0.0	90.58
		90.58	0.0	0.0		11.3	-243.57	33.73	0.0	0.0	0.0	93.68
60	10	-1.37	0.0	8.80e-04	-27.08	0.0	-91.57	22.79	0.0	0.0	0.0	-4.61
		-4.61	0.0	0.0		11.3	-89.91	34.49	0.0	0.0	0.0	-1.37
60	12	17.83	0.0	-1.59e-04	-5.31	0.0	-84.02	-13.82	0.0	0.0	0.0	17.83
		16.80	0.0	0.0		11.3	-82.36	-4.50	0.0	0.0	0.0	16.80
60	13	20.38	0.0	-1.25e-05	-1.37	0.0	-81.17	-23.61	0.0	0.0	0.0	20.38
		18.22	0.0	0.0		11.3	-79.51	-14.72	0.0	0.0	0.0	18.22
60	14	69.40	0.0	8.44e-05	-5.95	0.0	-182.08	15.59	0.0	0.0	0.0	67.10
		67.10	0.0	0.0		11.3	-180.42	24.99	0.0	0.0	0.0	69.40
60	17	3.71	0.0	6.55e-04	-20.42	0.0	-88.88	10.76	0.0	0.0	0.0	1.87
		1.87	0.0	0.0		11.3	-87.22	21.73	0.0	0.0	0.0	3.71
60	18	20.38	0.0	-1.25e-05	-1.37	0.0	-81.17	-23.61	0.0	0.0	0.0	20.38
		18.22	0.0	0.0		11.3	-79.51	-14.72	0.0	0.0	0.0	18.22
60	19	56.60	0.0	6.64e-05	-4.80	0.0	-156.85	5.79	0.0	0.0	0.0	55.42
		55.42	0.0	0.0		11.3	-155.19	15.06	0.0	0.0	0.0	56.60
60	20	7.34	0.0	4.94e-04	-15.66	0.0	-86.95	2.17	0.0	0.0	0.0	6.50
		6.50	0.0	0.0		11.3	-85.29	12.62	0.0	0.0	0.0	7.34
60	21	20.38	0.0	-1.25e-05	-1.37	0.0	-81.17	-23.61	0.0	0.0	0.0	20.38
		18.22	0.0	0.0		11.3	-79.51	-14.72	0.0	0.0	0.0	18.22
61	3	90.59	0.0	-1.40e-04	-18.50	0.0	-214.76	56.81	0.0	0.0	0.0	83.40
		83.40	0.0	0.0		11.3	-209.94	70.23	0.0	0.0	0.0	90.59
61	10	-4.52	0.0	-8.78e-04	-32.36	0.0	-71.26	26.83	0.0	0.0	0.0	-8.23
		-8.23	0.0	0.0		11.3	-67.69	38.79	0.0	0.0	0.0	-4.52
61	12	17.96	0.0	-1.64e-04	-7.71	0.0	-82.10	-5.63	0.0	0.0	0.0	17.96
		17.77	0.0	0.0		11.3	-78.53	3.63	0.0	0.0	0.0	17.85
61	14	67.11	0.0	-1.04e-04	-13.70	0.0	-159.08	42.08	0.0	0.0	0.0	61.78
		61.78	0.0	0.0		11.3	-155.51	52.03	0.0	0.0	0.0	67.11
61	17	1.94	0.0	-6.55e-04	-24.79	0.0	-74.45	16.01	0.0	0.0	0.0	-0.51
		-0.51	0.0	0.0		11.3	-70.87	27.14	0.0	0.0	0.0	1.94
61	19	55.43	0.0	-8.25e-05	-11.07	0.0	-140.20	27.83	0.0	0.0	0.0	51.73
		51.73	0.0	0.0		11.3	-136.63	37.48	0.0	0.0	0.0	55.43
61	20	6.55	0.0	-4.96e-04	-19.39	0.0	-76.72	8.27	0.0	0.0	0.0	5.01
		5.01	0.0	0.0		11.3	-73.15	18.81	0.0	0.0	0.0	6.55
61	21	21.58	0.0	-1.84e-05	-3.17	0.0	-83.55	-14.92	0.0	0.0	0.0	21.58
		20.38	0.0	0.0		11.3	-79.97	-6.16	0.0	0.0	0.0	20.38
62	3	83.39	0.0	1.64e-04	-28.06	0.0	-180.02	87.18	0.0	0.0	0.0	72.97
		72.97	0.0	0.0		11.3	-173.95	98.58	0.0	0.0	0.0	83.39
62	10	-8.32	0.0	-8.76e-04	-36.17	0.0	-54.75	27.76	0.0	0.0	0.0	-11.96
		-11.96	0.0	0.0		11.3	-50.26	37.86	0.0	0.0	0.0	-8.32
62	12	17.95	0.0	1.69e-04	-9.74	0.0	-80.19	3.76	0.0	0.0	0.0	17.18
		17.18	0.0	0.0		11.3	-75.70	10.95	0.0	0.0	0.0	17.95
62	14	61.77	0.0	1.22e-04	-20.79	0.0	-133.34	64.58	0.0	0.0	0.0	54.05
		54.05	0.0	0.0		11.3	-128.85	73.02	0.0	0.0	0.0	61.77
62	17	-0.57	0.0	-6.55e-04	-28.04	0.0	-62.66	19.54	0.0	0.0	0.0	-3.23
		-3.23	0.0	0.0		11.3	-58.17	28.74	0.0	0.0	0.0	-0.57
62	19	51.72	0.0	9.75e-05	-16.79	0.0	-121.33	47.45	0.0	0.0	0.0	45.96
		45.96	0.0	0.0		11.3	-116.84	55.44	0.0	0.0	0.0	51.72
62	20	4.96	0.0	-4.97e-04	-22.23	0.0	-68.31	13.67	0.0	0.0	0.0	3.00
		3.00	0.0	0.0		11.3	-63.82	22.23	0.0	0.0	0.0	4.96
62	21	21.70	0.0	2.46e-05	-4.81	0.0	-85.27	-3.94	0.0	0.0	0.0	21.70
		21.51	0.0	0.0		11.3	-80.78	2.70	0.0	0.0	0.0	21.57
63	3	72.95	0.0	1.86e-04	-36.27	0.0	-133.85	114.98	0.0	0.0	0.0	59.57
		59.57	0.0	0.0		11.3	-136.56	121.63	0.0	0.0	0.0	72.95
63	10	-12.04	0.0	-8.72e-04	-38.34	0.0	-35.43	33.37	0.0	0.0	0.0	-16.17
		-16.17	0.0	0.0		11.3	-37.44	39.51	0.0	0.0	0.0	-12.04
63	12	17.17	0.0	1.74e-04	-11.32	0.0	-70.78	17.70	0.0	0.0	0.0	14.99
		14.99	0.0	0.0		11.3	-72.79	20.86	0.0	0.0	0.0	17.17
63	14	54.04	0.0	1.38e-04	-26.86	0.0	-99.15	85.17	0.0	0.0	0.0	44.12
		44.12	0.0	0.0		11.3	-101.16	90.09	0.0	0.0	0.0	54.04
63	17	-3.30	0.0	6.54e-04	-30.01	0.0	-46.62	27.74	0.0	0.0	0.0	-6.73
		-6.73	0.0	0.0		11.3	-48.63	32.96	0.0	0.0	0.0	-3.30
63	19	45.95	0.0	1.11e-04	-21.70	0.0	-94.01	66.79	0.0	0.0	0.0	38.15
		38.15	0.0	0.0		11.3	-96.02	71.13	0.0	0.0	0.0	45.95
63	20	2.95	0.0	4.98e-04	-24.06	0.0	-54.62	23.71	0.0	0.0	0.0	9.86e-03
		9.86e-03	0.0	0.0		11.3	-56.63	28.28	0.0	0.0	0.0	2.95
63	21	21.70	0.0	3.09e-05	-6.21	0.0	-78.60	11.64	0.0	0.0	0.0	20.23
		20.23	0.0	0.0		11.3	-80.61	14.24	0.0	0.0	0.0	21.70
64	3	59.57	0.0	-2.03e-04	-42.75	0.0	-87.50	131.16	0.0	0.0	0.0	44.28
		44.28	0.0	0.0		11.3	-89.60	139.06	0.0	0.0	0.0	59.57
64	10	-16.07	0.0	-8.67e-04	-38.79	0.0	-20.41	33.96	0.0	0.0	0.0	-20.29
		-20.29	0.0	0.0		11.3	-21.97	40.54	0.0	0.0	0.0	-16.07
64	11	32.01	0.0	6.18e-05	-1.72	0.0	-110.77	39.65	0.0	0.0	0.0	27.23

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		27.23	0.0	0.0		11.3	-114.16	44.82	0.0	0.0	0.0	32.01
64	12	15.00	0.0	-1.79e-04	-12.37	0.0	-60.41	28.27	0.0	0.0	0.0	11.60
		11.60	0.0	0.0		11.3	-61.97	31.94	0.0	0.0	0.0	15.00
64	13	20.23	0.0	-3.68e-05	-7.31	0.0	-69.93	24.61	0.0	0.0	0.0	17.26
		17.26	0.0	0.0		11.3	-71.48	27.72	0.0	0.0	0.0	20.23
64	14	44.13	0.0	-1.50e-04	-31.67	0.0	-64.81	97.16	0.0	0.0	0.0	32.80
		32.80	0.0	0.0		11.3	-66.37	103.01	0.0	0.0	0.0	44.13
64	17	-6.66	0.0	-6.52e-04	-30.63	0.0	-33.25	31.54	0.0	0.0	0.0	-10.55
		-10.55	0.0	0.0		11.3	-34.81	37.21	0.0	0.0	0.0	-6.66
64	18	20.23	0.0	-3.68e-05	-7.31	0.0	-69.93	24.61	0.0	0.0	0.0	17.26
		17.26	0.0	0.0		11.3	-71.48	27.72	0.0	0.0	0.0	20.23
64	19	38.15	0.0	-1.22e-04	-25.58	0.0	-66.09	79.02	0.0	0.0	0.0	28.92
		28.92	0.0	0.0		11.3	-67.65	84.19	0.0	0.0	0.0	38.15
64	20	0.06	0.0	-4.98e-04	-24.80	0.0	-42.42	29.81	0.0	0.0	0.0	-3.60
		-3.60	0.0	0.0		11.3	-43.98	34.84	0.0	0.0	0.0	0.06
64	21	20.23	0.0	-3.68e-05	-7.31	0.0	-69.93	24.61	0.0	0.0	0.0	17.26
		17.26	0.0	0.0		11.3	-71.48	27.72	0.0	0.0	0.0	20.23
65	3	44.27	0.0	2.16e-04	-47.21	0.0	-44.24	136.25	0.0	0.0	0.0	28.35
		28.35	0.0	0.0		11.3	-45.63	145.04	0.0	0.0	0.0	44.27
65	10	-20.32	0.0	-8.61e-04	-37.47	0.0	-10.62	27.17	0.0	0.0	0.0	-23.77
		-23.77	0.0	0.0		11.3	-11.65	33.87	0.0	0.0	0.0	-20.32
65	11	27.23	0.0	-6.97e-05	-1.68	0.0	-97.20	56.84	0.0	0.0	0.0	20.47
		20.47	0.0	0.0		11.3	-99.44	62.61	0.0	0.0	0.0	27.23
65	12	11.58	0.0	-1.82e-04	-12.84	0.0	-49.88	35.83	0.0	0.0	0.0	7.30
		7.30	0.0	0.0		11.3	-50.91	39.83	0.0	0.0	0.0	11.58
65	13	17.26	0.0	-4.17e-05	-8.06	0.0	-59.98	35.50	0.0	0.0	0.0	13.05
		13.05	0.0	0.0		11.3	-61.01	38.98	0.0	0.0	0.0	17.26
65	14	32.79	0.0	1.60e-04	-34.97	0.0	-32.77	100.93	0.0	0.0	0.0	21.00
		21.00	0.0	0.0		11.3	-33.80	107.44	0.0	0.0	0.0	32.79
65	17	-10.58	0.0	-6.49e-04	-29.85	0.0	-23.42	29.33	0.0	0.0	0.0	-14.23
		-14.23	0.0	0.0		11.3	-24.45	35.20	0.0	0.0	0.0	-10.58
65	18	17.26	0.0	-4.17e-05	-8.06	0.0	-59.98	35.50	0.0	0.0	0.0	13.05
		13.05	0.0	0.0		11.3	-61.01	38.98	0.0	0.0	0.0	17.26
65	19	28.91	0.0	1.30e-04	-28.24	0.0	-39.57	84.57	0.0	0.0	0.0	19.01
		19.01	0.0	0.0		11.3	-40.60	90.32	0.0	0.0	0.0	28.91
65	20	-3.62	0.0	-4.97e-04	-24.40	0.0	-32.56	30.87	0.0	0.0	0.0	-7.41
		-7.41	0.0	0.0		11.3	-33.59	36.14	0.0	0.0	0.0	-3.62
65	21	17.26	0.0	-4.17e-05	-8.06	0.0	-59.98	35.50	0.0	0.0	0.0	13.05
		13.05	0.0	0.0		11.3	-61.01	38.98	0.0	0.0	0.0	17.26
66	2	13.09	0.0	4.08e-05	-8.18	0.0	-54.93	37.62	0.0	0.0	0.0	9.10
		9.10	0.0	0.0		10.2	-55.67	40.82	0.0	0.0	0.0	13.09
66	3	28.42	0.0	-2.01e-04	-48.00	0.0	-24.41	132.54	0.0	0.0	0.0	14.52
		14.52	0.0	0.0		10.2	-25.41	140.60	0.0	0.0	0.0	28.42
66	4	23.84	0.0	-1.87e-04	-45.13	0.0	-5.19	119.37	0.0	0.0	0.0	11.34
		11.34	0.0	0.0		10.2	-5.93	126.32	0.0	0.0	0.0	23.84
66	10	-23.72	0.0	7.69e-04	-35.39	0.0	-8.96	27.18	0.0	0.0	0.0	-26.78
		-26.78	0.0	0.0		10.2	-9.70	33.07	0.0	0.0	0.0	-23.72
66	11	20.54	0.0	6.78e-05	-1.55	0.0	-90.72	60.12	0.0	0.0	0.0	14.15
		14.15	0.0	0.0		10.2	-92.33	65.44	0.0	0.0	0.0	20.54
66	12	7.34	0.0	1.65e-04	-12.61	0.0	-45.08	37.58	0.0	0.0	0.0	3.33
		3.33	0.0	0.0		10.2	-45.82	41.22	0.0	0.0	0.0	7.34
66	13	13.09	0.0	4.08e-05	-8.18	0.0	-54.93	37.62	0.0	0.0	0.0	9.10
		9.10	0.0	0.0		10.2	-55.67	40.82	0.0	0.0	0.0	13.09
66	14	21.05	0.0	-1.49e-04	-35.55	0.0	-18.08	98.17	0.0	0.0	0.0	10.76
		10.76	0.0	0.0		10.2	-18.83	104.15	0.0	0.0	0.0	21.05
66	17	-14.17	0.0	5.80e-04	-28.34	0.0	-20.88	29.88	0.0	0.0	0.0	-17.48
		-17.48	0.0	0.0		10.2	-21.62	35.08	0.0	0.0	0.0	-14.17
66	18	13.09	0.0	4.08e-05	-8.18	0.0	-54.93	37.62	0.0	0.0	0.0	9.10
		9.10	0.0	0.0		10.2	-55.67	40.82	0.0	0.0	0.0	13.09
66	19	19.06	0.0	-1.22e-04	-28.71	0.0	-27.29	83.04	0.0	0.0	0.0	10.34
		10.34	0.0	0.0		10.2	-28.04	88.32	0.0	0.0	0.0	19.06
66	20	-7.36	0.0	4.45e-04	-23.30	0.0	-29.39	31.82	0.0	0.0	0.0	-10.83
		-10.83	0.0	0.0		10.2	-30.13	36.51	0.0	0.0	0.0	-7.36
66	21	13.09	0.0	4.08e-05	-8.18	0.0	-54.93	37.62	0.0	0.0	0.0	9.10
		9.10	0.0	0.0		10.2	-55.67	40.82	0.0	0.0	0.0	13.09
67	3	14.58	0.0	2.05e-04	-47.82	0.0	-14.56	123.00	0.0	0.0	0.0	1.65
		1.65	0.0	0.0		10.2	-15.50	131.07	0.0	0.0	0.0	14.58
67	4	11.38	0.0	-1.90e-04	-44.97	0.0	3.80	110.88	0.0	0.0	0.0	-0.26
		-0.26	0.0	0.0		10.2	3.10	117.82	0.0	0.0	0.0	11.38
67	10	-26.74	0.0	7.62e-04	-33.65	0.0	-9.98	16.14	0.0	0.0	0.0	-28.67
		-28.67	0.0	0.0		10.2	-10.68	21.87	0.0	0.0	0.0	-26.74
67	11	14.20	0.0	7.12e-05	-1.41	0.0	-88.00	55.16	0.0	0.0	0.0	8.32
		8.32	0.0	0.0		10.2	-89.52	60.50	0.0	0.0	0.0	14.20

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
67	12	3.37	0.0	1.66e-04	-12.28	0.0	-42.98	33.18	0.0	0.0	0.0	-0.19
		-0.19	0.0	0.0		10.2	-43.67	36.80	0.0	0.0	0.0	3.37
67	13	9.14	0.0	4.30e-05	-8.14	0.0	-52.44	34.62	0.0	0.0	0.0	5.46
		5.46	0.0	0.0		10.2	-53.14	37.83	0.0	0.0	0.0	9.14
67	14	10.80	0.0	1.52e-04	-35.42	0.0	-10.78	91.11	0.0	0.0	0.0	1.22
		1.22	0.0	0.0		10.2	-11.48	97.09	0.0	0.0	0.0	10.80
67	17	-17.43	0.0	5.76e-04	-27.04	0.0	-20.99	20.93	0.0	0.0	0.0	-19.82
		-19.82	0.0	0.0		10.2	-21.69	26.01	0.0	0.0	0.0	-17.43
67	18	9.14	0.0	4.30e-05	-8.14	0.0	-52.44	34.62	0.0	0.0	0.0	5.46
		5.46	0.0	0.0		10.2	-53.14	37.83	0.0	0.0	0.0	9.14
67	19	10.38	0.0	1.25e-04	-28.60	0.0	-21.20	76.99	0.0	0.0	0.0	2.28
		2.28	0.0	0.0		10.2	-21.89	82.27	0.0	0.0	0.0	10.38
67	20	-10.79	0.0	4.43e-04	-22.31	0.0	-28.86	24.35	0.0	0.0	0.0	-13.50
		-13.50	0.0	0.0		10.2	-29.55	28.96	0.0	0.0	0.0	-10.79
67	21	9.14	0.0	4.30e-05	-8.14	0.0	-52.44	34.62	0.0	0.0	0.0	5.46
		5.46	0.0	0.0		10.2	-53.14	37.83	0.0	0.0	0.0	9.14
68	3	1.67	0.0	-2.05e-04	-47.62	0.0	-5.34	116.35	0.0	0.0	0.0	-10.58
		-10.58	0.0	0.0		10.2	-6.22	124.42	0.0	0.0	0.0	1.67
68	4	-0.24	0.0	-1.90e-04	-44.79	0.0	12.20	104.90	0.0	0.0	0.0	-11.27
		-11.27	0.0	0.0		10.2	11.55	111.84	0.0	0.0	0.0	-0.24
68	10	-28.67	0.0	7.56e-04	-31.91	0.0	-11.46	15.40	0.0	0.0	0.0	-30.52
		-30.52	0.0	0.0		10.2	-12.11	20.96	0.0	0.0	0.0	-28.67
68	11	8.33	0.0	-7.32e-05	-1.26	0.0	-85.46	52.03	0.0	0.0	0.0	2.77
		2.77	0.0	0.0		10.2	-86.88	57.38	0.0	0.0	0.0	8.33
68	12	-0.17	0.0	-1.66e-04	-11.95	0.0	-41.08	31.44	0.0	0.0	0.0	-3.55
		-3.55	0.0	0.0		10.2	-41.73	35.04	0.0	0.0	0.0	-0.17
68	13	5.48	0.0	-4.43e-05	-8.09	0.0	-50.12	32.70	0.0	0.0	0.0	1.99
		1.99	0.0	0.0		10.2	-50.77	35.92	0.0	0.0	0.0	5.48
68	14	1.24	0.0	-1.52e-04	-35.28	0.0	-3.96	86.18	0.0	0.0	0.0	-7.84
		-7.84	0.0	0.0		10.2	-4.61	92.16	0.0	0.0	0.0	1.24
68	17	-19.82	0.0	5.71e-04	-25.74	0.0	-21.48	19.88	0.0	0.0	0.0	-22.09
		-22.09	0.0	0.0		10.2	-22.13	24.84	0.0	0.0	0.0	-19.82
68	18	5.48	0.0	-4.43e-05	-8.09	0.0	-50.12	32.70	0.0	0.0	0.0	1.99
		1.99	0.0	0.0		10.2	-50.77	35.92	0.0	0.0	0.0	5.48
68	19	2.30	0.0	-1.25e-04	-28.48	0.0	-15.50	72.81	0.0	0.0	0.0	-5.38
		-5.38	0.0	0.0		10.2	-16.15	78.10	0.0	0.0	0.0	2.30
68	20	-13.49	0.0	4.39e-04	-21.32	0.0	-28.64	23.09	0.0	0.0	0.0	-16.07
		-16.07	0.0	0.0		10.2	-29.29	27.61	0.0	0.0	0.0	-13.49
68	21	5.48	0.0	-4.43e-05	-8.09	0.0	-50.12	32.70	0.0	0.0	0.0	1.99
		1.99	0.0	0.0		10.2	-50.77	35.92	0.0	0.0	0.0	5.48
69	3	-10.59	0.0	-2.03e-04	-47.41	0.0	3.23	106.42	0.0	0.0	0.0	-21.83
		-21.83	0.0	0.0		10.2	2.41	114.48	0.0	0.0	0.0	-10.59
69	4	-11.29	0.0	-1.87e-04	-44.60	0.0	20.01	95.90	0.0	0.0	0.0	-21.40
		-21.40	0.0	0.0		10.2	19.41	102.83	0.0	0.0	0.0	-11.29
69	9	-29.78	0.0	-7.64e-04	-32.99	0.0	-30.15	16.81	0.0	0.0	0.0	-31.82
		-31.82	0.0	0.0		10.2	-30.96	23.35	0.0	0.0	0.0	-29.78
69	10	-30.48	0.0	-7.48e-04	-30.18	0.0	-13.36	6.29	0.0	0.0	0.0	-31.40
		-31.40	0.0	0.0		10.2	-13.97	11.70	0.0	0.0	0.0	-30.48
69	11	2.79	0.0	-7.38e-05	-1.10	0.0	-83.11	47.97	0.0	0.0	0.0	-2.36
		-2.36	0.0	0.0		10.2	-84.42	53.33	0.0	0.0	0.0	2.79
69	12	-3.54	0.0	-1.65e-04	-11.61	0.0	-39.40	27.63	0.0	0.0	0.0	-6.53
		-6.53	0.0	0.0		10.2	-40.00	31.21	0.0	0.0	0.0	-3.54
69	13	2.00	0.0	-4.47e-05	-8.03	0.0	-47.96	30.06	0.0	0.0	0.0	-1.22
		-1.22	0.0	0.0		10.2	-48.57	33.28	0.0	0.0	0.0	2.00
69	14	-7.84	0.0	-1.50e-04	-35.12	0.0	2.39	78.83	0.0	0.0	0.0	-16.17
		-16.17	0.0	0.0		10.2	1.79	84.80	0.0	0.0	0.0	-7.84
69	17	-22.06	0.0	-5.66e-04	-24.44	0.0	-22.33	12.46	0.0	0.0	0.0	-23.57
		-23.57	0.0	0.0		10.2	-22.94	17.29	0.0	0.0	0.0	-22.06
69	18	2.00	0.0	-4.47e-05	-8.03	0.0	-47.96	30.06	0.0	0.0	0.0	-1.22
		-1.22	0.0	0.0		10.2	-48.57	33.28	0.0	0.0	0.0	2.00
69	19	-5.38	0.0	-1.24e-04	-28.34	0.0	-10.20	66.64	0.0	0.0	0.0	-12.43
		-12.43	0.0	0.0		10.2	-10.80	71.92	0.0	0.0	0.0	-5.38
69	20	-16.05	0.0	-4.36e-04	-20.33	0.0	-28.74	16.86	0.0	0.0	0.0	-17.99
		-17.99	0.0	0.0		10.2	-29.34	21.29	0.0	0.0	0.0	-16.05
69	21	2.00	0.0	-4.47e-05	-8.03	0.0	-47.96	30.06	0.0	0.0	0.0	-1.22
		-1.22	0.0	0.0		10.2	-48.57	33.28	0.0	0.0	0.0	2.00
70	2	-1.23	0.0	-4.45e-05	-7.97	0.0	-45.97	27.73	0.0	0.0	0.0	-4.21
		-4.21	0.0	0.0		10.2	-46.52	30.96	0.0	0.0	0.0	-1.23
70	3	-21.84	0.0	-1.98e-04	-47.18	0.0	11.15	100.11	0.0	0.0	0.0	-32.44
		-32.44	0.0	0.0		10.2	10.40	108.17	0.0	0.0	0.0	-21.84
70	4	-21.41	0.0	-1.82e-04	-44.39	0.0	27.24	90.41	0.0	0.0	0.0	-30.96
		-30.96	0.0	0.0		10.2	26.68	97.33	0.0	0.0	0.0	-21.41
70	9	-31.86	0.0	-7.56e-04	-31.23	0.0	-31.77	13.70	0.0	0.0	0.0	-33.57

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
70	10	-33.57	0.0	0.0		10.2	-32.52	20.07	0.0	0.0	0.0	-31.86
		-31.43	0.0	-7.41e-04	-28.45	0.0	-15.68	3.99	0.0	0.0	0.0	-32.10
		-32.10	0.0	0.0		10.2	-16.24	9.23	0.0	0.0	0.0	-31.43
70	11	-2.36	0.0	-7.33e-05	-0.94	0.0	-80.94	44.15	0.0	0.0	0.0	-7.12
		-7.12	0.0	0.0		10.2	-82.15	49.52	0.0	0.0	0.0	-2.36
70	12	-6.54	0.0	-1.64e-04	-11.27	0.0	-37.92	25.29	0.0	0.0	0.0	-9.29
		-9.29	0.0	0.0		10.2	-38.48	28.84	0.0	0.0	0.0	-6.54
70	13	-1.23	0.0	-4.45e-05	-7.97	0.0	-45.97	27.73	0.0	0.0	0.0	-4.21
		-4.21	0.0	0.0		10.2	-46.52	30.96	0.0	0.0	0.0	-1.23
70	14	-16.18	0.0	-1.46e-04	-34.95	0.0	8.26	74.16	0.0	0.0	0.0	-24.03
		-24.03	0.0	0.0		10.2	7.70	80.12	0.0	0.0	0.0	-16.18
70	17	-23.60	0.0	-5.60e-04	-23.14	0.0	-23.53	10.15	0.0	0.0	0.0	-24.87
		-24.87	0.0	0.0		10.2	-24.09	14.86	0.0	0.0	0.0	-23.60
70	18	-1.23	0.0	-4.45e-05	-7.97	0.0	-45.97	27.73	0.0	0.0	0.0	-4.21
		-4.21	0.0	0.0		10.2	-46.52	30.96	0.0	0.0	0.0	-1.23
70	19	-12.44	0.0	-1.21e-04	-28.20	0.0	-5.30	62.55	0.0	0.0	0.0	-19.07
		-19.07	0.0	0.0		10.2	-5.85	67.83	0.0	0.0	0.0	-12.44
70	20	-18.01	0.0	-4.31e-04	-19.34	0.0	-29.14	14.54	0.0	0.0	0.0	-19.71
		-19.71	0.0	0.0		10.2	-29.70	18.89	0.0	0.0	0.0	-18.01
70	21	-1.23	0.0	-4.45e-05	-7.97	0.0	-45.97	27.73	0.0	0.0	0.0	-4.21
		-4.21	0.0	0.0		10.2	-46.52	30.96	0.0	0.0	0.0	-1.23
71	2	-4.18	0.0	4.35e-05	-7.90	0.0	-44.14	26.03	0.0	0.0	0.0	-7.00
		-7.00	0.0	0.0		10.2	-44.65	29.26	0.0	0.0	0.0	-4.18
71	3	-32.35	0.0	1.90e-04	-46.94	0.0	18.42	91.94	0.0	0.0	0.0	-42.11
		-42.11	0.0	0.0		10.2	17.73	99.98	0.0	0.0	0.0	-32.35
71	4	-30.88	0.0	1.75e-04	-44.18	0.0	33.87	82.83	0.0	0.0	0.0	-39.66
		-39.66	0.0	0.0		10.2	33.36	89.74	0.0	0.0	0.0	-30.88
71	10	-32.02	0.0	7.33e-04	-26.72	0.0	-18.39	-1.31	0.0	0.0	0.0	-32.15
		-32.15	0.0	0.0		10.2	-18.90	3.77	0.0	0.0	0.0	-32.02
71	11	-7.08	0.0	7.16e-05	-0.78	0.0	-78.95	41.07	0.0	0.0	0.0	-11.53
		-11.53	0.0	0.0		10.2	-80.07	46.45	0.0	0.0	0.0	-7.08
71	12	-9.26	0.0	1.62e-04	-10.93	0.0	-36.64	22.99	0.0	0.0	0.0	-11.78
		-11.78	0.0	0.0		10.2	-37.15	26.52	0.0	0.0	0.0	-9.26
71	13	-4.18	0.0	4.35e-05	-7.90	0.0	-44.14	26.03	0.0	0.0	0.0	-7.00
		-7.00	0.0	0.0		10.2	-44.65	29.26	0.0	0.0	0.0	-4.18
71	14	-23.96	0.0	1.41e-04	-34.77	0.0	13.65	68.10	0.0	0.0	0.0	-31.19
		-31.19	0.0	0.0		10.2	13.14	74.06	0.0	0.0	0.0	-23.96
71	17	-24.81	0.0	5.54e-04	-21.84	0.0	-25.06	5.78	0.0	0.0	0.0	-25.63
		-25.63	0.0	0.0		10.2	-25.57	10.38	0.0	0.0	0.0	-24.81
71	18	-4.18	0.0	4.35e-05	-7.90	0.0	-44.14	26.03	0.0	0.0	0.0	-7.00
		-7.00	0.0	0.0		10.2	-44.65	29.26	0.0	0.0	0.0	-4.18
71	19	-19.02	0.0	1.16e-04	-28.06	0.0	-0.80	57.58	0.0	0.0	0.0	-25.14
		-25.14	0.0	0.0		10.2	-1.31	62.86	0.0	0.0	0.0	-19.02
71	20	-19.65	0.0	4.27e-04	-18.36	0.0	-29.83	10.84	0.0	0.0	0.0	-20.97
		-20.97	0.0	0.0		10.2	-30.34	15.10	0.0	0.0	0.0	-19.65
71	21	-4.18	0.0	4.35e-05	-7.90	0.0	-44.14	26.03	0.0	0.0	0.0	-7.00
		-7.00	0.0	0.0		10.2	-44.65	29.26	0.0	0.0	0.0	-4.18
72	2	-6.95	0.0	4.18e-05	-7.84	0.0	-42.47	23.24	0.0	0.0	0.0	-9.48
		-9.48	0.0	0.0		10.2	-42.93	26.48	0.0	0.0	0.0	-6.95
72	3	-42.02	0.0	1.80e-04	-46.71	0.0	25.05	83.32	0.0	0.0	0.0	-50.91
		-50.91	0.0	0.0		10.2	24.42	91.35	0.0	0.0	0.0	-42.02
72	4	-39.59	0.0	1.65e-04	-43.97	0.0	39.91	75.18	0.0	0.0	0.0	-47.59
		-47.59	0.0	0.0		10.2	39.45	82.08	0.0	0.0	0.0	-39.59
72	10	-31.79	0.0	7.26e-04	-25.00	0.0	-21.47	-5.18	0.0	0.0	0.0	-31.79
		-32.07	0.0	0.0		10.2	-21.94	-0.27	0.0	0.0	0.0	-32.07
72	11	-11.47	0.0	6.89e-05	-0.63	0.0	-77.15	36.79	0.0	0.0	0.0	-15.49
		-15.49	0.0	0.0		10.2	-78.16	42.17	0.0	0.0	0.0	-11.47
72	12	-11.73	0.0	1.59e-04	-10.59	0.0	-35.56	19.91	0.0	0.0	0.0	-13.93
		-13.93	0.0	0.0		10.2	-36.02	23.41	0.0	0.0	0.0	-11.73
72	13	-6.95	0.0	4.18e-05	-7.84	0.0	-42.47	23.24	0.0	0.0	0.0	-9.48
		-9.48	0.0	0.0		10.2	-42.93	26.48	0.0	0.0	0.0	-6.95
72	14	-31.13	0.0	1.33e-04	-34.60	0.0	18.56	61.72	0.0	0.0	0.0	-37.71
		-37.71	0.0	0.0		10.2	18.09	67.67	0.0	0.0	0.0	-31.13
72	17	-25.56	0.0	5.48e-04	-20.55	0.0	-26.91	2.19	0.0	0.0	0.0	-26.01
		-26.01	0.0	0.0		10.2	-27.38	6.67	0.0	0.0	0.0	-25.56
72	18	-6.95	0.0	4.18e-05	-7.84	0.0	-42.47	23.24	0.0	0.0	0.0	-9.48
		-9.48	0.0	0.0		10.2	-42.93	26.48	0.0	0.0	0.0	-6.95
72	19	-25.08	0.0	1.10e-04	-27.91	0.0	3.30	52.10	0.0	0.0	0.0	-30.65
		-30.65	0.0	0.0		10.2	2.84	57.37	0.0	0.0	0.0	-25.08
72	20	-20.90	0.0	4.22e-04	-17.37	0.0	-30.80	7.45	0.0	0.0	0.0	-21.87
		-21.87	0.0	0.0		10.2	-31.27	11.62	0.0	0.0	0.0	-20.90
72	21	-6.95	0.0	4.18e-05	-7.84	0.0	-42.47	23.24	0.0	0.0	0.0	-9.48
		-9.48	0.0	0.0		10.2	-42.93	26.48	0.0	0.0	0.0	-6.95



Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
73	2	-9.44	0.0	3.96e-05	-7.77	0.0	-40.97	21.07	0.0	0.0	0.0	-11.75
		-11.75	0.0	0.0		10.2	-41.38	24.31	0.0	0.0	0.0	-9.44
73	3	-50.82	0.0	1.68e-04	-46.48	0.0	31.03	74.89	0.0	0.0	0.0	-58.85
		-58.85	0.0	0.0		10.2	30.46	82.91	0.0	0.0	0.0	-50.82
73	4	-47.52	0.0	1.54e-04	-43.76	0.0	45.36	67.52	0.0	0.0	0.0	-54.74
		-54.74	0.0	0.0		10.2	44.95	74.41	0.0	0.0	0.0	-47.52
73	10	-30.98	0.0	-7.18e-04	-23.29	0.0	-24.91	-8.91	0.0	0.0	0.0	-30.98
		-31.65	0.0	0.0		10.2	-25.32	-4.17	0.0	0.0	0.0	-31.65
73	11	-15.44	0.0	6.52e-05	-0.48	0.0	-75.53	33.07	0.0	0.0	0.0	-19.08
		-19.08	0.0	0.0		10.2	-76.44	38.45	0.0	0.0	0.0	-15.44
73	12	-13.88	0.0	1.56e-04	-10.25	0.0	-34.68	17.42	0.0	0.0	0.0	-15.83
		-15.83	0.0	0.0		10.2	-35.09	20.90	0.0	0.0	0.0	-13.88
73	13	-9.44	0.0	3.96e-05	-7.77	0.0	-40.97	21.07	0.0	0.0	0.0	-11.75
		-11.75	0.0	0.0		10.2	-41.38	24.31	0.0	0.0	0.0	-9.44
73	14	-37.65	0.0	1.24e-04	-34.43	0.0	22.98	55.48	0.0	0.0	0.0	-43.59
		-43.59	0.0	0.0		10.2	22.56	61.42	0.0	0.0	0.0	-37.65
73	17	-25.89	0.0	5.42e-04	-19.27	0.0	-29.07	-1.14	0.0	0.0	0.0	-26.00
		-26.01	0.0	0.0		10.2	-29.49	3.22	0.0	0.0	0.0	-25.89
73	18	-9.44	0.0	3.96e-05	-7.77	0.0	-40.97	21.07	0.0	0.0	0.0	-11.75
		-11.75	0.0	0.0		10.2	-41.38	24.31	0.0	0.0	0.0	-9.44
73	19	-30.60	0.0	1.03e-04	-27.76	0.0	7.00	46.87	0.0	0.0	0.0	-35.63
		-35.63	0.0	0.0		10.2	6.58	52.14	0.0	0.0	0.0	-30.60
73	20	-21.78	0.0	4.17e-04	-16.39	0.0	-32.04	4.41	0.0	0.0	0.0	-22.43
		-22.43	0.0	0.0		10.2	-32.46	8.49	0.0	0.0	0.0	-21.78
73	21	-9.44	0.0	3.96e-05	-7.77	0.0	-40.97	21.07	0.0	0.0	0.0	-11.75
		-11.75	0.0	0.0		10.2	-41.38	24.31	0.0	0.0	0.0	-9.44
74	2	-11.72	0.0	-3.68e-05	-7.71	0.0	-39.63	18.31	0.0	0.0	0.0	-13.74
		-13.74	0.0	0.0		10.2	-40.00	21.55	0.0	0.0	0.0	-11.72
74	3	-58.77	0.0	-1.54e-04	-46.25	0.0	36.35	65.96	0.0	0.0	0.0	-65.89
		-65.89	0.0	0.0		10.2	35.85	73.97	0.0	0.0	0.0	-58.77
74	4	-54.67	0.0	-1.41e-04	-43.56	0.0	50.22	59.55	0.0	0.0	0.0	-61.08
		-61.08	0.0	0.0		10.2	49.85	66.42	0.0	0.0	0.0	-54.67
74	10	-29.53	0.0	-7.11e-04	-21.59	0.0	-28.68	-16.80	0.0	0.0	0.0	-29.53
		-31.00	0.0	0.0		10.2	-29.05	-12.23	0.0	0.0	0.0	-31.00
74	11	-19.04	0.0	-6.07e-05	-0.34	0.0	-74.09	28.80	0.0	0.0	0.0	-22.24
		-22.24	0.0	0.0		10.2	-74.90	34.19	0.0	0.0	0.0	-19.04
74	12	-15.80	0.0	-1.52e-04	-9.92	0.0	-33.99	13.79	0.0	0.0	0.0	-17.38
		-17.38	0.0	0.0		10.2	-34.36	17.24	0.0	0.0	0.0	-15.80
74	13	-11.72	0.0	-3.68e-05	-7.71	0.0	-39.63	18.31	0.0	0.0	0.0	-13.74
		-13.74	0.0	0.0		10.2	-40.00	21.55	0.0	0.0	0.0	-11.72
74	14	-43.53	0.0	-1.14e-04	-34.26	0.0	26.93	48.86	0.0	0.0	0.0	-48.81
		-48.81	0.0	0.0		10.2	26.56	54.79	0.0	0.0	0.0	-43.53
74	17	-25.43	0.0	-5.36e-04	-17.99	0.0	-31.52	-7.70	0.0	0.0	0.0	-25.43
		-26.00	0.0	0.0		10.2	-31.89	-3.47	0.0	0.0	0.0	-26.00
74	18	-11.72	0.0	-3.68e-05	-7.71	0.0	-39.63	18.31	0.0	0.0	0.0	-13.74
		-13.74	0.0	0.0		10.2	-40.00	21.55	0.0	0.0	0.0	-11.72
74	19	-35.58	0.0	-9.48e-05	-27.62	0.0	10.29	41.22	0.0	0.0	0.0	-40.04
		-40.04	0.0	0.0		10.2	9.92	46.48	0.0	0.0	0.0	-35.58
74	20	-22.43	0.0	-4.11e-04	-15.42	0.0	-33.54	-1.20	0.0	0.0	0.0	-22.51
		-22.53	0.0	0.0		10.2	-33.91	2.79	0.0	0.0	0.0	-22.43
74	21	-11.72	0.0	-3.68e-05	-7.71	0.0	-39.63	18.31	0.0	0.0	0.0	-13.74
		-13.74	0.0	0.0		10.2	-40.00	21.55	0.0	0.0	0.0	-11.72
75	2	-13.72	0.0	-3.36e-05	-7.65	0.0	-38.46	15.80	0.0	0.0	0.0	-15.50
		-15.50	0.0	0.0		10.2	-38.78	19.05	0.0	0.0	0.0	-13.72
75	3	-65.85	0.0	1.38e-04	-46.05	0.0	41.03	56.72	0.0	0.0	0.0	-72.03
		-72.03	0.0	0.0		10.2	40.60	64.72	0.0	0.0	0.0	-65.85
75	4	-61.05	0.0	1.27e-04	-43.37	0.0	54.49	51.19	0.0	0.0	0.0	-66.60
		-66.60	0.0	0.0		10.2	54.17	58.06	0.0	0.0	0.0	-61.05
75	10	-28.05	0.0	-7.04e-04	-19.89	0.0	-32.76	-17.10	0.0	0.0	0.0	-28.05
		-29.56	0.0	0.0		10.2	-33.08	-12.69	0.0	0.0	0.0	-29.56
75	11	-22.22	0.0	-5.55e-05	-0.21	0.0	-72.84	24.76	0.0	0.0	0.0	-25.01
		-25.01	0.0	0.0		10.2	-73.54	30.15	0.0	0.0	0.0	-22.22
75	12	-17.37	0.0	-1.48e-04	-9.59	0.0	-33.49	11.58	0.0	0.0	0.0	-18.72
		-18.72	0.0	0.0		10.2	-33.81	15.01	0.0	0.0	0.0	-17.37
75	13	-13.72	0.0	-3.36e-05	-7.65	0.0	-38.46	15.80	0.0	0.0	0.0	-15.50
		-15.50	0.0	0.0		10.2	-38.78	19.05	0.0	0.0	0.0	-13.72
75	14	-48.78	0.0	1.03e-04	-34.11	0.0	30.39	42.02	0.0	0.0	0.0	-53.35
		-53.35	0.0	0.0		10.2	30.07	47.94	0.0	0.0	0.0	-48.78
75	17	-24.79	0.0	-5.30e-04	-16.72	0.0	-34.24	-8.57	0.0	0.0	0.0	-24.79
		-25.46	0.0	0.0		10.2	-34.56	-4.46	0.0	0.0	0.0	-25.46
75	18	-13.72	0.0	-3.36e-05	-7.65	0.0	-38.46	15.80	0.0	0.0	0.0	-15.50
		-15.50	0.0	0.0		10.2	-38.78	19.05	0.0	0.0	0.0	-13.72
75	19	-40.01	0.0	-8.53e-05	-27.49	0.0	13.18	35.46	0.0	0.0	0.0	-43.89

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
75	20	-43.89	0.0	0.0		10.2	12.86	40.72	0.0	0.0	0.0	-40.01
		-22.47	0.0	-4.06e-04	-14.45	0.0	-35.29	-2.48	0.0	0.0	0.0	-22.47
		-22.55	0.0	0.0		10.2	-35.61	1.42	0.0	0.0	0.0	-22.52
75	21	-13.72	0.0	-3.36e-05	-7.65	0.0	-38.46	15.80	0.0	0.0	0.0	-15.50
		-15.50	0.0	0.0		10.2	-38.78	19.05	0.0	0.0	0.0	-13.72
76	2	-15.49	0.0	2.99e-05	-7.60	0.0	-37.45	13.03	0.0	0.0	0.0	-16.98
		-16.98	0.0	0.0		10.2	-37.72	16.27	0.0	0.0	0.0	-15.49
76	3	-72.06	0.0	1.21e-04	-45.85	0.0	45.06	47.04	0.0	0.0	0.0	-77.25
		-77.25	0.0	0.0		10.2	44.69	55.03	0.0	0.0	0.0	-72.06
76	4	-66.64	0.0	1.11e-04	-43.19	0.0	58.17	42.48	0.0	0.0	0.0	-71.31
		-71.31	0.0	0.0		10.2	57.89	49.33	0.0	0.0	0.0	-66.64
76	10	-25.88	0.0	6.97e-04	-18.20	0.0	-37.14	-23.47	0.0	0.0	0.0	-25.88
		-28.05	0.0	0.0		10.2	-37.41	-19.22	0.0	0.0	0.0	-28.05
76	11	-25.01	0.0	4.95e-05	-0.09	0.0	-71.76	20.52	0.0	0.0	0.0	-27.37
		-27.37	0.0	0.0		10.2	-72.36	25.91	0.0	0.0	0.0	-25.01
76	12	-18.71	0.0	1.43e-04	-9.26	0.0	-33.17	8.13	0.0	0.0	0.0	-19.71
		-19.71	0.0	0.0		10.2	-33.45	11.53	0.0	0.0	0.0	-18.71
76	13	-15.49	0.0	2.99e-05	-7.60	0.0	-37.45	13.03	0.0	0.0	0.0	-16.98
		-16.98	0.0	0.0		10.2	-37.72	16.27	0.0	0.0	0.0	-15.49
76	14	-53.38	0.0	9.00e-05	-33.96	0.0	33.38	34.84	0.0	0.0	0.0	-57.22
		-57.22	0.0	0.0		10.2	33.10	40.76	0.0	0.0	0.0	-53.38
76	17	-23.57	0.0	5.24e-04	-15.45	0.0	-37.22	-14.00	0.0	0.0	0.0	-23.57
		-24.79	0.0	0.0		10.2	-37.49	-10.02	0.0	0.0	0.0	-24.79
76	18	-15.49	0.0	2.99e-05	-7.60	0.0	-37.45	13.03	0.0	0.0	0.0	-16.98
		-16.98	0.0	0.0		10.2	-37.72	16.27	0.0	0.0	0.0	-15.49
76	19	-43.91	0.0	7.49e-05	-27.37	0.0	15.67	29.39	0.0	0.0	0.0	-47.16
		-47.16	0.0	0.0		10.2	15.40	34.64	0.0	0.0	0.0	-43.91
76	20	-21.92	0.0	4.01e-04	-13.49	0.0	-37.28	-7.25	0.0	0.0	0.0	-21.92
		-22.47	0.0	0.0		10.2	-37.55	-3.44	0.0	0.0	0.0	-22.47
76	21	-15.49	0.0	2.99e-05	-7.60	0.0	-37.45	13.03	0.0	0.0	0.0	-16.98
		-16.98	0.0	0.0		10.2	-37.72	16.27	0.0	0.0	0.0	-15.49
77	2	-16.98	0.0	-2.59e-05	-7.55	0.0	-36.61	10.63	0.0	0.0	0.0	-18.23
		-18.23	0.0	0.0		10.2	-36.83	13.88	0.0	0.0	0.0	-16.98
77	3	-77.25	0.0	-1.03e-04	-45.68	0.0	48.44	39.57	0.0	0.0	0.0	-81.69
		-81.69	0.0	0.0		10.2	48.13	47.56	0.0	0.0	0.0	-77.25
77	4	-71.31	0.0	-9.41e-05	-43.04	0.0	61.25	35.85	0.0	0.0	0.0	-75.31
		-75.31	0.0	0.0		10.2	61.03	42.70	0.0	0.0	0.0	-71.31
77	10	-23.60	0.0	-6.91e-04	-16.52	0.0	-41.79	-24.77	0.0	0.0	0.0	-23.60
		-25.92	0.0	0.0		10.2	-42.02	-20.69	0.0	0.0	0.0	-25.92
77	11	-27.36	0.0	-4.31e-05	0.11	0.0	-70.87	16.70	0.0	0.0	0.0	-29.34
		-29.34	0.0	0.0		10.2	-71.37	22.09	0.0	0.0	0.0	-27.36
77	12	-19.72	0.0	-1.39e-04	-8.94	0.0	-33.04	5.84	0.0	0.0	0.0	-20.49
		-20.49	0.0	0.0		10.2	-33.27	9.21	0.0	0.0	0.0	-19.72
77	13	-16.98	0.0	-2.59e-05	-7.55	0.0	-36.61	10.63	0.0	0.0	0.0	-18.23
		-18.23	0.0	0.0		10.2	-36.83	13.88	0.0	0.0	0.0	-16.98
77	14	-57.22	0.0	-7.64e-05	-33.84	0.0	35.88	29.31	0.0	0.0	0.0	-60.51
		-60.51	0.0	0.0		10.2	35.65	35.23	0.0	0.0	0.0	-57.22
77	17	-22.21	0.0	-5.19e-04	-14.19	0.0	-40.45	-15.59	0.0	0.0	0.0	-22.21
		-23.60	0.0	0.0		10.2	-40.67	-11.73	0.0	0.0	0.0	-23.60
77	18	-16.98	0.0	-2.59e-05	-7.55	0.0	-36.61	10.63	0.0	0.0	0.0	-18.23
		-18.23	0.0	0.0		10.2	-36.83	13.88	0.0	0.0	0.0	-16.98
77	19	-47.16	0.0	-6.38e-05	-27.26	0.0	17.76	24.64	0.0	0.0	0.0	-49.94
		-49.94	0.0	0.0		10.2	17.53	29.89	0.0	0.0	0.0	-47.16
77	20	-21.22	0.0	-3.95e-04	-12.53	0.0	-39.49	-9.04	0.0	0.0	0.0	-21.22
		-21.95	0.0	0.0		10.2	-39.71	-5.33	0.0	0.0	0.0	-21.95
77	21	-16.98	0.0	-2.59e-05	-7.55	0.0	-36.61	10.63	0.0	0.0	0.0	-18.23
		-18.23	0.0	0.0		10.2	-36.83	13.88	0.0	0.0	0.0	-16.98
78	2	-18.23	0.0	-2.16e-05	-7.50	0.0	-35.93	7.94	0.0	0.0	0.0	-19.20
		-19.20	0.0	0.0		10.2	-36.11	11.18	0.0	0.0	0.0	-18.23
78	3	-81.65	0.0	-8.39e-05	-45.53	0.0	51.17	30.01	0.0	0.0	0.0	-85.11
		-85.11	0.0	0.0		10.2	50.93	37.98	0.0	0.0	0.0	-81.65
78	4	-75.27	0.0	-7.63e-05	-42.90	0.0	63.75	27.23	0.0	0.0	0.0	-78.39
		-78.39	0.0	0.0		10.2	63.57	34.07	0.0	0.0	0.0	-75.27
78	10	-20.87	0.0	-6.86e-04	-14.85	0.0	-46.70	-28.50	0.0	0.0	0.0	-20.87
		-23.58	0.0	0.0		10.2	-46.88	-24.58	0.0	0.0	0.0	-23.58
78	11	-29.34	0.0	-3.61e-05	0.19	0.0	-70.16	12.40	0.0	0.0	0.0	-30.87
		-30.87	0.0	0.0		10.2	-70.56	17.79	0.0	0.0	0.0	-29.34
78	12	-20.48	0.0	-1.34e-04	-8.63	0.0	-33.09	2.90	0.0	0.0	0.0	-20.95
		-20.95	0.0	0.0		10.2	-33.28	6.24	0.0	0.0	0.0	-20.48
78	13	-18.23	0.0	-2.16e-05	-7.50	0.0	-35.93	7.94	0.0	0.0	0.0	-19.20
		-19.20	0.0	0.0		10.2	-36.11	11.18	0.0	0.0	0.0	-18.23
78	14	-60.48	0.0	-6.21e-05	-33.72	0.0	37.91	22.23	0.0	0.0	0.0	-63.04
		-63.04	0.0	0.0		10.2	37.73	28.13	0.0	0.0	0.0	-60.48

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
78	17	-20.44	0.0	-5.13e-04	-12.94	0.0	-43.91	-19.05	0.0	0.0	0.0	-20.44
		-22.19	0.0	0.0		10.2	-44.09	-15.31	0.0	0.0	0.0	-22.19
78	18	-18.23	0.0	-2.16e-05	-7.50	0.0	-35.93	7.94	0.0	0.0	0.0	-19.20
		-19.20	0.0	0.0		10.2	-36.11	11.18	0.0	0.0	0.0	-18.23
78	19	-49.92	0.0	-5.20e-05	-27.17	0.0	19.45	18.66	0.0	0.0	0.0	-52.08
		-52.08	0.0	0.0		10.2	19.27	23.90	0.0	0.0	0.0	-49.92
78	20	-20.13	0.0	-3.90e-04	-11.58	0.0	-41.91	-12.31	0.0	0.0	0.0	-20.13
		-21.20	0.0	0.0		10.2	-42.09	-8.69	0.0	0.0	0.0	-21.20
78	21	-18.23	0.0	-2.16e-05	-7.50	0.0	-35.93	7.94	0.0	0.0	0.0	-19.20
		-19.20	0.0	0.0		10.2	-36.11	11.18	0.0	0.0	0.0	-18.23
79	3	-85.11	0.0	-6.37e-05	-45.40	0.0	53.26	20.93	0.0	0.0	0.0	-87.64
		-87.64	0.0	0.0		10.2	53.08	28.89	0.0	0.0	0.0	-85.11
79	4	-78.38	0.0	-5.78e-05	-42.79	0.0	65.65	19.04	0.0	0.0	0.0	-80.67
		-80.67	0.0	0.0		10.2	65.52	25.88	0.0	0.0	0.0	-78.38
79	10	-17.92	0.0	-6.81e-04	-13.18	0.0	-51.84	-30.64	0.0	0.0	0.0	-17.92
		-20.85	0.0	0.0		10.2	-51.97	-26.88	0.0	0.0	0.0	-20.85
79	11	-30.88	0.0	-2.88e-05	0.25	0.0	-69.63	8.43	0.0	0.0	0.0	-32.02
		-32.02	0.0	0.0		10.2	-69.92	13.82	0.0	0.0	0.0	-30.88
79	12	-20.95	0.0	-1.29e-04	-8.33	0.0	-33.32	0.32	0.0	0.0	0.0	-21.15
		-21.15	0.0	0.0		10.2	-33.46	3.64	0.0	0.0	0.0	-20.95
79	14	-63.04	0.0	-4.72e-05	-33.63	0.0	39.45	15.50	0.0	0.0	0.0	-64.92
		-64.92	0.0	0.0		10.2	39.32	21.40	0.0	0.0	0.0	-63.04
79	17	-18.44	0.0	-5.09e-04	-11.70	0.0	-47.58	-21.30	0.0	0.0	0.0	-18.44
		-20.42	0.0	0.0		10.2	-47.71	-17.68	0.0	0.0	0.0	-20.42
79	19	-52.08	0.0	-3.97e-05	-27.09	0.0	20.73	12.97	0.0	0.0	0.0	-53.67
		-53.67	0.0	0.0		10.2	20.60	18.21	0.0	0.0	0.0	-52.08
79	20	-18.81	0.0	-3.86e-04	-10.64	0.0	-44.54	-14.63	0.0	0.0	0.0	-18.81
		-20.12	0.0	0.0		10.2	-44.67	-11.11	0.0	0.0	0.0	-20.12
79	21	-19.21	0.0	-1.70e-05	-7.47	0.0	-35.42	5.37	0.0	0.0	0.0	-19.93
		-19.93	0.0	0.0		10.2	-35.55	8.62	0.0	0.0	0.0	-19.21
80	3	-87.63	0.0	4.30e-05	-45.30	0.0	54.69	12.34	0.0	0.0	0.0	-89.29
		-89.29	0.0	0.0		10.2	54.58	20.30	0.0	0.0	0.0	-87.63
80	4	-80.65	0.0	3.87e-05	-42.70	0.0	66.97	11.26	0.0	0.0	0.0	-82.15
		-82.15	0.0	0.0		10.2	66.88	18.08	0.0	0.0	0.0	-80.65
80	9	-21.76	0.0	-6.81e-04	-14.12	0.0	-69.47	-32.88	0.0	0.0	0.0	-21.76
		-24.87	0.0	0.0		10.2	-69.58	-28.16	0.0	0.0	0.0	-24.87
80	10	-14.62	0.0	-6.76e-04	-11.52	0.0	-57.19	-33.96	0.0	0.0	0.0	-14.62
		-17.90	0.0	0.0		10.2	-57.28	-30.37	0.0	0.0	0.0	-17.90
80	12	-21.09	0.0	-1.24e-04	-8.03	0.0	-33.72	-2.22	0.0	0.0	0.0	-21.09
		-21.16	0.0	0.0		10.2	-33.81	1.07	0.0	0.0	0.0	-21.14
80	14	-64.91	0.0	3.19e-05	-33.56	0.0	40.51	9.14	0.0	0.0	0.0	-66.14
		-66.14	0.0	0.0		10.2	40.43	15.04	0.0	0.0	0.0	-64.91
80	17	-16.12	0.0	-5.04e-04	-10.46	0.0	-51.46	-24.35	0.0	0.0	0.0	-16.12
		-18.42	0.0	0.0		10.2	-51.54	-20.86	0.0	0.0	0.0	-18.42
80	19	-53.66	0.0	2.70e-05	-27.03	0.0	21.62	7.63	0.0	0.0	0.0	-54.70
		-54.70	0.0	0.0		10.2	21.53	12.86	0.0	0.0	0.0	-53.66
80	20	-17.19	0.0	-3.81e-04	-9.71	0.0	-47.36	-17.49	0.0	0.0	0.0	-17.19
		-18.80	0.0	0.0		10.2	-47.45	-14.06	0.0	0.0	0.0	-18.80
80	21	-19.92	0.0	-1.23e-05	-7.44	0.0	-35.07	3.09	0.0	0.0	0.0	-20.40
		-20.40	0.0	0.0		10.2	-35.15	6.33	0.0	0.0	0.0	-19.92
81	3	-89.26	0.0	2.19e-05	-45.23	0.0	55.48	3.18	0.0	0.0	0.0	-89.99
		-89.99	0.0	0.0		10.2	55.43	11.14	0.0	0.0	0.0	-89.26
81	4	-82.13	0.0	1.93e-05	-42.64	0.0	67.69	2.92	0.0	0.0	0.0	-82.77
		-82.77	0.0	0.0		10.2	67.65	9.75	0.0	0.0	0.0	-82.13
81	9	-18.37	0.0	6.76e-04	-12.46	0.0	-74.95	-35.27	0.0	0.0	0.0	-18.37
		-21.73	0.0	0.0		10.2	-75.00	-30.72	0.0	0.0	0.0	-21.73
81	10	-11.16	0.0	6.73e-04	-9.87	0.0	-62.74	-35.52	0.0	0.0	0.0	-11.16
		-14.60	0.0	0.0		10.2	-62.78	-32.10	0.0	0.0	0.0	-14.60
81	12	-20.76	0.0	1.19e-04	-7.74	0.0	-34.30	-4.55	0.0	0.0	0.0	-20.76
		-21.06	0.0	0.0		10.2	-34.33	-1.28	0.0	0.0	0.0	-21.06
81	14	-66.12	0.0	1.62e-05	-33.50	0.0	41.10	2.35	0.0	0.0	0.0	-66.66
		-66.66	0.0	0.0		10.2	41.06	8.25	0.0	0.0	0.0	-66.12
81	17	-13.61	0.0	5.00e-04	-9.23	0.0	-55.52	-26.12	0.0	0.0	0.0	-13.61
		-16.10	0.0	0.0		10.2	-55.56	-22.75	0.0	0.0	0.0	-16.10
81	19	-54.68	0.0	1.40e-05	-26.98	0.0	22.10	1.95	0.0	0.0	0.0	-55.14
		-55.14	0.0	0.0		10.2	22.06	7.18	0.0	0.0	0.0	-54.68
81	20	-15.36	0.0	3.77e-04	-8.78	0.0	-50.36	-19.41	0.0	0.0	0.0	-15.36
		-17.17	0.0	0.0		10.2	-50.40	-16.07	0.0	0.0	0.0	-17.17
81	21	-20.37	0.0	7.50e-06	-7.41	0.0	-34.89	0.72	0.0	0.0	0.0	-20.61
		-20.61	0.0	0.0		10.2	-34.92	3.96	0.0	0.0	0.0	-20.37
82	3	-89.84	0.0	2.70e-06	-45.19	0.0	55.67	-4.77	0.0	0.0	0.0	-89.84
		-89.99	0.0	0.0		10.2	55.67	3.19	0.0	0.0	0.0	-89.92
82	4	-82.66	0.0	2.45e-06	-42.60	0.0	67.87	-4.04	0.0	0.0	0.0	-82.66

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
82	9	-82.78	0.0	0.0		10.2	67.87	2.78	0.0	0.0	0.0	-82.72
		-14.54	0.0	6.71e-04	-10.85	0.0	-80.50	-39.89	0.0	0.0	0.0	-14.54
		-18.38	0.0	0.0		10.2	-80.50	-35.50	0.0	0.0	0.0	-18.38
82	10	-7.36	0.0	6.70e-04	-8.26	0.0	-68.30	-39.17	0.0	0.0	0.0	-7.36
		-11.18	0.0	0.0		10.2	-68.30	-35.91	0.0	0.0	0.0	-11.18
82	12	-20.13	0.0	1.14e-04	-7.46	0.0	-35.00	-7.55	0.0	0.0	0.0	-20.13
		-20.73	0.0	0.0		10.2	-35.00	-4.31	0.0	0.0	0.0	-20.73
82	14	-66.55	0.0	2.00e-06	-33.47	0.0	41.24	-3.53	0.0	0.0	0.0	-66.55
		-66.66	0.0	0.0		10.2	41.24	2.36	0.0	0.0	0.0	-66.61
82	17	-10.77	0.0	4.97e-04	-8.04	0.0	-59.63	-29.55	0.0	0.0	0.0	-10.77
		-13.61	0.0	0.0		10.2	-59.63	-26.30	0.0	0.0	0.0	-13.61
82	19	-55.04	0.0	1.78e-06	-26.95	0.0	22.21	-3.16	0.0	0.0	0.0	-55.04
		-55.14	0.0	0.0		10.2	22.21	2.07	0.0	0.0	0.0	-55.10
82	20	-13.21	0.0	3.74e-04	-7.88	0.0	-53.44	-22.68	0.0	0.0	0.0	-13.21
		-15.35	0.0	0.0		10.2	-53.44	-19.43	0.0	0.0	0.0	-15.35
82	21	-20.53	0.0	2.63e-06	-7.40	0.0	-34.85	-2.07	0.0	0.0	0.0	-20.53
		-20.59	0.0	0.0		10.2	-34.85	1.17	0.0	0.0	0.0	-20.57
83	3	-88.62	0.0	2.06e-05	-45.21	0.0	55.09	-15.58	0.0	0.0	0.0	-88.62
		-89.80	0.0	0.0		10.2	55.19	-7.62	0.0	0.0	0.0	-89.80
83	4	-81.55	0.0	1.98e-05	-42.63	0.0	67.35	-13.89	0.0	0.0	0.0	-81.55
		-82.62	0.0	0.0		10.2	67.42	-7.07	0.0	0.0	0.0	-82.62
83	9	-10.72	0.0	-6.68e-04	-9.11	0.0	-86.76	-38.89	0.0	0.0	0.0	-10.72
		-14.47	0.0	0.0		10.2	-86.67	-34.68	0.0	0.0	0.0	-14.47
83	10	-3.65	0.0	-6.69e-04	-6.52	0.0	-74.50	-37.20	0.0	0.0	0.0	-3.65
		-7.29	0.0	0.0		10.2	-74.44	-34.13	0.0	0.0	0.0	-7.29
83	12	-19.29	0.0	-1.09e-04	-7.18	0.0	-35.97	-9.65	0.0	0.0	0.0	-19.29
		-20.11	0.0	0.0		10.2	-35.91	-6.44	0.0	0.0	0.0	-20.11
83	14	-65.65	0.0	1.53e-05	-33.49	0.0	40.81	-11.54	0.0	0.0	0.0	-65.65
		-66.52	0.0	0.0		10.2	40.88	-5.64	0.0	0.0	0.0	-66.52
83	17	-7.94	0.0	-4.95e-04	-6.75	0.0	-64.27	-28.81	0.0	0.0	0.0	-7.94
		-10.72	0.0	0.0		10.2	-64.20	-25.69	0.0	0.0	0.0	-10.72
83	19	-54.28	0.0	1.20e-05	-26.97	0.0	21.85	-9.86	0.0	0.0	0.0	-54.28
		-55.02	0.0	0.0		10.2	21.92	-4.63	0.0	0.0	0.0	-55.02
83	20	-11.01	0.0	-3.70e-04	-6.91	0.0	-56.96	-22.81	0.0	0.0	0.0	-11.01
		-13.17	0.0	0.0		10.2	-56.89	-19.66	0.0	0.0	0.0	-13.17
83	21	-20.19	0.0	-2.23e-06	-7.39	0.0	-35.03	-4.81	0.0	0.0	0.0	-20.19
		-20.52	0.0	0.0		10.2	-34.96	-1.57	0.0	0.0	0.0	-20.52
84	3	-86.57	0.0	-4.16e-05	-45.28	0.0	53.96	-24.32	0.0	0.0	0.0	-86.57
		-88.64	0.0	0.0		10.2	54.10	-16.36	0.0	0.0	0.0	-88.64
84	4	-79.71	0.0	3.91e-05	-42.69	0.0	66.32	-21.65	0.0	0.0	0.0	-79.71
		-81.57	0.0	0.0		10.2	66.43	-14.83	0.0	0.0	0.0	-81.57
84	9	-6.23	0.0	-6.65e-04	-7.51	0.0	-92.72	-46.31	0.0	0.0	0.0	-6.23
		-10.74	0.0	0.0		10.2	-92.57	-42.26	0.0	0.0	0.0	-10.74
84	10	0.63	0.0	-6.68e-04	-4.92	0.0	-80.35	-43.64	0.0	0.0	0.0	0.63
		-3.67	0.0	0.0		10.2	-80.25	-40.72	0.0	0.0	0.0	-3.67
84	12	-18.14	0.0	-1.05e-04	-6.92	0.0	-37.00	-13.13	0.0	0.0	0.0	-18.14
		-19.31	0.0	0.0		10.2	-36.90	-9.95	0.0	0.0	0.0	-19.31
84	14	-64.13	0.0	-3.08e-05	-33.54	0.0	39.97	-18.01	0.0	0.0	0.0	-64.13
		-65.66	0.0	0.0		10.2	40.07	-12.12	0.0	0.0	0.0	-65.66
84	17	-4.62	0.0	-4.93e-04	-5.56	0.0	-68.68	-34.30	0.0	0.0	0.0	-4.62
		-7.96	0.0	0.0		10.2	-68.57	-31.30	0.0	0.0	0.0	-7.96
84	19	-53.00	0.0	-2.48e-05	-27.01	0.0	21.14	-15.42	0.0	0.0	0.0	-53.00
		-54.30	0.0	0.0		10.2	21.25	-10.19	0.0	0.0	0.0	-54.30
84	20	-8.36	0.0	-3.68e-04	-6.02	0.0	-60.34	-27.63	0.0	0.0	0.0	-8.36
		-11.02	0.0	0.0		10.2	-60.23	-24.57	0.0	0.0	0.0	-11.02
84	21	-19.60	0.0	-7.00e-06	-7.40	0.0	-35.33	-7.62	0.0	0.0	0.0	-19.60
		-20.22	0.0	0.0		10.2	-35.22	-4.39	0.0	0.0	0.0	-20.22
85	3	-83.67	0.0	-6.20e-05	-45.37	0.0	52.16	-32.28	0.0	0.0	0.0	-83.67
		-86.55	0.0	0.0		10.2	52.36	-24.31	0.0	0.0	0.0	-86.55
85	4	-77.09	0.0	-5.80e-05	-42.77	0.0	64.69	-29.02	0.0	0.0	0.0	-77.09
		-79.69	0.0	0.0		10.2	64.84	-22.20	0.0	0.0	0.0	-79.69
85	9	-1.99	0.0	6.64e-04	-5.86	0.0	-99.01	-43.94	0.0	0.0	0.0	-1.99
		-6.27	0.0	0.0		10.2	-98.80	-40.06	0.0	0.0	0.0	-6.27
85	10	4.59	0.0	6.68e-04	-3.28	0.0	-86.48	-40.69	0.0	0.0	0.0	4.59
		0.59	0.0	0.0		10.2	-86.32	-37.94	0.0	0.0	0.0	0.59
85	12	-16.84	0.0	1.00e-04	-6.66	0.0	-38.22	-14.16	0.0	0.0	0.0	-16.84
		-18.13	0.0	0.0		10.2	-38.07	-11.02	0.0	0.0	0.0	-18.13
85	14	-61.98	0.0	-4.59e-05	-33.61	0.0	38.63	-23.91	0.0	0.0	0.0	-61.98
		-64.11	0.0	0.0		10.2	38.79	-18.01	0.0	0.0	0.0	-64.11
85	17	-1.48	0.0	4.92e-04	-4.34	0.0	-73.34	-32.55	0.0	0.0	0.0	-1.48
		-4.64	0.0	0.0		10.2	-73.18	-29.68	0.0	0.0	0.0	-4.64
85	19	-51.18	0.0	-3.74e-05	-27.06	0.0	20.02	-20.25	0.0	0.0	0.0	-51.18
		-52.98	0.0	0.0		10.2	20.18	-15.02	0.0	0.0	0.0	-52.98

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
85	20	-5.81	0.0	3.66e-04	-5.11	0.0	-63.95	-26.73	0.0	0.0	0.0	-5.81
		-8.38	0.0	0.0		10.2	-63.80	-23.77	0.0	0.0	0.0	-8.38
85	21	-18.80	0.0	1.16e-05	-7.42	0.0	-35.80	-9.29	0.0	0.0	0.0	-18.80
		-19.58	0.0	0.0		10.2	-35.65	-6.05	0.0	0.0	0.0	-19.58
86	3	-79.76	0.0	8.18e-05	-45.48	0.0	49.71	-42.01	0.0	0.0	0.0	-79.76
		-83.63	0.0	0.0		10.2	49.98	-34.05	0.0	0.0	0.0	-83.63
86	4	-73.58	0.0	7.62e-05	-42.87	0.0	62.46	-37.56	0.0	0.0	0.0	-73.58
		-77.05	0.0	0.0		10.2	62.66	-30.72	0.0	0.0	0.0	-77.05
86	9	2.81	0.0	6.63e-04	-4.22	0.0	-105.45	-48.56	0.0	0.0	0.0	2.81
		-1.95	0.0	0.0		10.2	-105.18	-44.85	0.0	0.0	0.0	-1.95
86	10	8.98	0.0	6.69e-04	-1.63	0.0	-92.69	-44.10	0.0	0.0	0.0	8.98
		4.63	0.0	0.0		10.2	-92.49	-41.53	0.0	0.0	0.0	4.63
86	12	-15.18	0.0	9.64e-05	-6.41	0.0	-39.60	-17.71	0.0	0.0	0.0	-15.18
		-16.82	0.0	0.0		10.2	-39.40	-14.59	0.0	0.0	0.0	-16.82
86	14	-59.08	0.0	6.06e-05	-33.69	0.0	36.82	-31.12	0.0	0.0	0.0	-59.08
		-61.94	0.0	0.0		10.2	37.02	-25.22	0.0	0.0	0.0	-61.94
86	17	2.08	0.0	4.91e-04	-3.13	0.0	-78.11	-35.97	0.0	0.0	0.0	2.08
		-1.44	0.0	0.0		10.2	-77.91	-33.22	0.0	0.0	0.0	-1.44
86	19	-48.72	0.0	4.95e-05	-27.13	0.0	18.50	-26.53	0.0	0.0	0.0	-48.72
		-51.15	0.0	0.0		10.2	18.71	-21.29	0.0	0.0	0.0	-51.15
86	20	-2.85	0.0	3.64e-04	-4.20	0.0	-67.69	-30.16	0.0	0.0	0.0	-2.85
		-5.78	0.0	0.0		10.2	-67.49	-27.29	0.0	0.0	0.0	-5.78
86	21	-17.65	0.0	1.61e-05	-7.45	0.0	-36.44	-12.74	0.0	0.0	0.0	-17.65
		-18.79	0.0	0.0		10.2	-36.24	-9.50	0.0	0.0	0.0	-18.79
87	3	-74.95	0.0	1.01e-04	-45.62	0.0	46.61	-51.45	0.0	0.0	0.0	-74.95
		-79.78	0.0	0.0		10.2	46.95	-43.48	0.0	0.0	0.0	-79.78
87	4	-69.25	0.0	9.36e-05	-43.00	0.0	59.65	-46.10	0.0	0.0	0.0	-69.25
		-73.59	0.0	0.0		10.2	59.90	-39.26	0.0	0.0	0.0	-73.59
87	9	7.50	0.0	6.64e-04	-2.58	0.0	-112.02	-47.71	0.0	0.0	0.0	7.50
		2.82	0.0	0.0		10.2	-111.68	-44.18	0.0	0.0	0.0	2.82
87	10	13.20	0.0	6.71e-04	1.47	0.0	-98.98	-42.37	0.0	0.0	0.0	13.20
		9.01	0.0	0.0		10.2	-98.73	-39.97	0.0	0.0	0.0	9.01
87	12	-13.35	0.0	-9.28e-05	-6.16	0.0	-41.13	-19.65	0.0	0.0	0.0	-13.35
		-15.20	0.0	0.0		10.2	-40.88	-16.56	0.0	0.0	0.0	-15.20
87	14	-55.52	0.0	7.46e-05	-33.79	0.0	34.53	-38.11	0.0	0.0	0.0	-55.52
		-59.10	0.0	0.0		10.2	34.78	-32.20	0.0	0.0	0.0	-59.10
87	17	5.55	0.0	4.92e-04	-1.91	0.0	-82.98	-35.34	0.0	0.0	0.0	5.55
		2.09	0.0	0.0		10.2	-82.73	-32.73	0.0	0.0	0.0	2.09
87	19	-45.71	0.0	6.10e-05	-27.21	0.0	16.58	-32.40	0.0	0.0	0.0	-45.71
		-48.74	0.0	0.0		10.2	16.83	-27.16	0.0	0.0	0.0	-48.74
87	20	0.09	0.0	3.64e-04	-3.29	0.0	-71.54	-30.32	0.0	0.0	0.0	0.09
		-2.85	0.0	0.0		10.2	-71.30	-27.55	0.0	0.0	0.0	-2.85
87	21	-16.29	0.0	-2.03e-05	-7.48	0.0	-37.25	-15.27	0.0	0.0	0.0	-16.29
		-17.68	0.0	0.0		10.2	-37.00	-12.03	0.0	0.0	0.0	-17.68
88	3	-69.32	0.0	-1.18e-04	-45.78	0.0	42.87	-59.48	0.0	0.0	0.0	-69.32
		-74.96	0.0	0.0		10.2	43.27	-51.51	0.0	0.0	0.0	-74.96
88	4	-64.18	0.0	-1.10e-04	-43.15	0.0	56.24	-53.24	0.0	0.0	0.0	-64.18
		-69.25	0.0	0.0		10.2	56.54	-46.40	0.0	0.0	0.0	-69.25
88	9	12.57	0.0	-6.66e-04	-0.93	0.0	-118.70	-51.59	0.0	0.0	0.0	12.57
		7.49	0.0	0.0		10.2	-118.30	-48.23	0.0	0.0	0.0	7.49
88	10	17.70	0.0	-6.74e-04	3.13	0.0	-105.32	-45.35	0.0	0.0	0.0	17.70
		13.20	0.0	0.0		10.2	-105.03	-43.12	0.0	0.0	0.0	13.20
88	12	-11.25	0.0	-8.96e-05	-5.92	0.0	-42.80	-22.41	0.0	0.0	0.0	-11.25
		-13.38	0.0	0.0		10.2	-42.50	-19.35	0.0	0.0	0.0	-13.38
88	14	-51.35	0.0	-8.77e-05	-33.91	0.0	31.75	-44.06	0.0	0.0	0.0	-51.35
		-55.53	0.0	0.0		10.2	32.05	-38.15	0.0	0.0	0.0	-55.53
88	17	9.31	0.0	-4.93e-04	-0.69	0.0	-87.93	-38.21	0.0	0.0	0.0	9.31
		5.55	0.0	0.0		10.2	-87.63	-35.73	0.0	0.0	0.0	5.55
88	19	-42.18	0.0	-7.18e-05	-27.31	0.0	14.26	-37.51	0.0	0.0	0.0	-42.18
		-45.73	0.0	0.0		10.2	14.56	-32.26	0.0	0.0	0.0	-45.73
88	20	3.31	0.0	-3.64e-04	-2.38	0.0	-75.50	-33.12	0.0	0.0	0.0	3.31
		0.08	0.0	0.0		10.2	-75.20	-30.45	0.0	0.0	0.0	0.08
88	21	-14.67	0.0	-2.41e-05	-7.51	0.0	-38.22	-17.83	0.0	0.0	0.0	-14.67
		-16.32	0.0	0.0		10.2	-37.92	-14.60	0.0	0.0	0.0	-16.32
89	3	-62.74	0.0	-1.35e-04	-45.95	0.0	38.48	-68.46	0.0	0.0	0.0	-62.74
		-69.30	0.0	0.0		10.2	38.94	-60.48	0.0	0.0	0.0	-69.30
89	4	-58.25	0.0	-1.25e-04	-43.31	0.0	52.25	-61.42	0.0	0.0	0.0	-58.25
		-64.15	0.0	0.0		10.2	52.59	-54.56	0.0	0.0	0.0	-64.15
89	9	17.52	0.0	-6.69e-04	2.15	0.0	-125.47	-50.93	0.0	0.0	0.0	17.52
		12.50	0.0	0.0		10.2	-125.00	-47.75	0.0	0.0	0.0	12.50
89	10	22.00	0.0	-6.78e-04	4.80	0.0	-111.70	-43.89	0.0	0.0	0.0	22.00
		17.64	0.0	0.0		10.2	-111.35	-41.84	0.0	0.0	0.0	17.64
89	12	-8.97	0.0	-8.69e-05	-5.69	0.0	-44.62	-24.24	0.0	0.0	0.0	-8.97

Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
89	14	-11.29	0.0	0.0		10.2	-44.27	-21.20	0.0	0.0	0.0	-11.29
		-46.47	0.0	-9.98e-05	-34.04	0.0	28.50	-50.71	0.0	0.0	0.0	-46.47
		-51.33	0.0	0.0		10.2	28.85	-44.80	0.0	0.0	0.0	-51.33
89	17	12.98	0.0	-4.95e-04	1.59	0.0	-92.94	-37.73	0.0	0.0	0.0	12.98
		9.26	0.0	0.0		10.2	-92.59	-35.37	0.0	0.0	0.0	9.26
89	19	-38.06	0.0	-8.18e-05	-27.42	0.0	11.54	-43.07	0.0	0.0	0.0	-38.06
		-42.17	0.0	0.0		10.2	11.88	-37.82	0.0	0.0	0.0	-42.17
89	20	6.53	0.0	-3.65e-04	-1.48	0.0	-79.54	-33.33	0.0	0.0	0.0	6.53
		3.27	0.0	0.0		10.2	-79.20	-30.75	0.0	0.0	0.0	3.27
89	21	-12.81	0.0	-2.76e-05	-7.55	0.0	-39.35	-20.13	0.0	0.0	0.0	-12.81
		-14.69	0.0	0.0		10.2	-39.01	-16.90	0.0	0.0	0.0	-14.69
90	3	-55.27	0.0	-1.50e-04	-46.15	0.0	33.44	-77.35	0.0	0.0	0.0	-55.27
		-62.74	0.0	0.0		10.2	33.97	-69.35	0.0	0.0	0.0	-62.74
90	4	-51.53	0.0	-1.39e-04	-43.49	0.0	47.67	-69.50	0.0	0.0	0.0	-51.53
		-58.25	0.0	0.0		10.2	48.06	-62.64	0.0	0.0	0.0	-58.25
90	9	22.55	0.0	6.73e-04	3.82	0.0	-132.30	-50.22	0.0	0.0	0.0	22.55
		17.59	0.0	0.0		10.2	-131.77	-47.22	0.0	0.0	0.0	17.59
90	10	26.29	0.0	-6.84e-04	6.48	0.0	-118.08	-42.37	0.0	0.0	0.0	26.29
		22.07	0.0	0.0		10.2	-117.69	-40.50	0.0	0.0	0.0	22.07
90	12	-6.47	0.0	8.48e-05	-5.45	0.0	-46.58	-26.03	0.0	0.0	0.0	-6.47
		-8.97	0.0	0.0		10.2	-46.18	-23.03	0.0	0.0	0.0	-8.97
90	14	-40.94	0.0	-1.11e-04	-34.18	0.0	24.77	-57.30	0.0	0.0	0.0	-40.94
		-46.47	0.0	0.0		10.2	25.16	-51.37	0.0	0.0	0.0	-46.47
90	17	16.70	0.0	4.98e-04	2.83	0.0	-98.00	-37.20	0.0	0.0	0.0	16.70
		13.03	0.0	0.0		10.2	-97.61	-34.98	0.0	0.0	0.0	13.03
90	19	-33.38	0.0	9.08e-05	-27.54	0.0	8.42	-48.58	0.0	0.0	0.0	-33.38
		-38.06	0.0	0.0		10.2	8.81	-43.33	0.0	0.0	0.0	-38.06
90	20	9.85	0.0	3.66e-04	-0.57	0.0	-83.66	-33.51	0.0	0.0	0.0	9.85
		6.57	0.0	0.0		10.2	-83.27	-31.03	0.0	0.0	0.0	6.57
90	21	-10.70	0.0	3.06e-05	-7.60	0.0	-40.64	-22.43	0.0	0.0	0.0	-10.70
		-12.81	0.0	0.0		10.2	-40.25	-19.20	0.0	0.0	0.0	-12.81
91	3	-46.99	0.0	-1.63e-04	-46.35	0.0	27.76	-85.04	0.0	0.0	0.0	-46.99
		-55.24	0.0	0.0		10.2	28.35	-77.04	0.0	0.0	0.0	-55.24
91	4	-44.07	0.0	1.51e-04	-43.68	0.0	42.49	-76.47	0.0	0.0	0.0	-44.07
		-51.50	0.0	0.0		10.2	42.93	-69.59	0.0	0.0	0.0	-51.50
91	9	27.81	0.0	-6.78e-04	5.49	0.0	-139.18	-53.18	0.0	0.0	0.0	27.81
		22.54	0.0	0.0		10.2	-138.59	-50.36	0.0	0.0	0.0	22.54
91	10	30.73	0.0	-6.90e-04	8.17	0.0	-124.45	-44.61	0.0	0.0	0.0	30.73
		26.28	0.0	0.0		10.2	-124.01	-42.92	0.0	0.0	0.0	26.28
91	12	-3.74	0.0	-8.33e-05	-5.22	0.0	-48.67	-28.18	0.0	0.0	0.0	-3.74
		-6.45	0.0	0.0		10.2	-48.23	-25.21	0.0	0.0	0.0	-6.45
91	14	-34.81	0.0	-1.20e-04	-34.33	0.0	20.56	-62.99	0.0	0.0	0.0	-34.81
		-40.92	0.0	0.0		10.2	21.00	-57.06	0.0	0.0	0.0	-40.92
91	17	20.60	0.0	-5.02e-04	4.07	0.0	-103.10	-39.40	0.0	0.0	0.0	20.60
		16.70	0.0	0.0		10.2	-102.66	-37.31	0.0	0.0	0.0	16.70
91	19	-28.19	0.0	-9.87e-05	-27.66	0.0	4.89	-53.37	0.0	0.0	0.0	-28.19
		-33.36	0.0	0.0		10.2	5.33	-48.12	0.0	0.0	0.0	-33.36
91	20	13.36	0.0	-3.68e-04	1.14	0.0	-87.85	-35.67	0.0	0.0	0.0	13.36
		9.85	0.0	0.0		10.2	-87.41	-33.30	0.0	0.0	0.0	9.85
91	21	-8.35	0.0	-3.31e-05	-7.64	0.0	-42.10	-24.49	0.0	0.0	0.0	-8.35
		-10.67	0.0	0.0		10.2	-41.67	-21.27	0.0	0.0	0.0	-10.67
92	3	-37.78	0.0	-1.74e-04	-46.61	0.0	22.03	-94.40	0.0	0.0	0.0	-37.78
		-46.96	0.0	0.0		10.2	22.67	-86.39	0.0	0.0	0.0	-46.96
92	4	-35.79	0.0	-1.61e-04	-43.92	0.0	37.28	-84.69	0.0	0.0	0.0	-35.79
		-44.04	0.0	0.0		10.2	37.75	-77.80	0.0	0.0	0.0	-44.04
92	9	32.92	0.0	6.84e-04	7.11	0.0	-145.78	-52.03	0.0	0.0	0.0	32.92
		27.76	0.0	0.0		10.2	-145.14	-49.38	0.0	0.0	0.0	27.76
92	10	34.91	0.0	6.96e-04	9.80	0.0	-130.53	-42.32	0.0	0.0	0.0	34.91
		30.68	0.0	0.0		10.2	-130.06	-40.80	0.0	0.0	0.0	30.68
92	12	-0.76	0.0	8.23e-05	-5.01	0.0	-50.71	-30.71	0.0	0.0	0.0	-0.76
		-3.74	0.0	0.0		10.2	-50.24	-27.77	0.0	0.0	0.0	-3.74
92	14	-27.98	0.0	-1.29e-04	-34.53	0.0	16.32	-69.93	0.0	0.0	0.0	-27.98
		-34.79	0.0	0.0		10.2	16.79	-63.99	0.0	0.0	0.0	-34.79
92	17	24.38	0.0	5.07e-04	5.27	0.0	-107.98	-38.54	0.0	0.0	0.0	24.38
		20.57	0.0	0.0		10.2	-107.51	-36.58	0.0	0.0	0.0	20.57
92	19	-22.41	0.0	-1.05e-04	-27.82	0.0	1.35	-59.38	0.0	0.0	0.0	-22.41
		-28.17	0.0	0.0		10.2	1.82	-54.13	0.0	0.0	0.0	-28.17
92	20	16.87	0.0	3.71e-04	2.02	0.0	-91.88	-35.84	0.0	0.0	0.0	16.87
		13.34	0.0	0.0		10.2	-91.41	-33.57	0.0	0.0	0.0	13.34
92	21	-5.68	0.0	3.51e-05	-7.70	0.0	-43.55	-27.75	0.0	0.0	0.0	-5.68
		-8.34	0.0	0.0		10.2	-43.08	-24.53	0.0	0.0	0.0	-8.34
93	3	-27.74	0.0	1.83e-04	-46.71	0.0	13.90	-102.37	0.0	0.0	0.0	-27.74
		-37.76	0.0	0.0		10.2	14.64	-94.35	0.0	0.0	0.0	-37.76

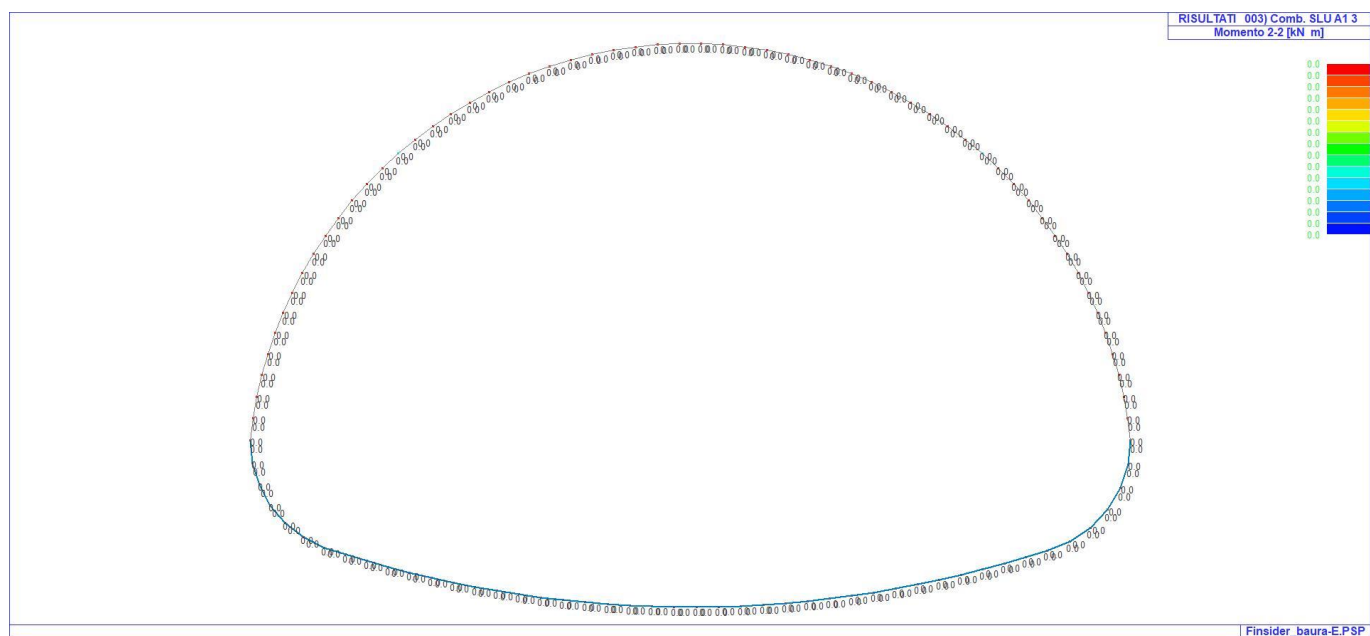
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
93	4	-26.74	0.0	1.70e-04	-44.01	0.0	29.89	-92.14	0.0	0.0	0.0	-26.74
		-35.78	0.0	0.0		10.2	30.44	-85.24	0.0	0.0	0.0	-35.78
93	9	37.92	0.0	-6.93e-04	8.94	0.0	-153.30	-49.90	0.0	0.0	0.0	37.92
		32.96	0.0	0.0		10.2	-152.57	-47.46	0.0	0.0	0.0	32.96
93	10	38.93	0.0	-7.06e-04	11.65	0.0	-137.32	-39.67	0.0	0.0	0.0	38.93
		34.95	0.0	0.0		10.2	-136.77	-38.35	0.0	0.0	0.0	34.95
93	12	2.32	0.0	-8.23e-05	-4.75	0.0	-53.44	-31.70	0.0	0.0	0.0	2.32
		-0.76	0.0	0.0		10.2	-52.89	-28.80	0.0	0.0	0.0	-0.76
93	14	-20.55	0.0	1.35e-04	-34.60	0.0	10.30	-75.83	0.0	0.0	0.0	-20.55
		-27.97	0.0	0.0		10.2	10.84	-69.89	0.0	0.0	0.0	-27.97
93	17	28.09	0.0	-5.14e-04	6.62	0.0	-113.56	-36.96	0.0	0.0	0.0	28.09
		24.42	0.0	0.0		10.2	-113.01	-35.15	0.0	0.0	0.0	24.42
93	19	-16.13	0.0	1.11e-04	-27.88	0.0	-3.70	-64.18	0.0	0.0	0.0	-16.13
		-22.40	0.0	0.0		10.2	-3.15	-58.92	0.0	0.0	0.0	-22.40
93	20	20.35	0.0	-3.76e-04	3.04	0.0	-96.59	-35.03	0.0	0.0	0.0	20.35
		16.89	0.0	0.0		10.2	-96.04	-32.87	0.0	0.0	0.0	16.89
93	21	-2.86	0.0	-3.65e-05	-7.73	0.0	-45.68	-29.24	0.0	0.0	0.0	-2.86
		-5.68	0.0	0.0		10.2	-45.13	-26.02	0.0	0.0	0.0	-5.68
94	3	-16.83	0.0	1.89e-04	-46.98	0.0	6.82	-111.04	0.0	0.0	0.0	-16.83
		-27.72	0.0	0.0		10.2	7.61	-103.01	0.0	0.0	0.0	-27.72
94	4	-16.91	0.0	1.76e-04	-44.26	0.0	23.44	-99.92	0.0	0.0	0.0	-16.91
		-26.73	0.0	0.0		10.2	24.01	-93.01	0.0	0.0	0.0	-26.73
94	9	42.96	0.0	7.02e-04	10.60	0.0	-159.88	-50.20	0.0	0.0	0.0	42.96
		37.96	0.0	0.0		10.2	-159.10	-47.93	0.0	0.0	0.0	37.96
94	10	42.88	0.0	7.15e-04	13.32	0.0	-143.27	-39.08	0.0	0.0	0.0	42.88
		38.96	0.0	0.0		10.2	-142.69	-37.94	0.0	0.0	0.0	38.96
94	12	5.64	0.0	-8.28e-05	-4.54	0.0	-55.74	-33.83	0.0	0.0	0.0	5.64
		2.34	0.0	0.0		10.2	-55.16	-30.95	0.0	0.0	0.0	2.34
94	14	-12.47	0.0	1.40e-04	-34.80	0.0	5.06	-82.25	0.0	0.0	0.0	-12.47
		-20.54	0.0	0.0		10.2	5.63	-76.30	0.0	0.0	0.0	-20.54
94	17	31.82	0.0	5.20e-04	7.85	0.0	-118.43	-37.18	0.0	0.0	0.0	31.82
		28.12	0.0	0.0		10.2	-117.85	-35.50	0.0	0.0	0.0	28.12
94	19	-9.30	0.0	1.14e-04	-28.05	0.0	-8.07	-69.63	0.0	0.0	0.0	-9.30
		-16.11	0.0	0.0		10.2	-7.49	-64.37	0.0	0.0	0.0	-16.11
94	20	23.92	0.0	3.80e-04	3.94	0.0	-100.69	-35.83	0.0	0.0	0.0	23.92
		20.38	0.0	0.0		10.2	-100.11	-33.77	0.0	0.0	0.0	20.38
94	21	0.22	0.0	-3.71e-05	-7.79	0.0	-47.46	-31.76	0.0	0.0	0.0	0.22
		-2.85	0.0	0.0		10.2	-46.88	-28.55	0.0	0.0	0.0	-2.85
95	3	-5.14	0.0	-1.93e-04	-47.18	0.0	-1.44	-118.95	0.0	0.0	0.0	-5.14
		-16.83	0.0	0.0		10.2	-0.60	-110.92	0.0	0.0	0.0	-16.83
95	4	-6.39	0.0	-1.80e-04	-44.44	0.0	15.91	-106.85	0.0	0.0	0.0	-6.39
		-16.91	0.0	0.0		10.2	16.53	-99.94	0.0	0.0	0.0	-16.91
95	9	47.91	0.0	-7.12e-04	12.33	0.0	-166.73	-49.67	0.0	0.0	0.0	47.91
		42.96	0.0	0.0		10.2	-165.89	-47.59	0.0	0.0	0.0	42.96
95	10	46.66	0.0	-7.25e-04	15.07	0.0	-149.39	-37.57	0.0	0.0	0.0	46.66
		42.88	0.0	0.0		10.2	-148.76	-36.61	0.0	0.0	0.0	42.88
95	12	9.16	0.0	-8.41e-05	-4.31	0.0	-58.34	-36.06	0.0	0.0	0.0	9.16
		5.64	0.0	0.0		10.2	-57.72	-33.23	0.0	0.0	0.0	5.64
95	14	-3.81	0.0	-1.43e-04	-34.95	0.0	-1.07	-88.11	0.0	0.0	0.0	-3.81
		-12.47	0.0	0.0		10.2	-0.44	-82.16	0.0	0.0	0.0	-12.47
95	17	35.49	0.0	-5.27e-04	9.13	0.0	-123.51	-36.79	0.0	0.0	0.0	35.49
		31.82	0.0	0.0		10.2	-122.88	-35.25	0.0	0.0	0.0	31.82
95	19	-1.96	0.0	-1.17e-04	-28.17	0.0	-13.19	-74.73	0.0	0.0	0.0	-1.96
		-9.30	0.0	0.0		10.2	-12.57	-69.47	0.0	0.0	0.0	-9.30
95	20	27.51	0.0	-3.86e-04	4.89	0.0	-105.02	-36.24	0.0	0.0	0.0	27.51
		23.92	0.0	0.0		10.2	-104.40	-34.29	0.0	0.0	0.0	23.92
95	21	3.57	0.0	3.71e-05	-7.83	0.0	-49.57	-34.58	0.0	0.0	0.0	3.57
		0.22	0.0	0.0		10.2	-48.94	-31.38	0.0	0.0	0.0	0.22
96	3	7.42	0.0	1.94e-04	-47.37	0.0	-10.35	-127.71	0.0	0.0	0.0	7.42
		-5.17	0.0	0.0		10.2	-9.44	-119.67	0.0	0.0	0.0	-5.17
96	4	4.93	0.0	1.82e-04	-44.61	0.0	7.79	-114.90	0.0	0.0	0.0	4.93
		-6.41	0.0	0.0		10.2	8.46	-107.99	0.0	0.0	0.0	-6.41
96	9	52.71	0.0	-7.23e-04	14.09	0.0	-173.52	-48.25	0.0	0.0	0.0	52.71
		47.89	0.0	0.0		10.2	-172.62	-46.37	0.0	0.0	0.0	47.89
96	10	50.22	0.0	-7.36e-04	16.84	0.0	-155.38	-35.45	0.0	0.0	0.0	50.22
		46.65	0.0	0.0		10.2	-154.71	-34.68	0.0	0.0	0.0	46.65
96	12	12.82	0.0	-8.63e-05	-4.07	0.0	-61.07	-37.51	0.0	0.0	0.0	12.82
		9.15	0.0	0.0		10.2	-60.40	-34.71	0.0	0.0	0.0	9.15
96	14	5.49	0.0	1.44e-04	-35.09	0.0	-7.67	-94.60	0.0	0.0	0.0	5.49
		-3.83	0.0	0.0		10.2	-7.00	-88.65	0.0	0.0	0.0	-3.83
96	17	39.04	0.0	-5.36e-04	10.43	0.0	-128.54	-35.74	0.0	0.0	0.0	39.04
		35.48	0.0	0.0		10.2	-127.86	-34.35	0.0	0.0	0.0	35.48
96	19	5.90	0.0	1.17e-04	-28.28	0.0	-18.71	-80.09	0.0	0.0	0.0	5.90

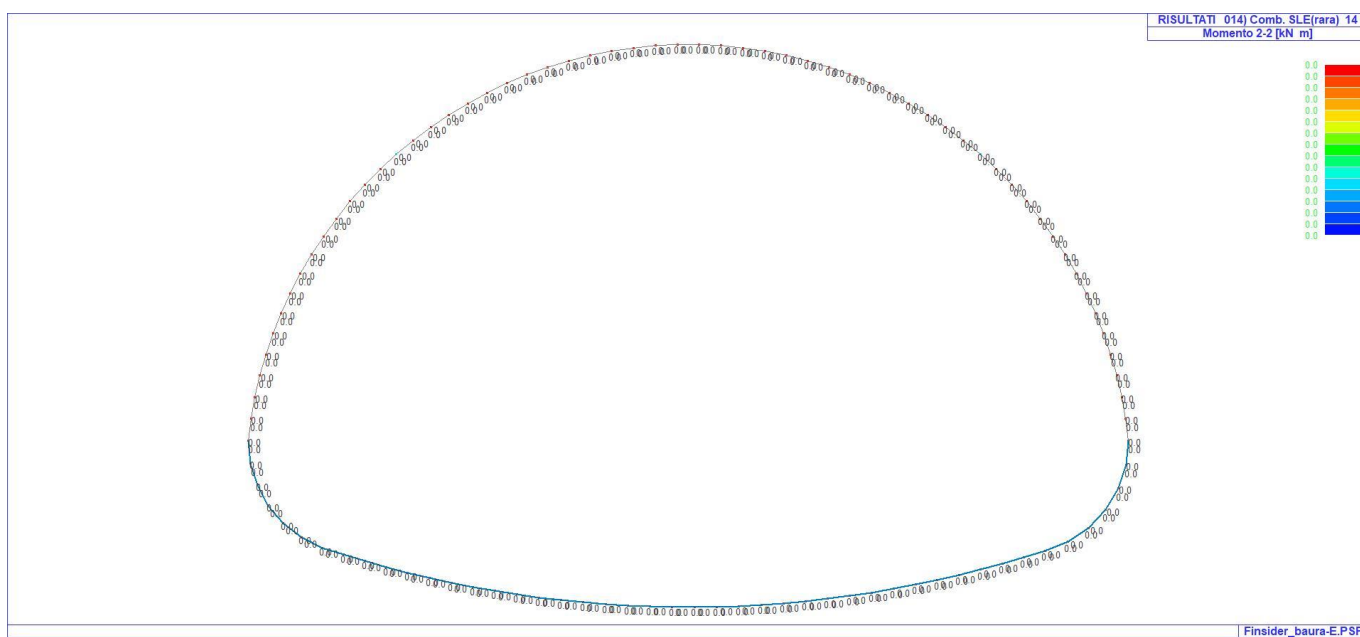
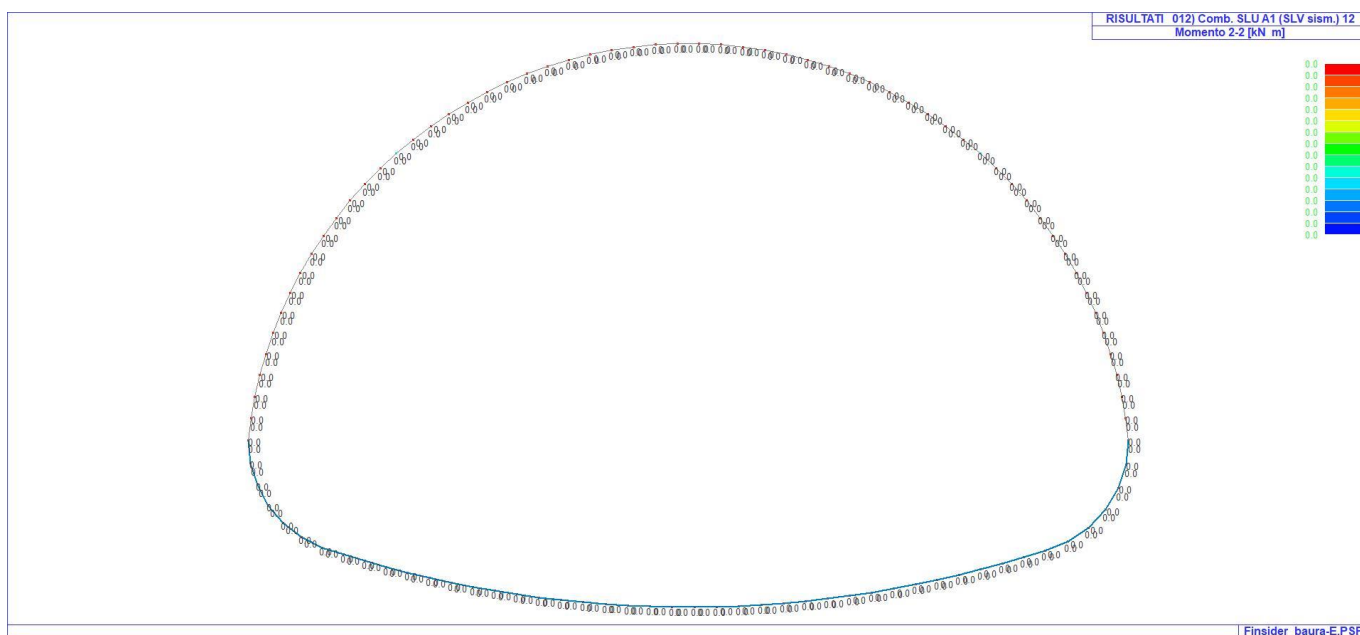
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		-1.98	0.0	0.0		10.2	-18.04	-74.83	0.0	0.0	0.0	-1.98
96	20	31.06	0.0	-3.93e-04	5.86	0.0	-109.36	-35.95	0.0	0.0	0.0	31.06
		27.49	0.0	0.0		10.2	-108.69	-34.11	0.0	0.0	0.0	27.49
96	21	7.11	0.0	-3.62e-05	-7.87	0.0	-51.84	-36.58	0.0	0.0	0.0	7.11
		3.55	0.0	0.0		10.2	-51.17	-33.39	0.0	0.0	0.0	3.55
97	3	20.61	0.0	-1.93e-04	-47.53	0.0	-19.90	-133.38	0.0	0.0	0.0	20.61
		7.45	0.0	0.0		10.2	-18.93	-125.35	0.0	0.0	0.0	7.45
97	4	16.81	0.0	-1.81e-04	-44.77	0.0	-0.91	-120.04	0.0	0.0	0.0	16.81
		4.95	0.0	0.0		10.2	-0.19	-113.12	0.0	0.0	0.0	4.95
97	9	57.30	0.0	-7.35e-04	15.86	0.0	-180.23	-45.81	0.0	0.0	0.0	57.30
		52.73	0.0	0.0		10.2	-179.26	-44.13	0.0	0.0	0.0	52.73
97	10	53.51	0.0	-7.48e-04	18.63	0.0	-161.23	-32.47	0.0	0.0	0.0	53.51
		50.23	0.0	0.0		10.2	-160.52	-31.90	0.0	0.0	0.0	50.23
97	12	16.62	0.0	-8.93e-05	-3.83	0.0	-63.91	-38.49	0.0	0.0	0.0	16.62
		12.84	0.0	0.0		10.2	-63.19	-35.73	0.0	0.0	0.0	12.84
97	14	15.27	0.0	-1.43e-04	-35.21	0.0	-14.74	-98.80	0.0	0.0	0.0	15.27
		5.52	0.0	0.0		10.2	-14.02	-92.85	0.0	0.0	0.0	5.52
97	17	42.45	0.0	-5.45e-04	11.75	0.0	-133.50	-33.93	0.0	0.0	0.0	42.45
		39.06	0.0	0.0		10.2	-132.78	-32.69	0.0	0.0	0.0	39.06
97	19	14.16	0.0	-1.16e-04	-28.38	0.0	-24.62	-83.62	0.0	0.0	0.0	14.16
		5.92	0.0	0.0		10.2	-23.90	-78.37	0.0	0.0	0.0	5.92
97	20	34.55	0.0	-4.00e-04	6.84	0.0	-113.69	-34.97	0.0	0.0	0.0	34.55
		31.08	0.0	0.0		10.2	-112.98	-33.24	0.0	0.0	0.0	31.08
97	21	10.85	0.0	-3.45e-05	-7.90	0.0	-54.27	-38.10	0.0	0.0	0.0	10.85
		7.14	0.0	0.0		10.2	-53.55	-34.92	0.0	0.0	0.0	7.14
98	2	14.84	0.0	-3.20e-05	-7.93	0.0	-56.85	-40.31	0.0	0.0	0.0	14.84
		10.90	0.0	0.0		10.2	-56.09	-37.14	0.0	0.0	0.0	10.90
98	3	34.71	0.0	-1.88e-04	-47.67	0.0	-30.09	-141.48	0.0	0.0	0.0	34.71
		20.72	0.0	0.0		10.2	-29.06	-133.45	0.0	0.0	0.0	20.72
98	4	29.52	0.0	-1.77e-04	-44.90	0.0	-10.19	-127.37	0.0	0.0	0.0	29.52
		16.91	0.0	0.0		10.2	-9.43	-120.46	0.0	0.0	0.0	16.91
98	9	61.75	0.0	-7.49e-04	17.67	0.0	-186.82	-43.94	0.0	0.0	0.0	61.75
		57.35	0.0	0.0		10.2	-185.80	-42.46	0.0	0.0	0.0	57.35
98	10	56.56	0.0	-7.60e-04	20.44	0.0	-166.93	-29.84	0.0	0.0	0.0	56.56
		53.54	0.0	0.0		10.2	-166.16	-29.47	0.0	0.0	0.0	53.54
98	12	20.61	0.0	-9.33e-05	-3.58	0.0	-66.86	-40.03	0.0	0.0	0.0	20.61
		16.67	0.0	0.0		10.2	-66.09	-37.31	0.0	0.0	0.0	16.67
98	13	14.84	0.0	-3.20e-05	-7.93	0.0	-56.85	-40.31	0.0	0.0	0.0	14.84
		10.90	0.0	0.0		10.2	-56.09	-37.14	0.0	0.0	0.0	10.90
98	14	25.71	0.0	-1.39e-04	-35.31	0.0	-22.29	-104.80	0.0	0.0	0.0	25.71
		15.35	0.0	0.0		10.2	-21.52	-98.85	0.0	0.0	0.0	15.35
98	17	45.74	0.0	-5.55e-04	13.09	0.0	-138.39	-32.55	0.0	0.0	0.0	45.74
		42.48	0.0	0.0		10.2	-137.63	-31.45	0.0	0.0	0.0	42.48
98	18	14.84	0.0	-3.20e-05	-7.93	0.0	-56.85	-40.31	0.0	0.0	0.0	14.84
		10.90	0.0	0.0		10.2	-56.09	-37.14	0.0	0.0	0.0	10.90
98	19	23.00	0.0	-1.12e-04	-28.47	0.0	-30.93	-88.68	0.0	0.0	0.0	23.00
		14.24	0.0	0.0		10.2	-30.17	-83.43	0.0	0.0	0.0	14.24
98	20	38.02	0.0	-4.08e-04	7.83	0.0	-118.00	-34.49	0.0	0.0	0.0	38.02
		34.59	0.0	0.0		10.2	-117.24	-32.87	0.0	0.0	0.0	34.59
98	21	14.84	0.0	-3.20e-05	-7.93	0.0	-56.85	-40.31	0.0	0.0	0.0	14.84
		10.90	0.0	0.0		10.2	-56.09	-37.14	0.0	0.0	0.0	10.90
99	2	18.38	0.0	-2.95e-05	-7.55	0.0	-64.87	-34.66	0.0	0.0	0.0	18.38
		14.88	0.0	0.0		10.6	-63.72	-31.56	0.0	0.0	0.0	14.88
99	4	43.10	0.0	-1.76e-04	-42.76	0.0	-38.38	-131.85	0.0	0.0	0.0	43.10
		29.53	0.0	0.0		10.6	-37.23	-125.03	0.0	0.0	0.0	29.53
99	9	63.42	0.0	-7.93e-04	20.63	0.0	-196.93	-15.50	0.0	0.0	0.0	63.42
		61.84	0.0	0.0		10.6	-195.38	-14.46	0.0	0.0	0.0	61.84
99	12	23.92	0.0	-1.02e-04	-2.88	0.0	-74.89	-32.25	0.0	0.0	0.0	23.92
		20.65	0.0	0.0		10.6	-73.74	-29.65	0.0	0.0	0.0	20.65
99	13	18.38	0.0	-2.95e-05	-7.55	0.0	-64.87	-34.66	0.0	0.0	0.0	18.38
		14.88	0.0	0.0		10.6	-63.72	-31.56	0.0	0.0	0.0	14.88
99	14	36.69	0.0	-1.38e-04	-33.63	0.0	-45.25	-106.65	0.0	0.0	0.0	36.69
		25.73	0.0	0.0		10.6	-44.10	-100.80	0.0	0.0	0.0	25.73
99	17	46.98	0.0	-5.88e-04	15.28	0.0	-145.87	-11.48	0.0	0.0	0.0	46.98
		45.81	0.0	0.0		10.6	-144.72	-10.71	0.0	0.0	0.0	45.81
99	18	18.38	0.0	-2.95e-05	-7.55	0.0	-64.87	-34.66	0.0	0.0	0.0	18.38
		14.88	0.0	0.0		10.6	-63.72	-31.56	0.0	0.0	0.0	14.88
99	19	32.11	0.0	-1.11e-04	-27.11	0.0	-50.15	-88.66	0.0	0.0	0.0	32.11
		23.02	0.0	0.0		10.6	-49.00	-83.49	0.0	0.0	0.0	23.02
99	20	39.83	0.0	-4.33e-04	9.58	0.0	-125.62	-17.27	0.0	0.0	0.0	39.83
		38.07	0.0	0.0		10.6	-124.47	-15.92	0.0	0.0	0.0	38.07
99	21	18.38	0.0	-2.95e-05	-7.55	0.0	-64.87	-34.66	0.0	0.0	0.0	18.38
		14.88	0.0	0.0		10.6	-63.72	-31.56	0.0	0.0	0.0	14.88

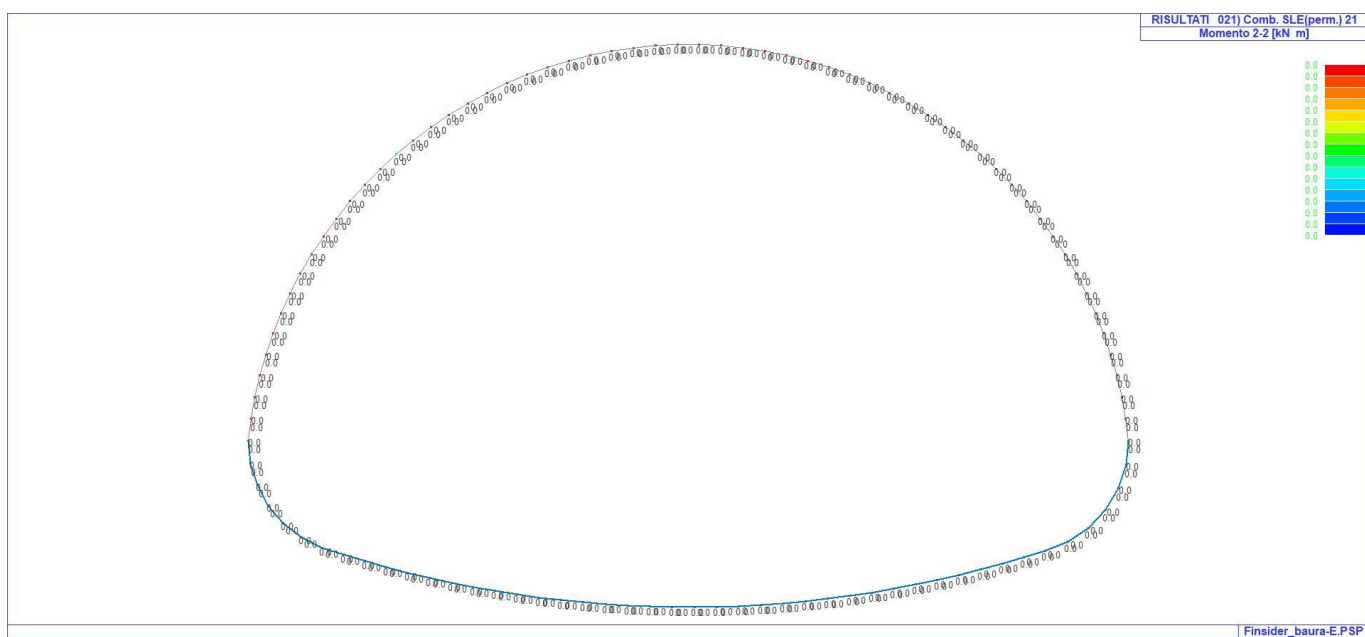
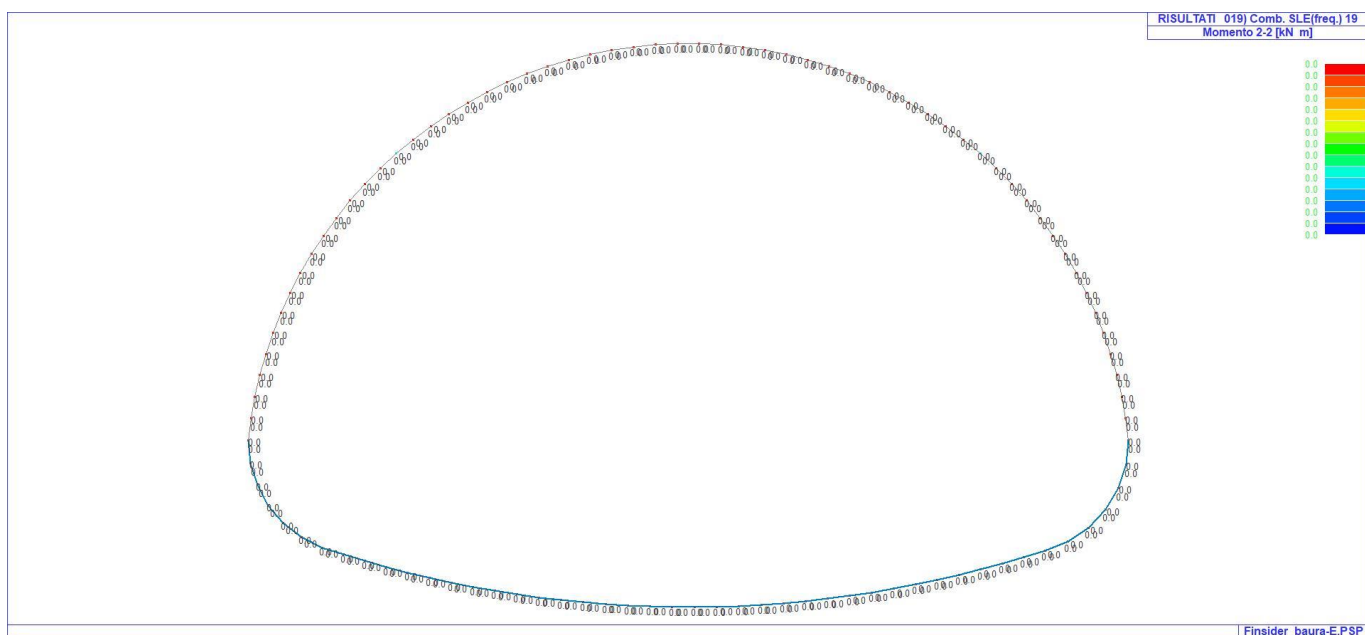


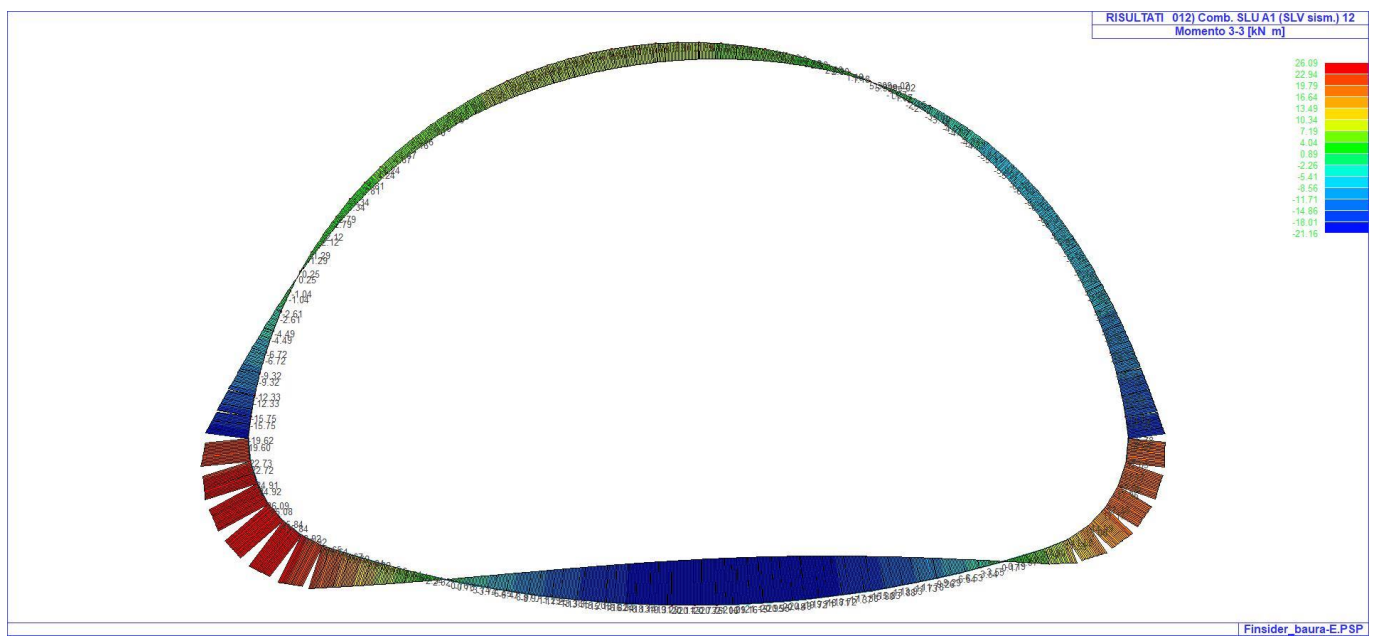
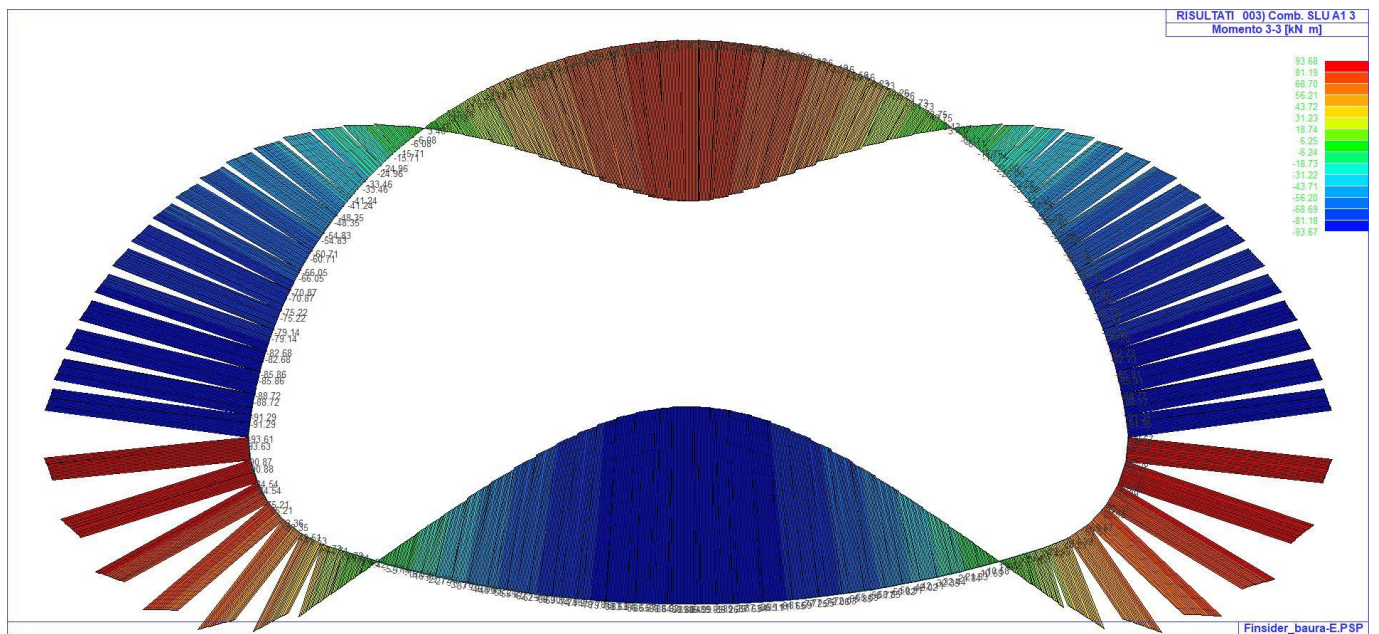
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
100	2	20.76	0.0	2.48e-05	-6.74	0.0	-74.21	-23.90	0.0	0.0	0.0	20.76
		18.38	0.0	0.0		10.6	-72.62	-21.15	0.0	0.0	0.0	18.38
100	3	63.35	0.0	1.74e-04	-40.59	0.0	-103.27	-134.53	0.0	0.0	0.0	63.35
		49.51	0.0	0.0		10.6	-101.12	-127.51	0.0	0.0	0.0	49.51
100	9	63.44	0.0	8.09e-04	23.37	0.0	-200.82	22.28	0.0	0.0	0.0	61.07
		61.07	0.0	0.0		10.6	-198.67	22.65	0.0	0.0	0.0	63.44
100	12	25.84	0.0	1.08e-04	-1.89	0.0	-83.34	-19.22	0.0	0.0	0.0	25.84
		23.92	0.0	0.0		10.6	-81.75	-16.99	0.0	0.0	0.0	23.92
100	13	20.76	0.0	2.48e-05	-6.74	0.0	-74.21	-23.90	0.0	0.0	0.0	20.76
		18.38	0.0	0.0		10.6	-72.62	-21.15	0.0	0.0	0.0	18.38
100	14	46.93	0.0	1.29e-04	-30.06	0.0	-76.49	-99.65	0.0	0.0	0.0	46.93
		36.67	0.0	0.0		10.6	-74.90	-94.45	0.0	0.0	0.0	36.67
100	17	47.00	0.0	5.99e-04	17.31	0.0	-148.75	16.50	0.0	0.0	0.0	45.24
		45.24	0.0	0.0		10.6	-147.16	16.78	0.0	0.0	0.0	47.00
100	18	20.76	0.0	2.48e-05	-6.74	0.0	-74.21	-23.90	0.0	0.0	0.0	20.76
		18.38	0.0	0.0		10.6	-72.62	-21.15	0.0	0.0	0.0	18.38
100	19	40.38	0.0	1.03e-04	-24.23	0.0	-75.92	-80.71	0.0	0.0	0.0	40.38
		32.10	0.0	0.0		10.6	-74.33	-76.13	0.0	0.0	0.0	32.10
100	20	39.84	0.0	4.43e-04	11.30	0.0	-130.12	6.40	0.0	0.0	0.0	39.12
		39.12	0.0	0.0		10.6	-128.53	7.29	0.0	0.0	0.0	39.84
100	21	20.76	0.0	2.48e-05	-6.74	0.0	-74.21	-23.90	0.0	0.0	0.0	20.76
		18.38	0.0	0.0		10.6	-72.62	-21.15	0.0	0.0	0.0	18.38
101	2	21.72	0.0	1.96e-05	-5.64	0.0	-82.16	-10.15	0.0	0.0	0.0	21.72
		20.77	0.0	0.0		10.6	-80.20	-7.88	0.0	0.0	0.0	20.77
101	3	75.21	0.0	1.58e-04	-34.10	0.0	-147.20	-115.03	0.0	0.0	0.0	75.21
		63.36	0.0	0.0		10.6	-144.54	-109.18	0.0	0.0	0.0	63.36
101	9	61.03	0.0	-8.25e-04	25.23	0.0	-194.97	63.22	0.0	0.0	0.0	54.36
		54.36	0.0	0.0		10.6	-192.31	62.91	0.0	0.0	0.0	61.03
101	12	26.08	0.0	1.15e-04	-0.81	0.0	-89.44	-3.16	0.0	0.0	0.0	26.08
		25.84	0.0	0.0		10.6	-87.47	-1.41	0.0	0.0	0.0	25.84
101	13	21.72	0.0	1.96e-05	-5.64	0.0	-82.16	-10.15	0.0	0.0	0.0	21.72
		20.77	0.0	0.0		10.6	-80.20	-7.88	0.0	0.0	0.0	20.77
101	14	55.71	0.0	1.17e-04	-25.26	0.0	-109.03	-85.20	0.0	0.0	0.0	55.71
		46.94	0.0	0.0		10.6	-107.07	-80.87	0.0	0.0	0.0	46.94
101	17	45.20	0.0	6.11e-04	18.69	0.0	-144.42	46.83	0.0	0.0	0.0	40.27
		40.27	0.0	0.0		10.6	-142.45	46.60	0.0	0.0	0.0	45.20
101	18	21.72	0.0	1.96e-05	-5.64	0.0	-82.16	-10.15	0.0	0.0	0.0	21.72
		20.77	0.0	0.0		10.6	-80.20	-7.88	0.0	0.0	0.0	20.77
101	19	47.21	0.0	9.24e-05	-20.35	0.0	-102.32	-66.44	0.0	0.0	0.0	47.21
		40.39	0.0	0.0		10.6	-100.35	-62.62	0.0	0.0	0.0	40.39
101	20	39.09	0.0	4.53e-04	12.61	0.0	-128.85	32.58	0.0	0.0	0.0	35.63
		35.63	0.0	0.0		10.6	-126.89	32.98	0.0	0.0	0.0	39.09
101	21	21.72	0.0	1.96e-05	-5.64	0.0	-82.16	-10.15	0.0	0.0	0.0	21.72
		20.77	0.0	0.0		10.6	-80.20	-7.88	0.0	0.0	0.0	20.77
102	2	21.73	0.0	1.41e-05	-4.31	0.0	-81.09	-1.27	0.0	0.0	0.0	21.45
		21.44	0.0	0.0		10.6	-85.86	6.46	0.0	0.0	0.0	21.73
102	3	84.54	0.0	-1.38e-04	-26.19	0.0	-180.63	-94.64	0.0	0.0	0.0	84.54
		75.21	0.0	0.0		10.6	-187.07	-82.07	0.0	0.0	0.0	75.21
102	12	26.09	0.0	-1.21e-04	0.56	0.0	-85.63	7.47	0.0	0.0	0.0	24.92
		24.92	0.0	0.0		10.6	-90.40	14.70	0.0	0.0	0.0	26.09
102	13	21.73	0.0	1.41e-05	-4.31	0.0	-81.09	-1.27	0.0	0.0	0.0	21.45
		21.44	0.0	0.0		10.6	-85.86	6.46	0.0	0.0	0.0	21.73
102	14	62.63	0.0	-1.03e-04	-19.40	0.0	-133.80	-70.10	0.0	0.0	0.0	62.63
		55.71	0.0	0.0		10.6	-138.57	-60.79	0.0	0.0	0.0	55.71
102	18	21.73	0.0	1.41e-05	-4.31	0.0	-81.09	-1.27	0.0	0.0	0.0	21.45
		21.44	0.0	0.0		10.6	-85.86	6.46	0.0	0.0	0.0	21.73
102	19	52.33	0.0	-8.05e-05	-15.62	0.0	-120.62	-52.89	0.0	0.0	0.0	52.33
		47.21	0.0	0.0		10.6	-125.39	-43.98	0.0	0.0	0.0	47.21
102	21	21.73	0.0	1.41e-05	-4.31	0.0	-81.09	-1.27	0.0	0.0	0.0	21.45
		21.44	0.0	0.0		10.6	-85.86	6.46	0.0	0.0	0.0	21.73
103	2	21.45	0.0	8.72e-06	-2.79	0.0	-80.22	7.39	0.0	0.0	0.0	20.24
		20.24	0.0	0.0		10.6	-83.38	15.58	0.0	0.0	0.0	21.45
103	3	90.88	0.0	-1.17e-04	-17.17	0.0	-213.86	-66.18	0.0	0.0	0.0	90.88
		84.54	0.0	0.0		10.6	-218.12	-53.72	0.0	0.0	0.0	84.54
103	12	24.91	0.0	1.27e-04	1.69	0.0	-81.27	16.87	0.0	0.0	0.0	22.72
		22.72	0.0	0.0		10.6	-84.42	24.60	0.0	0.0	0.0	24.91
103	13	21.45	0.0	8.72e-06	-2.79	0.0	-80.22	7.39	0.0	0.0	0.0	20.24
		20.24	0.0	0.0		10.6	-83.38	15.58	0.0	0.0	0.0	21.45
103	14	67.32	0.0	-8.67e-05	-12.72	0.0	-158.41	-49.02	0.0	0.0	0.0	67.32
		62.62	0.0	0.0		10.6	-161.57	-39.79	0.0	0.0	0.0	62.62
103	18	21.45	0.0	8.72e-06	-2.79	0.0	-80.22	7.39	0.0	0.0	0.0	20.24
		20.24	0.0	0.0		10.6	-83.38	15.58	0.0	0.0	0.0	21.45
103	19	55.55	0.0	-6.72e-05	-10.24	0.0	-138.87	-34.92	0.0	0.0	0.0	55.55

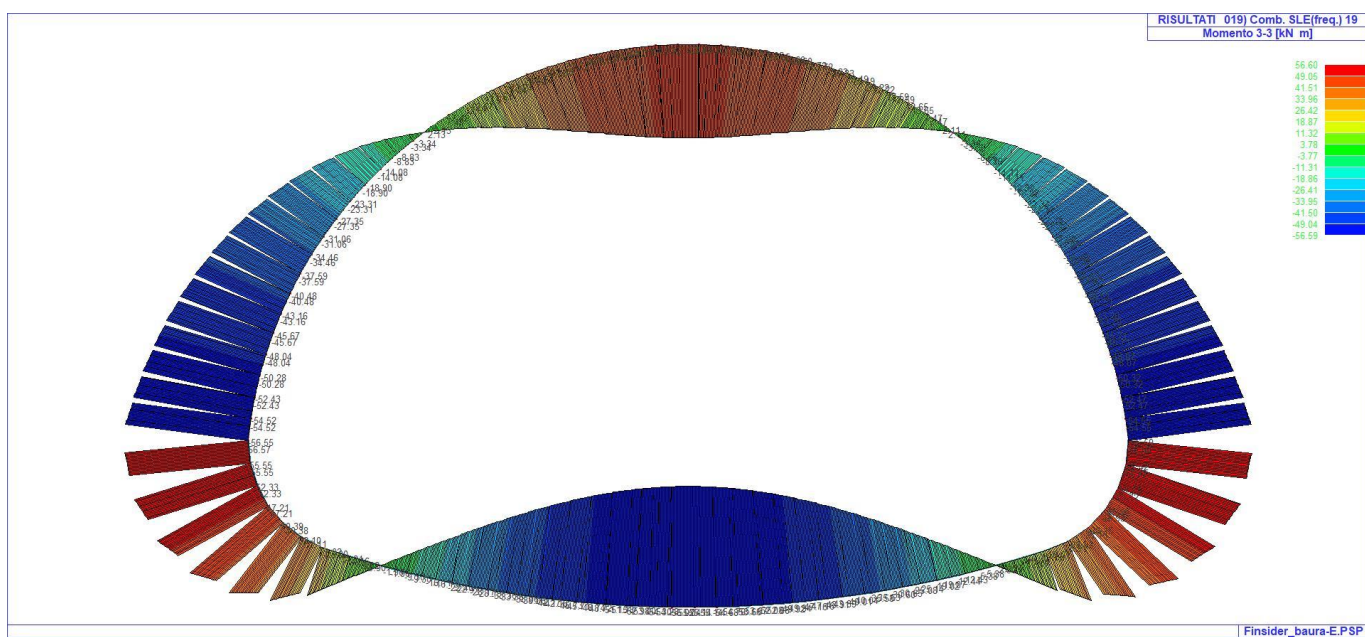
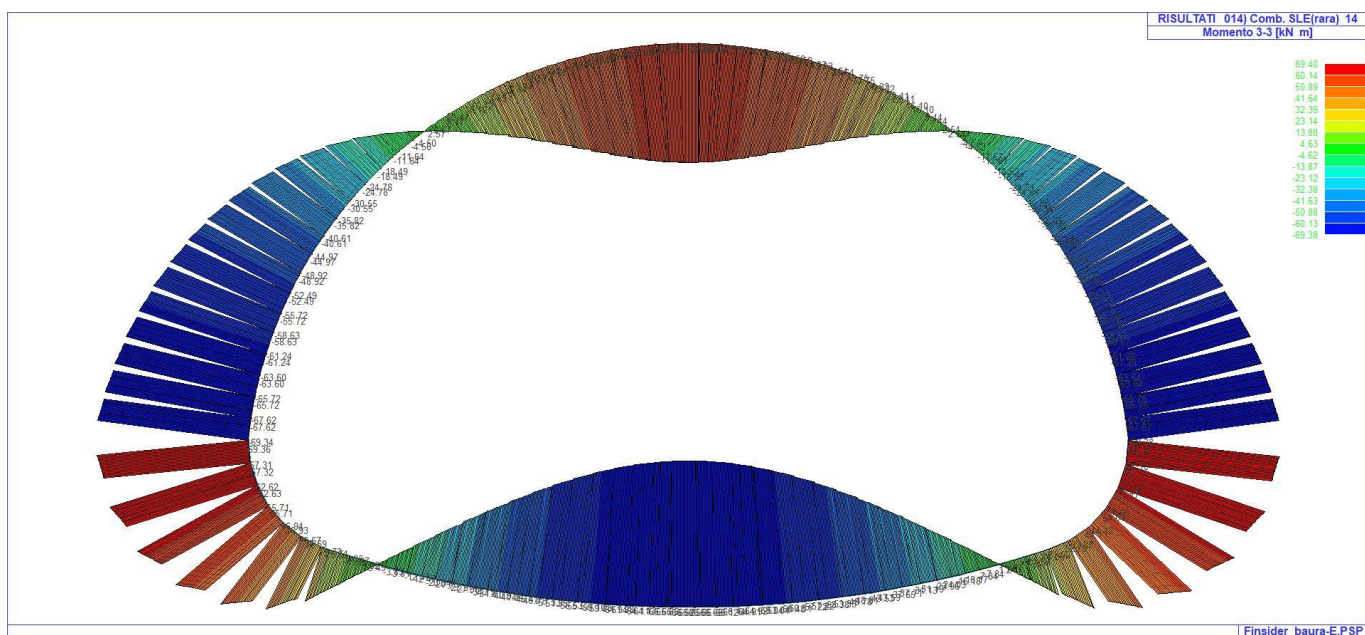
Trave f.	Cmb	M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt	Pos.	N	V 2	V 3	T	M 2	M 3
		52.33	0.0	0.0		10.6	-142.02	-25.95	0.0	0.0	0.0	52.33
103	21	21.45	0.0	8.72e-06	-2.79	0.0	-80.22	7.39	0.0	0.0	0.0	20.24
		20.24	0.0	0.0		10.6	-83.38	15.58	0.0	0.0	0.0	21.45
104	2	20.24	0.0	-3.61e-06	-1.14	0.0	-79.61	15.28	0.0	0.0	0.0	18.19
		18.19	0.0	0.0		10.6	-81.10	23.56	0.0	0.0	0.0	20.24
104	3	93.63	0.0	-9.40e-05	-7.41	0.0	-244.76	-31.99	0.0	0.0	0.0	93.63
		90.87	0.0	0.0		10.6	-246.77	-20.21	0.0	0.0	0.0	90.87
104	10	25.39	0.0	-8.59e-04	25.34	0.0	-73.38	112.85	0.0	0.0	0.0	12.83
		12.83	0.0	0.0		10.6	-75.52	124.89	0.0	0.0	0.0	25.39
104	12	22.73	0.0	-1.33e-04	2.77	0.0	-76.61	25.64	0.0	0.0	0.0	19.60
		19.60	0.0	0.0		10.6	-78.10	33.53	0.0	0.0	0.0	22.73
104	13	20.24	0.0	-3.61e-06	-1.14	0.0	-79.61	15.28	0.0	0.0	0.0	18.19
		18.19	0.0	0.0		10.6	-81.10	23.56	0.0	0.0	0.0	20.24
104	14	69.36	0.0	-6.97e-05	-5.49	0.0	-181.30	-23.70	0.0	0.0	0.0	69.36
		67.31	0.0	0.0		10.6	-182.79	-14.97	0.0	0.0	0.0	67.31
104	17	24.05	0.0	-6.35e-04	18.47	0.0	-75.00	87.55	0.0	0.0	0.0	14.22
		14.22	0.0	0.0		10.6	-76.97	98.62	0.0	0.0	0.0	24.05
104	18	20.24	0.0	-3.61e-06	-1.14	0.0	-79.61	15.28	0.0	0.0	0.0	18.19
		18.19	0.0	0.0		10.6	-81.10	23.56	0.0	0.0	0.0	20.24
104	19	56.57	0.0	-5.31e-05	-4.41	0.0	-155.88	-13.95	0.0	0.0	0.0	56.57
		55.55	0.0	0.0		10.6	-157.37	-5.34	0.0	0.0	0.0	55.55
104	20	23.10	0.0	-4.76e-04	13.57	0.0	-76.15	69.49	0.0	0.0	0.0	15.21
		15.21	0.0	0.0		10.6	-78.00	79.85	0.0	0.0	0.0	23.10
104	21	20.24	0.0	-3.61e-06	-1.14	0.0	-79.61	15.28	0.0	0.0	0.0	18.19
		18.19	0.0	0.0		10.6	-81.10	23.56	0.0	0.0	0.0	20.24
Trave f.		M3 mx/mn	M2 mx/mn	D 2 / D 3	Pt		N	V 2	V 3	T		
		-89.99	0.0	-8.78e-04	-48.00		-246.77	-141.48	0.0	0.0		
		93.68	0.0	8.80e-04	25.34		67.87	145.04	0.0	0.0		



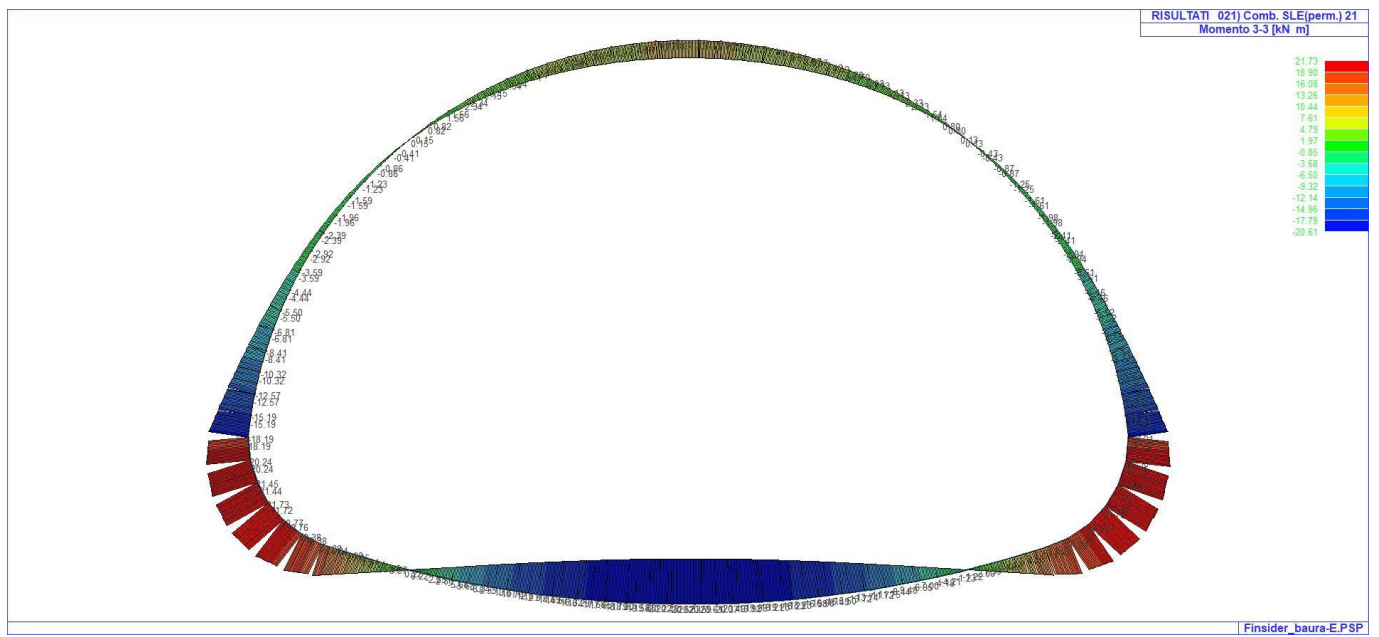












# VERIFICHE ELEMENTI TRAVE C.A.

## LEGENDA TABELLA VERIFICHE ELEMENTI TRAVE C.A.

In tabella vengono riportati per ogni elemento il numero identificativo ed il codice di verifica con le sigle **Ok** o **NV**.

Nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite (**S.L.**) vengono riportati: il rapporto  $x/d$ , le verifiche per sollecitazioni proporzionali e la verifica per compressione media con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

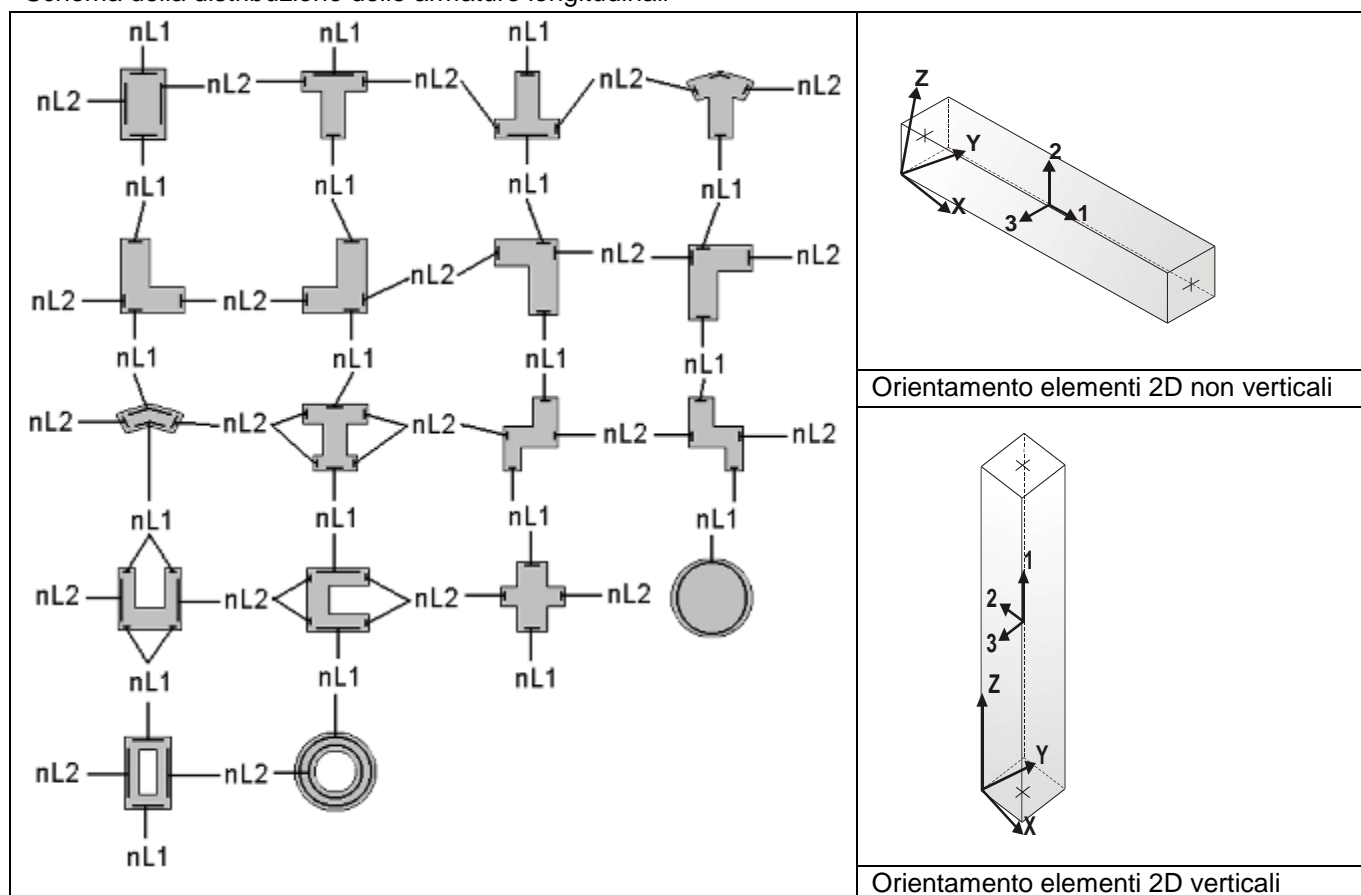
Nel caso in cui si sia proceduto alla progettazione con le tensioni ammissibili (**T.A.**) vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima compressione media nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale) con l'indicazione delle combinazioni in cui si sono attinti i rispettivi valori.

Nel caso in cui la struttura abbia comportamento dissipativo e sia prevista la progettazione con il criterio della gerarchia delle resistenze (**G.R.**) vengono riportate le verifiche di sovrarresistenza e del nodo.

Per gli elementi tipo pilastro sono riportati numero e diametro dei ferri di vertice, numero e diametro di ferri disposti lungo i lati L1 (paralleli alla base della sezione) e lungo i lati L2 (paralleli all'altezza della sezione).

Per gli elementi tipo trave sono riportati infine le quantità di armatura inferiore e superiore.

Schema della distribuzione delle armature longitudinali





## Progettazione delle fondazioni

Il D.M.14/02/2008 - par: 7.2.5 prevede:

“Per le strutture progettate sia per CD “A” sia per CD “B” il dimensionamento delle strutture di fondazione e la verifica di sicurezza del complesso fondazione-terreno devono essere eseguiti assumendo come azioni in fondazione le resistenze degli elementi strutturali soprastanti [...] si richiede tuttavia che tali azioni risultino non maggiori di quelle trasferite dagli elementi soprastanti, amplificate con un  $\gamma_{Rd}$  pari a 1,1 in CD “B” e 1,3 in CD “A” e comunque non maggiori di quelle derivanti da una analisi elastica della struttura in elevazione eseguita con un fattore di struttura  $q$  pari a 1....”

Nel contesto visualizzazione risultati e nella stampa della relazione sulle fondazioni PRO\_SAP mostra le sollecitazioni che derivano dall'analisi non incrementate sia in termini di pressioni sul terreno che in termini di sollecitazioni.

La progettazione degli elementi strutturali con proprietà fondazione è effettuata da PRO\_SAP (per travi e platee) o da PRO\_CAD Plinti (per plinti e pali di fondazione) incrementando le sollecitazioni delle combinazioni con sisma del fattore:  $\gamma_{rd} = 1.1$  in CDB  $\gamma_{rd} = 1.3$  in CDA per pali, plinti, travi e platee.

Per i bicchieri dei plinti di fondazione prefabbricati l'incremento delle sollecitazioni ha un fattore:  $\gamma_{rd} = 1.2$  in CDB  $\gamma_{rd} = 1.35$  in CDA.

N.B.: se il fattore di struttura  $q$  è =1 la progettazione viene effettuata senza nessun incremento.

Le verifiche geotecniche vengono effettuate dal modulo geotecnico incrementando automaticamente le sollecitazioni del fattore:  $\gamma_{rd} = 1.1$  in CDB  $\gamma_{rd} = 1.3$  in CDA per pali, plinti, travi e platee.

N.B.: se il fattore di struttura  $q$  è =1 le verifiche geotecniche vengono effettuate senza nessun incremento.

### Simbologia adottata nelle tabelle di verifica

Per le verifiche con il metodo agli stati limite è presente una tabella con i simboli di seguito descritti:

r. snell.	Rapporto $\lambda$ su $\lambda^*$ : valore superiore a 1 per elementi snelli, caso in cui viene effettuata la verifica con il metodo diretto dello stato di equilibrio
Verifica(verif.)	rapporto $S_d/S_u$ con sollecitazioni ultime proporzionali o a sforzo normale costante: valore minore o uguale a 1 per verifica positiva
ver.sis	rapporto $N_d/N_u$ con $N_u$ calcolato come al punto 7.4.4.2.2.1; valore minore o uguale a 1 per verifica positiva
ver.V/T	rapporto $S_d/S_u$ con sollecitazioni taglianti e torcenti proporzionali valore minore o uguale a 1 per verifica positiva
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)

Per gli elementi progettati secondo il criterio della gerarchia delle resistenze (pilastri e travi) si riporta una ulteriore tabella di seguito descritta:

M negativo i	Valore del momento resistente negativo (positivo) all'estremità iniziale i (finale f) della trave
V M-i M+f	Taglio generato dai momenti resistenti negativo i e positivo f (positivo i e negativo f)
V totale	Massimo valore assoluto ottenuto per combinazione del taglio isostatico e dei tagli concomitanti (p.to 7.4.4.1.1.)
Verif. V	Rapporto tra il taglio massimo e $V_{r1}$ (p.to 7.4.4.1.2.2);
Sovr. 2-2 i	Sovraresistenza del pilastro (come da formula 7.4.4). Rapporto tra i momenti resistenti delle travi e dei pilastri. Il valore del fattore rispettivamente per il momento 2-2 (3-3) alla base i ed alla sommità f del pilastro deve essere maggiore del $\gamma_{Rd}$ adottato
M 2-2 i	Valore del momento resistente rispettivamente per 2-2 (3-3) alla base i ed alla sommità f del pilastro (massimo momento in presenza dello sforzo normale di calcolo)
Luce per V	Luce di calcolo per la definizione del taglio (generato dai momenti resistenti)
V M2-2	Valore del taglio generato dai momenti resistenti 2-2 (3-3)

Per i nodi trave-pilastro viene riportata la seguente tabella relativa al calcolo delle armature di confinamento e alla verifica di resistenza del nodo (richiesta solo per strutture in classe di duttilità alta); le caselle vuote indicano parametri

non riportati in quanto non necessari.

Stato	Esito della verifica (come da formula 7.4.8) per resistenza a compressione del nodo (solo CDA)
I 7.4.29	Passo delle staffe di confinamento come richiesto dalla formula 7.4.29
Bj2(3)	Dimensione del nodo per il taglio in direzione 2 (3)
Hjc2(2)	Distanza tra le giaciture di armatura del pilastro per il taglio in direzione 2 (3)
V. 7.4.8	Rapporto tra il taglio Vjbd e il taglio resistente come da formula 7.4.8 (solo CDA)
I 7.4.10	Passo delle staffe valutato in funzione della formula 7.4.10 (solo CDA)

Per le verifiche con il metodo delle tensioni ammissibili è presente una tabella con i simboli di seguito descritti:

M_P X Y	Numero della pilastrata e posizione in pianta
M_T Z P P	Numero della travata, quota media pilastrata iniziale e finale (nodo in assenza di pilastrata)
Pilas. o Trave	numero identificativo dell'elemento
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m); nella terza riga viene riportato il valore delle snellezze in direzione 2-2 e 3-3
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Quota	Ascissa del punto di verifica
%Af	Percentuale di area di armatura rispetto a quella di calcestruzzo
Armat. long.	Numero e diametro dei ferri di armatura longitudinale: ferri di vertice + ferri di lato
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup	Area di armatura longitudinale posta all'estradosso della trave
Sc max	Massima tensione di compressione del calcestruzzo
Sc med	Massima tensione media di compressione del calcestruzzo
Sf max	Tensione massima nell'acciaio
staffe	Vengono riportati i dati del tratto di staffatura in cui cade la sezione di verifica; in particolare: numero dei bracci, diametro, passo, lunghezza tratto
Tau max	Tensione massima tangenziale nel cls
Rif. comb	Combinazioni in cui si generano i seguenti valori di tensione: Sc max, Sc med, Sf max, Tau max
AfV	area dell'armatura atta ad assorbire le azioni di taglio
AfT	area dell'armatura atta ad assorbire le azioni di torsione
Scorr. P	Scorrimento dei piegati
Af long.	Area del ferro longitudinale aggiuntivo per assorbire la torsione

Trave	Note	Pos.	%Af	Af inf.	Af. sup	Af long.	M_T = 1	Z=317.3	N=2	N=104	Staffe	Rif. cmb	
		cm					x/d	V N/M	V V/T cls	V V/T acc	L=cm		
1	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.91	0.22	0.16	2d12/5 L=10	3,9,9	
	s=1,m=4	10.0	0.40	8.0	10.1	0.0	0.16	0.88	0.19	0.14	2d12/5 L=10	3,9,9	
2	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.89	0.20	0.15	2d12/5 L=10	3,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.99	0.17	0.12	2d12/5 L=10	3,9,9	
3	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.86	0.17	0.13	2d12/5 L=10	3,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.96	0.15	0.11	2d12/5 L=10	3,9,9	
4	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.96	0.15	0.11	2d12/5 L=10	3,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.92	0.12	0.09	2d12/5 L=10	3,9,9	
5	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.92	0.13	0.10	2d12/5 L=10	3,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.88	0.10	0.23	2d12/15 L=0	3,9,9	
6	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.89	0.11	0.24	2d12/15 L=10	3,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.84	0.08	0.18	2d12/15 L=10	4,9,9	
7	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.84	0.08	0.19	2d12/15 L=10	4,9,9	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.79	0.06	0.14	2d12/15 L=10	4,3,3	
8	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.80	0.08	0.19	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.74	0.07	0.16	2d12/15 L=10	4,3,3	
9	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.74	0.09	0.20	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.68	0.08	0.18	2d12/15 L=10	4,3,3	
10	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.69	0.10	0.22	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.66	0.08	0.20	2d12/15 L=10	10,3,3	
11	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.66	0.11	0.24	2d12/15 L=10	10,3,3	

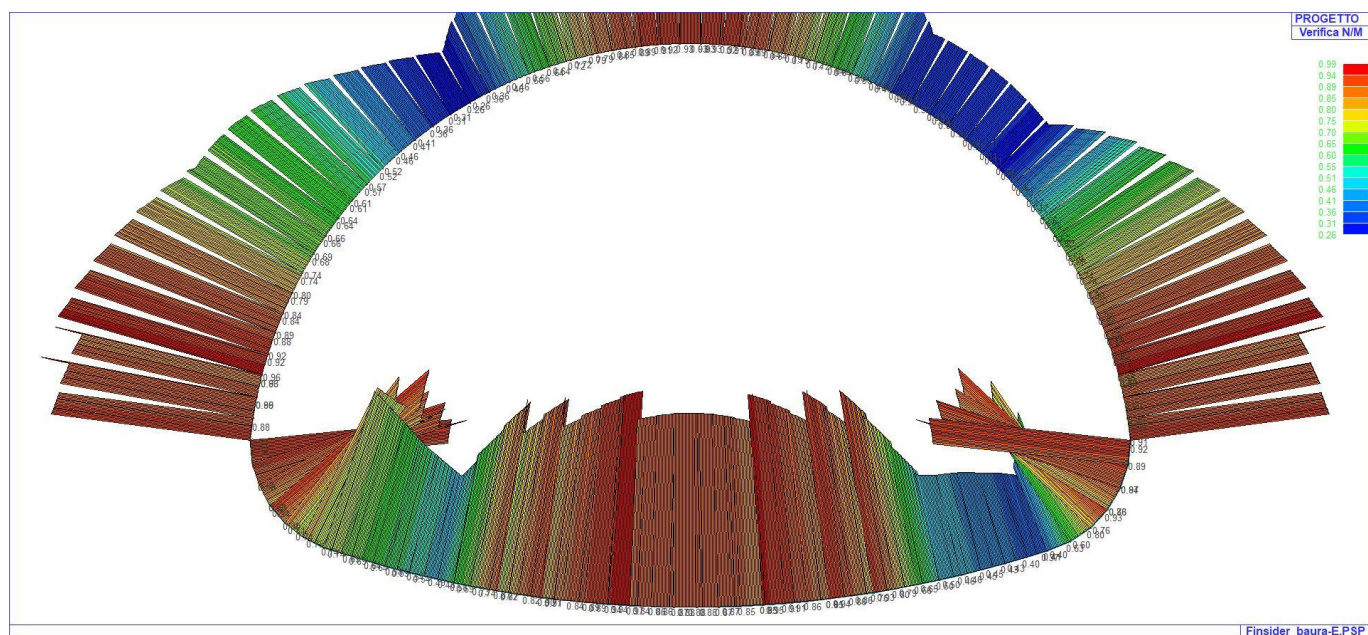
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.64	0.09	0.22	2d12/15 L=10	10,3,3	
12	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.64	0.11	0.27	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.61	0.10	0.24	2d12/15 L=10	10,3,3	
13	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.61	0.12	0.29	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.57	0.11	0.27	2d12/15 L=10	10,4,3	
14	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.57	0.14	0.31	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.52	0.13	0.29	2d12/15 L=10	10,3,3	
15	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.52	0.15	0.34	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.46	0.14	0.32	2d12/15 L=10	10,3,3	
16	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.46	0.16	0.37	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.41	0.14	0.32	2d12/15 L=10	10,3,3	
17	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.41	0.16	0.36	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.36	0.14	0.32	2d12/15 L=10	10,3,3	
18	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.36	0.16	0.36	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.31	0.13	0.31	2d12/15 L=10	10,3,3	
19	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.31	0.15	0.35	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.26	0.13	0.29	2d12/15 L=10	9,3,3	
20	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.26	0.14	0.33	2d12/15 L=10	9,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.36	0.12	0.28	2d12/15 L=10	3,3,3	
21	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.36	0.14	0.31	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.46	0.11	0.26	2d12/15 L=10	3,3,3	
22	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.46	0.13	0.29	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.56	0.10	0.23	2d12/15 L=10	3,3,3	
23	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.56	0.12	0.26	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.64	0.09	0.21	2d12/15 L=10	3,3,3	
24	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.64	0.10	0.24	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.72	0.08	0.18	2d12/15 L=10	3,3,3	
25	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.72	0.09	0.21	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.79	0.06	0.15	2d12/15 L=10	3,3,3	
26	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.79	0.08	0.17	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.84	0.05	0.11	2d12/15 L=10	3,3,3	
27	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.85	0.06	0.14	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.89	0.04	0.10	2d12/15 L=10	3,10,10	
28	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.89	0.05	0.11	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.91	0.04	0.10	2d12/15 L=10	3,10,10	
29	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.92	0.05	0.10	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.93	0.04	0.10	2d12/15 L=10	3,9,9	
30	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.93	0.04	0.10	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.93	0.04	0.10	2d12/15 L=10	3,12,12	
31	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.93	0.04	0.09	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.92	0.05	0.10	2d12/15 L=10	3,12,12	
32	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.91	0.04	0.09	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.89	0.05	0.11	2d12/15 L=10	3,12,12	
33	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.89	0.04	0.09	2d12/15 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.84	0.06	0.14	2d12/15 L=10	3,3,3	
34	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.84	0.05	0.11	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.79	0.08	0.17	2d12/15 L=10	3,3,3	
35	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.79	0.06	0.15	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.72	0.09	0.21	2d12/15 L=10	3,3,3	
36	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.72	0.08	0.18	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.64	0.10	0.24	2d12/15 L=10	3,3,3	
37	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.64	0.09	0.21	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.56	0.12	0.26	2d12/15 L=10	3,3,3	
38	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.56	0.10	0.23	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.46	0.13	0.29	2d12/15 L=10	3,3,3	
39	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.46	0.11	0.26	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.36	0.14	0.31	2d12/15 L=10	3,3,3	
40	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.36	0.12	0.28	2d12/15 L=10	3,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.32	0.14	0.33	2d12/15 L=10	10,3,3	
41	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.32	0.13	0.29	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.33	0.15	0.35	2d12/15 L=10	10,3,3	
42	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.33	0.13	0.31	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.33	0.16	0.36	2d12/15 L=10	10,3,3	
43	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.33	0.14	0.32	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.32	0.16	0.36	2d12/15 L=10	10,3,3	
44	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.32	0.14	0.32	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.31	0.16	0.37	2d12/15 L=10	10,3,3	
45	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.31	0.14	0.32	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.30	0.15	0.34	2d12/15 L=10	10,3,3	
46	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.30	0.13	0.29	2d12/15 L=10	10,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.38	0.14	0.31	2d12/15 L=10	4,3,3	
47	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.38	0.11	0.27	2d12/15 L=10	4,4,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.47	0.12	0.29	2d12/15 L=10	4,3,3	
48	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.47	0.10	0.24	2d12/15 L=10	4,3,3	

	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.55	0.11	0.27	2d12/15 L=10	4,3,3	
49	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.55	0.09	0.22	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.62	0.11	0.24	2d12/15 L=10	4,3,3	
50	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.62	0.08	0.20	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.69	0.10	0.22	2d12/15 L=10	4,3,3	
51	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.68	0.08	0.18	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.74	0.09	0.20	2d12/15 L=10	4,3,3	
52	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.74	0.07	0.16	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.80	0.08	0.19	2d12/15 L=10	4,3,3	
53	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.80	0.06	0.14	2d12/15 L=10	4,3,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.84	0.07	0.17	2d12/15 L=10	4,3,3	
54	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.84	0.06	0.12	2d12/15 L=10	4,12,3	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.89	0.07	0.16	2d12/15 L=10	3,3,3	
55	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.88	0.06	0.13	2d12/15 L=0	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.93	0.07	0.05	2d12/5 L=10	3,12,12	
56	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.92	0.06	0.05	2d12/5 L=10	3,12,12	
	s=1,m=4	10.0	0.32	8.0	8.0	0.0	0.15	0.96	0.08	0.06	2d12/5 L=10	3,12,12	
57	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.96	0.07	0.05	2d12/5 L=10	3,12,12	
	s=1,m=4	10.0	0.40	8.0	10.1	0.0	0.16	0.86	0.08	0.06	2d12/5 L=10	3,12,12	
58	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.86	0.08	0.06	2d12/5 L=10	3,12,12	
	s=1,m=4	10.0	0.40	8.0	10.1	0.0	0.16	0.89	0.09	0.07	2d12/5 L=10	3,12,12	
59	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.89	0.08	0.06	2d12/5 L=10	3,12,12	
	s=1,m=4	10.0	0.40	8.0	10.1	0.0	0.16	0.91	0.09	0.07	2d12/5 L=10	3,12,12	
60	ok,ok	0.0	0.40	10.1	8.0	0.0	0.16	0.89	0.06	0.13	2d12/15 L=11	3,11,11	
	s=2,m=4	11.3	0.40	10.1	8.0	0.0	0.16	0.92	0.06	0.14	2d12/15 L=11	3,4,4	
61	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.97	0.10	0.22	2d12/15 L=11	3,4,4	
	s=2,m=4	11.3	0.40	10.1	8.0	0.0	0.16	0.92	0.11	0.26	2d12/15 L=11	3,4,4	
62	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.88	0.14	0.32	2d12/15 L=11	3,4,4	
	s=2,m=4	11.3	0.40	10.1	8.0	0.0	0.16	0.87	0.16	0.35	2d12/15 L=11	3,3,3	
63	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.76	0.18	0.41	2d12/15 L=11	3,3,3	
	s=2,m=4	11.3	0.32	8.0	8.0	0.0	0.15	0.93	0.19	0.44	2d12/15 L=11	3,3,3	
64	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.60	0.21	0.47	2d12/15 L=11	3,3,3	
	s=2,m=4	11.3	0.32	8.0	8.0	0.0	0.15	0.80	0.22	0.50	2d12/15 L=11	3,3,3	
65	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.40	0.22	0.49	2d12/15 L=11	3,3,3	
	s=2,m=4	11.3	0.32	8.0	8.0	0.0	0.15	0.63	0.23	0.52	2d12/15 L=11	3,3,3	
66	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.40	0.22	0.48	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.41	0.23	0.50	2d12/15 L=10	3,3,3	
67	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.43	0.20	0.44	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.40	0.21	0.47	2d12/15 L=10	10,3,3	
68	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.45	0.19	0.42	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.43	0.20	0.45	2d12/15 L=10	10,3,3	
69	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.46	0.17	0.38	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.45	0.19	0.41	2d12/15 L=10	10,3,3	
70	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.50	0.16	0.36	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.46	0.18	0.39	2d12/15 L=10	10,3,3	
71	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.65	0.15	0.33	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.50	0.16	0.36	2d12/15 L=10	3,3,3	
72	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.79	0.14	0.30	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.66	0.15	0.33	2d12/15 L=10	3,3,3	
73	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.93	0.12	0.27	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.80	0.14	0.30	2d12/15 L=10	3,3,3	
74	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.86	0.11	0.24	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.40	8.0	10.1	0.0	0.16	0.76	0.12	0.27	2d12/15 L=10	3,3,3	
75	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.94	0.09	0.20	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.40	8.0	10.1	0.0	0.16	0.86	0.11	0.23	2d12/15 L=10	3,3,3	
76	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.86	0.08	0.17	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.40	8.0	10.1	0.0	0.16	0.95	0.09	0.20	2d12/15 L=10	3,3,3	
77	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.91	0.06	0.14	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.86	0.08	0.17	2d12/15 L=10	3,3,3	
78	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.95	0.05	0.11	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.91	0.06	0.14	2d12/15 L=10	3,3,3	
79	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.85	0.05	0.11	2d12/15 L=10	3,10,10	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.95	0.05	0.10	2d12/15 L=10	3,3,3	
80	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.87	0.05	0.12	2d12/15 L=10	3,10,10	
	s=2,m=4	10.2	0.56	8.0	14.1	0.0	0.18	0.85	0.05	0.11	2d12/15 L=10	3,10,10	
81	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.88	0.06	0.13	2d12/15 L=10	3,10,10	
	s=2,m=4	10.2	0.56	8.0	14.1	0.0	0.18	0.87	0.05	0.12	2d12/15 L=10	3,10,10	
82	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.88	0.06	0.14	2d12/15 L=10	3,9,9	
	s=2,m=4	10.2	0.56	8.0	14.1	0.0	0.18	0.88	0.06	0.13	2d12/15 L=10	3,10,10	
83	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.86	0.06	0.14	2d12/15 L=10	3,9,9	
	s=2,m=4	10.2	0.56	8.0	14.1	0.0	0.18	0.87	0.06	0.12	2d12/15 L=10	3,9,9	
84	ok,ok	0.0	0.56	8.0	14.1	0.0	0.18	0.84	0.07	0.17	2d12/15 L=10	3,9,9	
	s=2,m=4	10.2	0.56	8.0	14.1	0.0	0.18	0.86	0.07	0.15	2d12/15 L=10	3,9,9	
85	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.94	0.07	0.16	2d12/15 L=10	3,9,9	

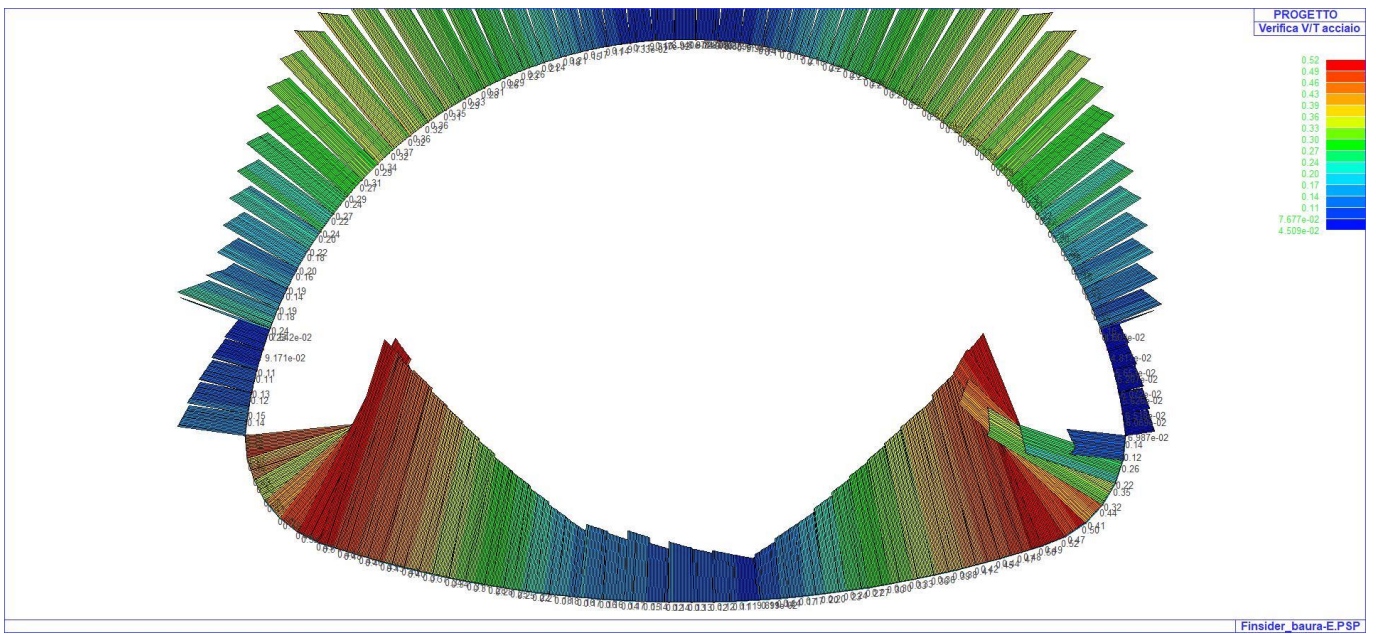
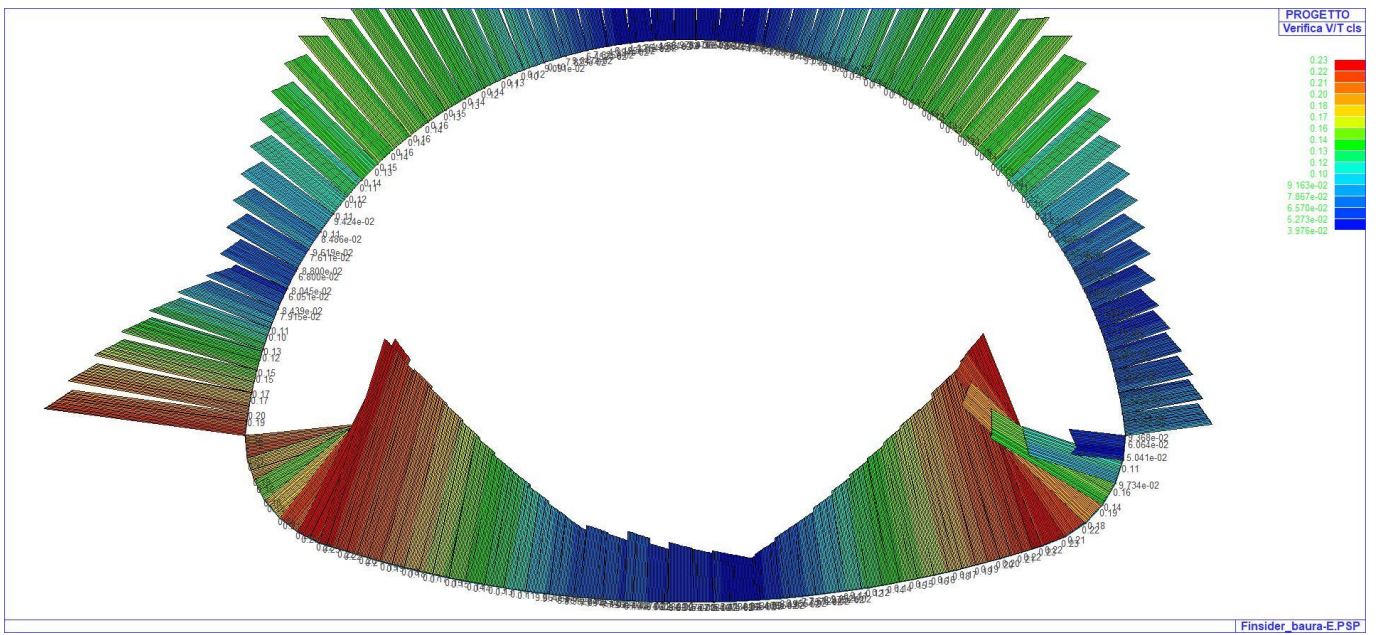
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.97	0.06	0.14	2d12/15 L=10	3,9,9	
86	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.89	0.08	0.17	2d12/15 L=10	3,9,9	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.94	0.07	0.16	2d12/15 L=10	3,9,9	
87	ok,ok	0.0	0.48	8.0	12.1	0.0	0.17	0.84	0.08	0.18	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.89	0.07	0.16	2d12/15 L=10	3,3,9	
88	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.91	0.10	0.21	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.48	8.0	12.1	0.0	0.17	0.83	0.08	0.18	2d12/15 L=10	3,3,3	
89	ok,ok	0.0	0.40	8.0	10.1	0.0	0.16	0.82	0.11	0.25	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.40	8.0	10.1	0.0	0.16	0.90	0.10	0.22	2d12/15 L=10	3,3,3	
90	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.87	0.13	0.28	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.40	8.0	10.1	0.0	0.16	0.81	0.11	0.25	2d12/15 L=10	3,3,3	
91	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.74	0.14	0.31	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.87	0.13	0.28	2d12/15 L=10	3,3,3	
92	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.59	0.15	0.34	2d12/15 L=10	3,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.73	0.14	0.31	2d12/15 L=10	3,3,3	
93	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.49	0.17	0.37	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.58	0.15	0.34	2d12/15 L=10	3,3,3	
94	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.54	0.18	0.40	2d12/15 L=10	10,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.49	0.17	0.37	2d12/15 L=10	10,3,3	
95	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.59	0.19	0.43	2d12/15 L=10	9,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.54	0.18	0.40	2d12/15 L=10	10,3,3	
96	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.64	0.21	0.46	2d12/15 L=10	9,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.58	0.19	0.43	2d12/15 L=10	9,3,3	
97	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.69	0.22	0.48	2d12/15 L=10	9,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.64	0.20	0.45	2d12/15 L=10	9,3,3	
98	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.74	0.23	0.51	2d12/15 L=10	9,3,3	
	s=2,m=4	10.2	0.32	8.0	8.0	0.0	0.15	0.69	0.22	0.48	2d12/15 L=10	9,3,3	
99	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.75	0.23	0.52	2d12/15 L=11	9,3,3	
	s=2,m=4	10.6	0.32	8.0	8.0	0.0	0.15	0.74	0.22	0.49	2d12/15 L=11	9,3,3	
100	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.84	0.21	0.48	2d12/15 L=11	3,3,3	
	s=2,m=4	10.6	0.32	8.0	8.0	0.0	0.15	0.75	0.20	0.46	2d12/15 L=11	9,3,3	
101	ok,ok	0.0	0.32	8.0	8.0	0.0	0.15	0.94	0.18	0.41	2d12/15 L=11	3,3,3	
	s=2,m=4	10.6	0.32	8.0	8.0	0.0	0.15	0.80	0.17	0.39	2d12/15 L=11	3,3,3	
102	ok,ok	0.0	0.40	10.1	8.0	0.0	0.16	0.88	0.15	0.34	2d12/15 L=11	3,4,3	
	s=2,m=4	10.6	0.32	8.0	8.0	0.0	0.15	0.90	0.16	0.36	2d12/15 L=11	3,9,9	
103	ok,ok	0.0	0.40	10.1	8.0	0.0	0.16	0.92	0.17	0.38	2d12/15 L=11	3,9,9	
	s=2,m=4	10.6	0.32	8.0	8.0	0.0	0.15	0.98	0.19	0.43	2d12/15 L=11	3,9,9	
104	ok,ok	0.0	0.40	10.1	8.0	0.0	0.16	0.92	0.19	0.42	2d12/15 L=11	3,9,9	
	s=2,m=4	10.6	0.40	10.1	8.0	0.0	0.16	0.89	0.21	0.48	2d12/15 L=11	3,9,9	
Trave													
			%Af	Af inf.	Af. sup	Af long.	x/d	V N/M	V V/T cls	V V/T acc			
			0.56	10.05	14.07	0.0	0.18	0.99	0.23	0.52			

Trave	M negativo i	M positivo i	M negativo f	M positivo f	Luce per V	V M-i M+f	V M+i M-f	VEd,min	VEd,max	Vr1	As
	kN m	kN m	kN m	kN m	cm	kN	kN	kN	kN	kN	cm2
1	80.13	66.54	80.13	66.54	592.77	24.74	24.74	0.0	0.0	0.0	0.0
2	80.13	66.54	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
3	80.13	66.54	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
4	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
5	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
6	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
7	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
8	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
9	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
10	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
11	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
12	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
13	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
14	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
15	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
16	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
17	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
18	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
19	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
20	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
21	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
22	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
23	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
24	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
25	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
26	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0

Trave	M negativo i	M positivo i	M negativo f	M positivo f	Luce per V	V M-i M+f	V M+i M-f	VEd,min	VEd,max	Vr1	As
27	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
28	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
29	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
30	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
31	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
32	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
33	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
34	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
35	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
36	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
37	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
38	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
39	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
40	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
41	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
42	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
43	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
44	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
45	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
46	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
47	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
48	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
49	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
50	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
51	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
52	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
53	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
54	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
55	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
56	66.31	66.31	66.31	66.31	592.77	24.74	24.74	0.0	0.0	0.0	0.0
57	66.31	66.31	80.13	66.54	592.77	24.74	24.74	0.0	0.0	0.0	0.0
58	80.13	66.54	80.13	66.54	592.77	24.74	24.74	0.0	0.0	0.0	0.0
59	80.13	66.54	80.13	66.54	592.77	24.74	24.74	0.0	0.0	0.0	0.0
Trave	M negativo i	M positivo i	M negativo f	M positivo f		V M-i M+f	V M+i M-f	VEd,min	VEd,max	Vr1	As
								0.0			
	80.13	66.54	80.13	66.54		24.74	24.74		0.0	0.0	0.0







# STATI LIMITE D' ESERCIZIO

## LEGENDA TABELLA STATI LIMITE D' ESERCIZIO

In tabella vengono riportati i valori di interesse per il controllo degli stati limite d'esercizio.

In particolare vengono riportati, in relazione al tipo di elemento strutturale, i risultati relativi alle tre categorie di combinazione considerate:

- Combinazioni rare
- Combinazioni frequenti
- Combinazioni quasi permanenti.

I valori di interesse sono i seguenti:

<b>rRfck</b>	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni rare [normalizzato a 1]
<b>rRfyk</b>	rapporto tra la massima tensione nell'acciaio e la tensione fyk in combinazioni rare [normalizzato a 1]
<b>rPfck</b>	rapporto tra la massima compressione nel calcestruzzo e la tensione fck in combinazioni quasi permanenti [normalizzato a 1]
<b>wR</b>	apertura caratteristica delle fessure in combinazioni rare [mm]
<b>wF</b>	apertura caratteristica delle fessure in combinazioni frequenti [mm]
<b>wP</b>	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]
<b>dR</b>	massima deformazione in combinazioni rare
<b>dF</b>	massima deformazione in combinazioni frequenti
<b>dP</b>	massima deformazione in combinazioni quasi permanenti

Per ognuno dei nove valori soprariportati viene indicata (Rif.cmb) la combinazione in cui si è verificato.

In relazione al tipo di elemento strutturale i valori sono selezionati nel modo seguente:

pilastrati	<b>rRfck</b>	<b>rRfyk</b>	<b>rPfck</b>	per sezioni significative
travi	<b>rRfck</b>	<b>rRfyk</b>	<b>rPfck</b>	per sezioni significative
	<b>wR</b>	<b>wF</b>	<b>wP</b>	per sezioni significative
	<b>dR</b>	<b>dF</b>	<b>dP</b>	massimi in campata
setti e gusci	<b>rRfck</b>	<b>rRfyk</b>	<b>rPfck</b>	massimi nei nodi dell'elemento
	<b>wR</b>	<b>wF</b>	<b>wP</b>	massimi nei nodi dell'elemento

Si precisa che i valori di massima deformazione per travi sono riferiti al piano verticale (piano locale 1-2 con momenti flettenti 3-3).



Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	cm					mm	mm	mm		cm	cm	cm	
1	0.0	0.53	0.77	0.19	14,14,21	0.24	0.21	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.52	0.74	0.15	14,14,21	0.22	0.19	0.0	14,19,0				
2	0.0	0.52	0.74	0.16	14,14,21	0.22	0.19	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.54	0.88	0.13	14,14,21	0.30	0.25	0.0	14,19,0				
3	0.0	0.51	0.72	0.13	14,14,21	0.21	0.18	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.53	0.84	0.11	14,14,21	0.28	0.23	0.0	14,19,0				
4	0.0	0.53	0.84	0.11	14,14,21	0.28	0.23	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.51	0.80	0.09	14,14,21	0.27	0.21	0.0	14,19,0				
5	0.0	0.51	0.80	0.09	14,14,21	0.27	0.21	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.49	0.75	0.07	14,14,21	0.25	0.19	0.0	14,19,0				
6	0.0	0.49	0.75	0.07	14,14,21	0.25	0.19	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.46	0.69	0.05	14,14,21	0.23	0.17	0.0	14,19,0				
7	0.0	0.46	0.70	0.05	14,14,21	0.23	0.17	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.43	0.64	0.05	14,14,21	0.21	0.15	0.0	14,19,0				
8	0.0	0.43	0.64	0.05	14,14,21	0.21	0.15	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.40	0.57	0.04	14,14,21	0.19	0.13	0.0	14,19,0				
9	0.0	0.40	0.57	0.04	14,14,21	0.19	0.13	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.37	0.51	0.04	14,17,21	0.18	0.0	0.0	17,0,0				
10	0.0	0.37	0.51	0.04	14,17,21	0.18	0.0	0.0	17,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.33	0.51	0.03	14,17,21	0.17	0.0	0.0	17,0,0				
11	0.0	0.33	0.51	0.03	14,17,21	0.17	0.0	0.0	17,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.29	0.49	0.03	14,17,21	0.17	0.0	0.0	17,0,0				
12	0.0	0.29	0.49	0.03	14,17,21	0.17	0.0	0.0	17,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.27	0.46	0.03	17,17,21	0.16	0.0	0.0	17,0,0				
13	0.0	0.27	0.46	0.03	17,17,21	0.16	0.0	0.0	17,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.26	0.41	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
14	0.0	0.26	0.41	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.24	0.36	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
15	0.0	0.24	0.35	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.21	0.29	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
16	0.0	0.21	0.29	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.19	0.24	0.02	17,17,21	0.0	0.0	0.0	0,0,0				
17	0.0	0.19	0.24	0.02	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.17	0.19	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
18	0.0	0.17	0.19	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.14	0.15	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
19	0.0	0.14	0.15	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.12	0.11	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
20	0.0	0.12	0.11	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.18	0.18	0.04	14,14,21	0.0	0.0	0.0	0,0,0				
21	0.0	0.18	0.18	0.04	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.23	0.29	0.04	14,14,21	0.0	0.0	0.0	0,0,0				
22	0.0	0.23	0.30	0.04	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.28	0.40	0.05	14,14,21	0.0	0.0	0.0	0,0,0				
23	0.0	0.28	0.41	0.05	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.32	0.50	0.05	14,14,21	0.17	0.0	0.0	14,0,0				
24	0.0	0.32	0.50	0.05	14,14,21	0.17	0.0	0.0	14,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.36	0.59	0.06	14,14,21	0.20	0.15	0.0	14,19,0				
25	0.0	0.36	0.59	0.06	14,14,21	0.20	0.15	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.39	0.66	0.07	14,14,21	0.22	0.17	0.0	14,19,0				
26	0.0	0.39	0.67	0.07	14,14,21	0.23	0.17	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.41	0.72	0.07	14,14,21	0.25	0.18	0.0	14,19,0				
27	0.0	0.41	0.73	0.07	14,14,21	0.25	0.18	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.43	0.77	0.08	14,14,21	0.26	0.20	0.0	14,19,0				
28	0.0	0.43	0.77	0.08	14,14,21	0.26	0.20	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.44	0.80	0.08	14,14,21	0.27	0.21	0.0	14,19,0				
29	0.0	0.44	0.80	0.08	14,14,21	0.27	0.21	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.45	0.82	0.08	14,14,21	0.28	0.22	0.0	14,19,0				
30	0.0	0.45	0.82	0.08	14,14,21	0.28	0.22	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.45	0.82	0.08	14,14,21	0.28	0.22	0.0	14,19,0				
31	0.0	0.45	0.82	0.08	14,14,21	0.28	0.22	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.44	0.80	0.08	14,14,21	0.27	0.21	0.0	14,19,0				
32	0.0	0.44	0.80	0.08	14,14,21	0.27	0.21	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.43	0.77	0.08	14,14,21	0.26	0.20	0.0	14,19,0				
33	0.0	0.43	0.77	0.08	14,14,21	0.26	0.20	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.41	0.73	0.07	14,14,21	0.25	0.18	0.0	14,19,0				
34	0.0	0.41	0.72	0.07	14,14,21	0.25	0.18	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.39	0.67	0.07	14,14,21	0.23	0.17	0.0	14,19,0				
35	0.0	0.39	0.66	0.07	14,14,21	0.22	0.17	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.36	0.59	0.06	14,14,21	0.20	0.15	0.0	14,19,0				

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
36	0.0	0.36	0.59	0.06	14,14,21	0.20	0.15	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.32	0.50	0.05	14,14,21	0.17	0.0	0.0	14,0,0				
37	0.0	0.32	0.50	0.05	14,14,21	0.17	0.0	0.0	14,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.28	0.40	0.05	14,14,21	0.0	0.0	0.0	0,0,0				
38	0.0	0.28	0.40	0.05	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.23	0.30	0.04	14,14,21	0.0	0.0	0.0	0,0,0				
39	0.0	0.23	0.29	0.04	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.18	0.18	0.04	14,14,21	0.0	0.0	0.0	0,0,0				
40	0.0	0.18	0.18	0.04	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
41	0.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
42	0.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
43	0.0	0.15	0.14	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.15	0.14	0.02	17,17,21	0.0	0.0	0.0	0,0,0				
44	0.0	0.15	0.14	0.02	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.15	0.13	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
45	0.0	0.15	0.13	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.14	0.12	0.03	17,17,21	0.0	0.0	0.0	0,0,0				
46	0.0	0.14	0.12	0.03	17,17,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.19	0.15	0.03	14,14,21	0.0	0.0	0.0	0,0,0				
47	0.0	0.19	0.15	0.03	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.25	0.25	0.03	14,14,21	0.0	0.0	0.0	0,0,0				
48	0.0	0.24	0.24	0.03	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.29	0.34	0.03	14,14,21	0.0	0.0	0.0	0,0,0				
49	0.0	0.29	0.34	0.03	14,14,21	0.0	0.0	0.0	0,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.33	0.42	0.03	14,14,21	0.14	0.0	0.0	14,0,0				
50	0.0	0.33	0.42	0.03	14,14,21	0.13	0.0	0.0	14,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.37	0.50	0.04	14,14,21	0.16	0.0	0.0	14,0,0				
51	0.0	0.37	0.50	0.04	14,14,21	0.16	0.0	0.0	14,0,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.40	0.57	0.04	14,14,21	0.19	0.13	0.0	14,19,0				
52	0.0	0.40	0.57	0.04	14,14,21	0.19	0.13	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.43	0.64	0.05	14,14,21	0.21	0.15	0.0	14,19,0				
53	0.0	0.43	0.64	0.05	14,14,21	0.21	0.15	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.46	0.70	0.05	14,14,21	0.23	0.17	0.0	14,19,0				
54	0.0	0.46	0.70	0.05	14,14,21	0.23	0.17	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.49	0.75	0.07	14,14,21	0.25	0.19	0.0	14,19,0				
55	0.0	0.49	0.75	0.07	14,14,21	0.25	0.19	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.51	0.80	0.09	14,14,21	0.27	0.21	0.0	14,19,0				
56	0.0	0.51	0.80	0.09	14,14,21	0.27	0.21	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.53	0.84	0.11	14,14,21	0.28	0.23	0.0	14,19,0				
57	0.0	0.53	0.84	0.11	14,14,21	0.28	0.23	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.51	0.72	0.13	14,14,21	0.21	0.18	0.0	14,19,0				
58	0.0	0.51	0.72	0.13	14,14,21	0.21	0.18	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.52	0.74	0.16	14,14,21	0.22	0.19	0.0	14,19,0				
59	0.0	0.52	0.74	0.16	14,14,21	0.22	0.19	0.0	14,19,0	-7.70	-5.34	-0.06	17,20,21
	10.0	0.53	0.77	0.19	14,14,21	0.24	0.21	0.0	14,19,0				
60	0.0	0.52	0.75	0.21	14,14,21	0.23	0.20	0.0	14,19,0	0.15	0.11	-2.75e-03	17,20,21
	11.3	0.53	0.78	0.19	14,14,21	0.24	0.21	0.0	14,19,0				
61	0.0	0.51	0.86	0.24	14,14,21	0.29	0.27	0.0	14,19,0	-0.16	-0.11	-4.05e-03	17,20,21
	11.3	0.52	0.78	0.21	14,14,21	0.24	0.22	0.0	14,19,0				
62	0.0	0.45	0.76	0.24	14,14,21	0.26	0.23	0.0	14,19,0	-0.14	-0.11	5.42e-03	17,20,21
	11.3	0.47	0.74	0.22	14,14,21	0.22	0.20	0.0	14,19,0				
63	0.0	0.37	0.64	0.22	14,14,21	0.22	0.18	0.0	14,19,0	0.15	0.11	6.87e-03	17,20,21
	11.3	0.45	0.82	0.24	14,14,21	0.28	0.25	0.0	14,19,0				
64	0.0	0.27	0.49	0.19	14,14,21	0.17	0.0	0.0	14,0,0	-0.14	-0.11	-8.17e-03	17,20,21
	11.3	0.37	0.69	0.22	14,14,21	0.24	0.20	0.0	14,19,0				
65	0.0	0.17	0.33	0.14	14,14,21	0.0	0.0	0.0	0,0,0	-0.14	-0.11	-9.28e-03	17,20,21
	11.3	0.27	0.54	0.19	14,14,21	0.19	0.0	0.0	14,0,0				
66	0.0	0.15	0.28	0.10	17,17,21	0.0	0.0	0.0	0,0,0	0.13	0.10	9.07e-03	17,20,21
	10.2	0.17	0.35	0.14	14,14,21	0.0	0.0	0.0	0,0,0				
67	0.0	0.16	0.33	0.06	17,17,21	0.0	0.0	0.0	0,0,0	0.13	0.10	9.55e-03	17,20,21
	10.2	0.14	0.28	0.10	17,17,21	0.0	0.0	0.0	0,0,0				
68	0.0	0.18	0.37	0.02	17,17,21	0.0	0.0	0.0	0,0,0	0.13	0.10	-9.84e-03	17,20,21
	10.2	0.16	0.32	0.06	17,17,21	0.0	0.0	0.0	0,0,0				
69	0.0	0.20	0.39	0.02	17,17,21	0.0	0.0	0.0	0,0,0	-0.13	-0.10	-9.94e-03	17,20,21
	10.2	0.18	0.36	0.02	17,17,21	0.0	0.0	0.0	0,0,0				
70	0.0	0.21	0.45	0.04	17,14,21	0.0	0.0	0.0	0,0,0	-0.12	-0.10	-9.88e-03	17,20,21
	10.2	0.20	0.39	0.02	17,17,21	0.0	0.0	0.0	0,0,0				
71	0.0	0.26	0.60	0.07	14,14,21	0.21	0.0	0.0	14,0,0	0.12	0.09	9.66e-03	17,20,21
	10.2	0.21	0.46	0.04	17,14,21	0.0	0.0	0.0	0,0,0				
72	0.0	0.31	0.72	0.10	14,14,21	0.26	0.20	0.0	14,19,0	0.12	0.09	9.29e-03	17,20,21

Trave	Pos.	rRfck	rRfyk	rPfck	Rif. cmb	wR	wF	wP	Rif. cmb	dR	dF	dP	Rif. cmb
	10.2	0.26	0.60	0.07	14,14,21	0.21	0.0	0.0	14,0,0				
73	0.0	0.36	0.84	0.13	14,14,21	0.30	0.25	0.0	14,19,0	0.12	0.09	8.80e-03	17,20,21
	10.2	0.31	0.73	0.10	14,14,21	0.26	0.20	0.0	14,19,0				
74	0.0	0.37	0.76	0.14	14,14,21	0.23	0.21	0.0	14,19,0	-0.12	-0.09	-8.09e-03	17,20,21
	10.2	0.33	0.68	0.12	14,14,21	0.21	0.17	0.0	14,19,0				
75	0.0	0.40	0.83	0.16	14,14,21	0.27	0.24	0.0	14,19,0	-0.12	-0.09	-7.37e-03	17,20,21
	10.2	0.37	0.76	0.14	14,14,21	0.24	0.21	0.0	14,19,0				
76	0.0	0.40	0.75	0.16	14,14,21	0.22	0.20	0.0	14,19,0	0.11	0.09	6.49e-03	17,20,21
	10.2	0.40	0.84	0.16	14,14,21	0.27	0.24	0.0	14,19,0				
77	0.0	0.42	0.79	0.18	14,14,21	0.24	0.21	0.0	14,19,0	-0.11	-0.09	-5.61e-03	17,20,21
	10.2	0.40	0.75	0.16	14,14,21	0.23	0.20	0.0	14,19,0				
78	0.0	0.44	0.83	0.18	14,14,21	0.26	0.23	0.0	14,19,0	-0.11	-0.08	-4.68e-03	17,20,21
	10.2	0.42	0.79	0.18	14,14,21	0.25	0.21	0.0	14,19,0				
79	0.0	0.43	0.73	0.18	14,14,21	0.21	0.18	0.0	14,19,0	-0.11	-0.08	-3.65e-03	17,20,21
	10.2	0.44	0.83	0.18	14,14,21	0.26	0.23	0.0	14,19,0				
80	0.0	0.43	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0	-0.11	-0.08	-2.64e-03	17,20,21
	10.2	0.43	0.74	0.18	14,14,21	0.21	0.18	0.0	14,19,0				
81	0.0	0.44	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0	0.11	0.08	1.60e-03	17,20,21
	10.2	0.43	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0				
82	0.0	0.44	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0	0.11	0.08	5.62e-04	17,20,21
	10.2	0.44	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0				
83	0.0	0.43	0.74	0.18	14,14,21	0.22	0.19	0.0	14,19,0	-0.11	-0.08	-4.77e-04	17,20,21
	10.2	0.44	0.75	0.19	14,14,21	0.22	0.19	0.0	14,19,0				
84	0.0	0.42	0.73	0.18	14,14,21	0.21	0.18	0.0	14,19,0	-0.11	-0.08	-1.50e-03	17,20,21
	10.2	0.43	0.74	0.18	14,14,21	0.22	0.19	0.0	14,19,0				
85	0.0	0.43	0.81	0.18	14,14,21	0.25	0.22	0.0	14,19,0	0.11	0.08	2.52e-03	17,20,21
	10.2	0.45	0.84	0.19	14,14,21	0.27	0.23	0.0	14,19,0				
86	0.0	0.41	0.78	0.17	14,14,21	0.24	0.21	0.0	14,19,0	0.08	0.08	3.49e-03	17,20,21
	10.2	0.43	0.81	0.18	14,14,21	0.25	0.22	0.0	14,19,0				
87	0.0	0.39	0.73	0.16	14,14,21	0.22	0.19	0.0	14,19,0	0.10	0.09	-4.39e-03	17,20,21
	10.2	0.41	0.77	0.17	14,14,21	0.24	0.21	0.0	14,19,0				
88	0.0	0.38	0.80	0.15	14,14,21	0.26	0.22	0.0	14,19,0	-0.10	-0.07	-5.23e-03	17,20,21
	10.2	0.39	0.73	0.16	14,14,21	0.21	0.19	0.0	14,19,0				
89	0.0	0.35	0.73	0.13	14,14,21	0.22	0.19	0.0	14,19,0	-0.11	-0.08	-6.06e-03	17,20,21
	10.2	0.38	0.80	0.15	14,14,21	0.25	0.22	0.0	14,19,0				
90	0.0	0.34	0.79	0.12	14,14,21	0.28	0.22	0.0	14,19,0	0.11	0.08	6.73e-03	17,20,21
	10.2	0.35	0.72	0.13	14,14,21	0.22	0.19	0.0	14,19,0				
91	0.0	0.29	0.67	0.09	14,14,21	0.24	0.0	0.0	14,0,0	-0.11	-0.08	-7.37e-03	17,20,21
	10.2	0.34	0.79	0.12	14,14,21	0.28	0.22	0.0	14,19,0				
92	0.0	0.23	0.54	0.06	14,14,21	0.19	0.0	0.0	14,0,0	0.11	0.08	7.79e-03	17,20,21
	10.2	0.29	0.67	0.09	14,14,21	0.24	0.0	0.0	14,0,0				
93	0.0	0.23	0.39	0.03	17,14,21	0.0	0.0	0.0	0,0,0	-0.11	-0.08	-8.11e-03	17,20,21
	10.2	0.23	0.53	0.06	14,14,21	0.0	0.0	0.0	0,0,0				
94	0.0	0.26	0.38	0.01	17,17,21	0.0	0.0	0.0	0,0,0	0.12	0.08	-8.25e-03	17,20,21
	10.2	0.23	0.39	0.03	17,14,21	0.0	0.0	0.0	0,0,0				
95	0.0	0.29	0.44	0.04	17,17,21	0.15	0.0	0.0	17,0,0	-0.15	-0.09	8.24e-03	17,20,21
	10.2	0.26	0.38	0.01	17,17,21	0.0	0.0	0.0	0,0,0				
96	0.0	0.32	0.50	0.07	17,17,21	0.17	0.0	0.0	17,0,0	-0.21	-0.09	-8.05e-03	17,20,21
	10.2	0.29	0.43	0.03	17,17,21	0.14	0.0	0.0	17,0,0				
97	0.0	0.35	0.55	0.12	17,17,21	0.18	0.15	0.0	17,20,0	-0.23	-0.12	-7.68e-03	17,20,21
	10.2	0.32	0.49	0.07	17,17,21	0.16	0.0	0.0	17,0,0				
98	0.0	0.38	0.60	0.16	17,17,21	0.20	0.17	0.0	17,20,0	-0.25	-0.21	-7.10e-03	17,20,21
	10.2	0.35	0.54	0.12	17,17,21	0.18	0.14	0.0	17,20,0				
99	0.0	0.39	0.61	0.20	17,17,21	0.21	0.17	0.0	14,19,0	-0.28	-0.23	-6.55e-03	17,20,21
	10.6	0.38	0.59	0.16	17,17,21	0.20	0.16	0.0	17,20,0				
100	0.0	0.39	0.73	0.23	14,14,21	0.25	0.21	0.0	14,19,0	0.28	0.23	5.52e-03	17,20,21
	10.6	0.39	0.61	0.20	17,17,21	0.20	0.17	0.0	17,20,0				
101	0.0	0.46	0.83	0.24	14,14,21	0.28	0.26	0.0	14,19,0	0.26	0.23	4.36e-03	17,20,21
	10.6	0.39	0.68	0.23	14,14,21	0.23	0.19	0.0	14,19,0				
102	0.0	0.48	0.74	0.22	14,14,21	0.23	0.20	0.0	14,19,0	-0.21	-0.12	3.11e-03	17,20,21
	10.6	0.46	0.78	0.24	14,14,21	0.26	0.24	0.0	14,19,0				
103	0.0	0.52	0.78	0.21	14,14,21	0.24	0.22	0.0	14,19,0	-0.14	-0.10	1.92e-03	17,20,21
	10.6	0.52	0.87	0.24	14,14,21	0.29	0.27	0.0	14,19,0				
104	0.0	0.53	0.78	0.19	14,14,21	0.24	0.21	0.0	14,19,0	-0.14	-0.10	-7.94e-04	17,20,21
	10.6	0.52	0.75	0.21	14,14,21	0.23	0.20	0.0	14,19,0				
Trave		rRfck	rRfyk	rPfck		wR	wF	wP		dR	dF	dP	
										-7.70	-5.34	-0.06	
		0.54	0.88	0.24		0.30	0.27	0.0		0.28	0.23	9.66e-03	